

# Assessment of engineering noise controls at a talc processing plant

## Introduction

In 2003, more than 12,000 non-metal employees worked in preparation or mill plants (NIOSH, 2003). A NIOSH study revealed that by age 50, approximately 49% of metal/non-metal miners have a material hearing impairment (NIOSH, 2007). Accordingly, there is potential for almost 6,000 nonmetal processing plant workers to be hearing impaired by age 50. This study's noise control work will be useful for the approximately 150 U.S. nonmetal-processing plants (MSHA, 2005) to help them reduce the sound levels of their mills.

With the cooperation of mine officials at a talc processing plant, NIOSH conducted a study to quantify in-plant sound levels and to determine the amount of sound reduction provided by engineering noise controls installed by mine personnel. The long-term goals of the mine officials were to reduce in-plant sound levels and worker noise exposure. The noise control evaluation at the talc processing plant was performed as part of NIOSH's effort to locate and evaluate state-of-the-art engineering noise controls. In addition to locating and assessing existing controls, NIOSH is also identifying processes or machines in need of noise controls, gaps in technology that impede the use of noise controls and barriers to the use of noise controls, including collateral hazards (NIOSH, 1996).

## Abstract

*National Institute for Occupational Safety and Health (NIOSH) researchers conducted an investigation to quantify sound levels and to determine the amount of sound reduction provided by engineering noise controls installed in a talc processing plant. Baseline sound level and sound intensity measurements were performed at the plant, and the measurement locations were recorded for comparison to post-control measurements. Follow-up measurements were then made at the same locations after the initial noise controls were installed. The plant subsequently decided to implement additional noise controls and the researchers returned to conduct measurements for a final analysis of all noise controls. The most significant results showed a sound level reduction in the main mill area from a range of 93 to 104 dB(A) down to a range of 90 to 94 dB(A) and a total sound power level reduction of 21 dB(A) for air classifying Mill 3.*

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The specific noise controls for this study — acoustic curtains and sound barrier and sound absorber materials — as well as the theoretical concepts can be applied not only to talc plants but also to other comparable machinery in all industrial sectors. The noise control retrofit treatments for mining machinery can be found in the Bureau of Mines handbook titled *Mining Machinery Noise Control Guidelines* (Bartholomae and Parker, 1983). There is a high level of consensus about the theory, appropriate principles and evaluation methods for engineering noise controls (Bies and Hansen, 1987; Lord, 1988; Driscoll, 1996; Harris, 1998). This study applied the consensus noise control approach by identifying and quantifying noise sources, developing appropriate engineering and administrative controls, and quantifying the extent of noise reduction attributable to each control intervention alone and in combination.

To identify noise sources and their relative importance, baseline sound level and sound intensity measurements were performed with equipment turned on or off in a pre-selected process. The sound levels and their measurement locations were then entered into SSG-Surfer™ software<sup>1</sup> to produce sound level contour mappings of the mill floor area. Temporary and fixed acoustic curtains and sound absorption material were then used, and post-control sound level and sound intensity measurements were taken to further identify the noise sources. After additional engineering noise controls were installed, sound level and sound intensity measurements were taken to quantify the post-control noise levels and the effectiveness of the controls. For this study, the sound level measurement was averaged for at least 12 seconds (time determined by researcher using B&K and American National Standards Institute [ANSI] recommendations) at each location (American National Standards Institute, 2001). Figure 1 is a top view of the main mill area showing each numbered measurement location. During these measurements, the Bruel & Kjaer<sup>1</sup> (B&K) 2260 Investigator™ was mounted on a tripod such that the measurement microphone was 1.43 m (56 in.) above the floor (International Organization for Standardization, 1987).

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<sup>1</sup> Reference to specific brand names does not imply endorsement by the National Institute for Occupational Safety and Health.

The work patterns and employee locations in this facility fluctuated unpredictably, depending on events that occurred during talc processing. In most cases, employees would be moving in and out of the noisiest areas, and their exposures would probably be very low. However, the mine officials felt that unusual situations could arise where workers would spend prolonged periods of time in the noisy areas. These situations were too unpredictable to be captured reliably through standard full-shift dosimetry. Instead, the scope of the current study was limited to reducing noise sources with the expectation that dose reductions could be verified later, if necessary.

### Sound level measurements

Sound level measurements were conducted at 47 locations, approximately 2 m (79 in.) apart, on the processing plant floor under full operating conditions both with and without noise controls installed. A spot marking each measurement location was painted on the concrete floor to make the repeated measurements as consistent as possible. At every measurement location, the A-weighted equivalent continuous sound pressure level ( $L_{Aeq}$ ) spectrum was measured using a B&K 2260 Investigator™ running Enhanced Sound Analysis software. The reference used when dealing with sound pressure is  $2 \times 10^{-5}$  Pascals (Pa), which is the sound pressure that is barely audible at 1,000 Hz. When measured, this sound pressure would yield a value of 0 dB. The term “level” is commonly used to designate a logarithmic ratio of relevant parameters. Therefore, a sound pressure equal to the reference pressure of  $2 \times 10^{-5}$  Pa ( $1 \text{ Pascal} = 1.45 \times 10^{-4}$  pounds per square inch) produces a sound pressure level (SPL) of 0 dB. To quantify the change in pressure at any point due to a passing sound wave, the root-mean-square (RMS) value is used. The SPL for any sound can be calculated using

$$SPL = 20 \log \times \left( \frac{P_{RMS}}{P_{ref}} \right) \quad (1)$$

where

$P_{RMS}$  is the root mean square sound pressure in Pascals; and

$P_{ref}$  is the reference sound pressure, 0.00002 Pascals (Rossing, 1982).

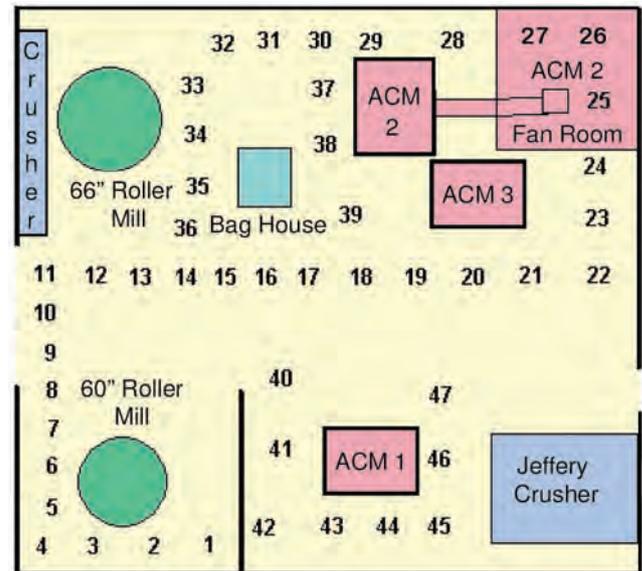
### Sound intensity measurements

Because sound pressure level measurements alone do not locate the primary noise sources, sound intensity measurements were also taken. Once the primary noise sources were located, the sound intensity measurements were repeated after implementing noise controls to quantify their effectiveness.

**Baseline.** To identify noise sources it is recommended to turn components on and off while taking measurements (Driscoll, 1996). For the initial visit to the processing plant, sound levels were measured under different operating conditions (e.g., fluid energy mill [FEM] fans, roller mills or crushers off and/or an air classifying mill [ACM] off — Table 1). These measurements were used to further identify the noise sources by taking baseline measurements with certain machines turned on and/or off and then using acoustic curtains and sound absorptive

**FIGURE 1**

**Sound level measurement locations (not to scale).**



material around or next to certain machines, repeating the measurements and comparing the results. The baseline sound levels with all machines operating ranged from 93 to 104 dB(A), with the highest levels being measured near ACM 3, Location 20 in Fig. 1.

The long-term goals expressed by the plant’s management were to reduce in-plant sound levels and noise exposures of employees. Measuring the baseline sound levels with all equipment operating and measuring the resulting reduction of sound levels after the noise controls are implemented will quantify these goals for the company and demonstrate potential noise reduction. (Note: a second baseline measurement was taken after maintenance and repairs were conducted on ACM 3. This was done to evaluate the reduction of the sound levels resulting from only the noise control installation.)

**Initial engineering noise controls.** For the initial engineering noise controls, and to quantify the contribution to the sound level from these machines, temporary noise controls were recommended to isolate and identify noise sources (Driscoll, 1996). For the study, acoustic curtains were installed around the FEM fans (Fig. 2) and the Jeffrey crusher (Fig. 3). Both of these controls were located on a level above but open to the main mill floor. The ACM 2 fan room is also above the floor area, but it is fully enclosed and not a significant noise contributor. Additional curtains were added to block sound radiating from the lower part of the Jeffrey crusher on the first floor. With the FEM fans and crushers operating, a sound level reduction was achieved in the main mill area from a baseline range of 84 to 91 dB(A) down to an initial control range of 83 to 89 dB(A) (Table 1). While this reduction of about 2 dB(A) is a small numeric change, a reduction of 3 dB(A) would be attributed to reducing the sound energy of the noise source by half (Fader, 1981). Further, when taken in context with the additional controls to be implemented, this initial step was significant

Table 1

Sound level measurements in the main mill area.

Operating condition	Sound level measurements, dB(A)			
	Baseline	Second baseline <sup>1</sup>	Initial controls <sup>2</sup>	Final test <sup>3</sup>
1 FEM fans – On	79-89	78-89	78-88	–
2 FEM fans and crushers – On	84-91	86-91	83-89	79 <sup>5</sup> -92
3 FEM fans, crushers, and ACM 2 – On	87-92	–	–	–
4 FEM fans, crushers, and ACM 3 – On	87-104	–	–	–
5 FEM fans, crushers, all ACMs, and 1.5-m (60-in.) roller mill – On	92-106	91-98	–	–
6 FEM fans, crushers, all ACMs, and 1.7-m (66-in.) roller mill – On	–	90-98	88-94 <sup>4</sup>	–
7 FEM fans, crushers, all ACMs and 60- and 66-in. roller mills – On	93-104	91-100	90-99	90-94 <sup>6</sup>
8 All Machines – Off (background measurements)	–	70-81	–	–

<sup>1</sup> Sound level measurements were taken after maintenance and repairs to ACM 3, with no controls installed.

<sup>2</sup> Initial noise controls; acoustic curtains around FEM fans and Jeffrey crusher, and maintenance and repairs on ACM 3, operating conditions 1, 2 and 7 were measured.

<sup>3</sup> Engineering noise controls installed.

<sup>4</sup> For the measurement of operating Condition 6, additional temporary welding screens draped with acoustical curtains were placed in front of the ACMs and absorptive noise control material was inserted under the hood of the ACM 2.

<sup>5</sup> The low range is suspect because material stopped flowing through the Jeffery crusher while measurements were being taken in that area.

<sup>6</sup> One FEM was not operational, but it was not considered to be a major noise source contributor per Baseline and Second Operating Condition 1.

because it reduced these noise sources' sound energy by almost 35%, it identified the sound level contributions of these noise sources and it allowed for a progression to the next noise control effort.

To study the noise contribution of the ACMs to the main mill area, temporary welding screens draped with acoustical curtains were placed in front of the ACMs. The installation of one of these barriers in front of ACM 2 is shown in Fig. 4. Also, because of the high sound levels measured next to ACM 2, Location 37 in Fig. 1 and the 99 dB(A) area in Fig. 11 (c), sound-absorbing material was inserted under the hood of ACM 2. Under the same operating conditions, the sound levels without

noise controls ranged from 90 to 99 dB(A), while the sound levels with the noise controls ranged from 88 to 94 dB(A) (Table 1, Operating Condition 6). The curtains reduced the sound levels around ACM 1 and ACM 3 by about 2 dB(A). Additionally, while using the sound absorbing material under its hood and curtains around ACM 2, the sound level in front of ACM 2 was reduced from 96 to 92 dB(A). This reduction of 4 dB(A) would be attributed to reducing the sound energy contribution of the noise source to the main mill area by more than 40% (Fader, 1981).

**Air Classification Mill 3.** To further identify the source

FIGURE 2

Curtains around the FEM fans.



FIGURE 3

Curtains around the Jeffrey crusher.



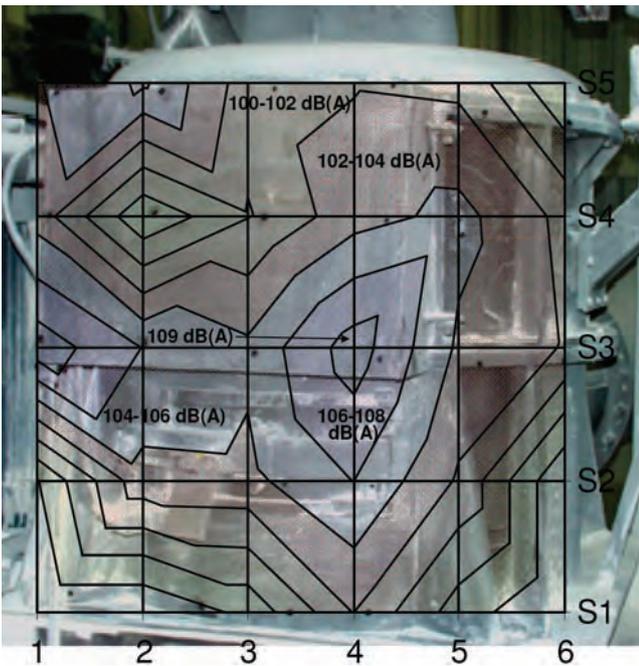
**FIGURE 4**

Acoustic curtain being placed in front of ACM 2.



**FIGURE 5**

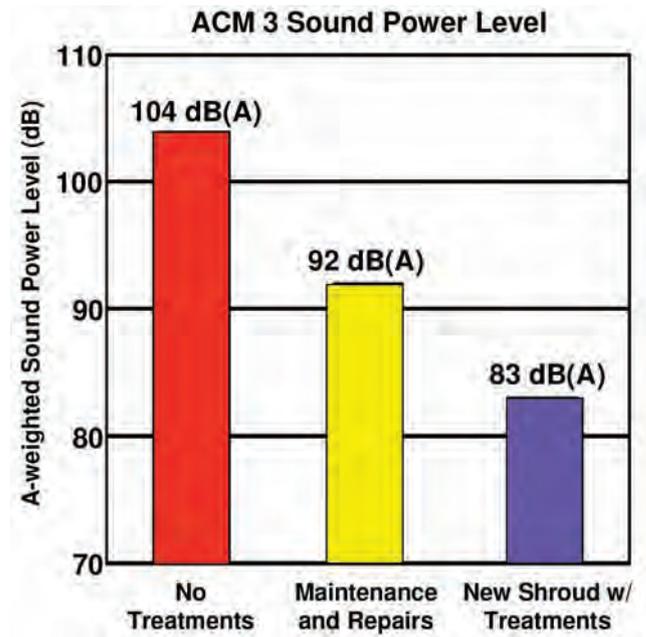
Sound intensity measurement grid on Surface 1 of ACM 3.



of the high sound level of 104 dB(A) measured at Location 20 in Fig. 1, sound intensity measurements were taken in front of ACM 3, designated as Surface 1. Figure 5 shows the measurement grid and the initial sound intensity contour map overlaid on a picture of Surface 1. It can be seen in Fig. 5 that the highest intensity level of 109 dB(A) was measured around the center of the ACM. The calculated sound power level of the grid area is 104 dB(A) (Fig. 6). A frequency analysis of ACM 3 showed a high level at 800 Hz. This calculated high sound power

**FIGURE 6**

Calculated sound power for no noise control treatments, maintenance and repairs and noise controls on Surface 1 of ACM 3.



level was due mainly to this peak and most likely corresponded to the fan blade pass frequency. Once these results were discussed with plant management, the ACM 3's fan was balanced and the shroud door was sealed. Sound intensity measurements after these maintenance and repairs were done ranged from 85 to 96 dB(A). The reduction of the calculated sound power was 12 dB(A) (Fig. 6).

Because a significant sound level reduction of about 3 dB(A), from an average of 95 dB(A) down to about 92 dB(A), was achieved using the acoustical curtains in front of the ACMs, it was decided to engineer noise controls for ACM 3. A larger shroud for ACM 3 was built, and the interior of the shroud was lined with commercially available sound barrier and sound absorber materials — Acoustiblok® and Baff-sorp®, respectively. The sound intensity measured after the new acoustical shroud was in place ranged from 76 to 86 dB(A), the reduction of the calculated sound power level was 9 dB(A) (Fig. 6), and the sound level was reduced by about 7 dB(A) in this area of the plant. Taken alone, this total reduction would be attributed to reducing the sound power contribution of Surface 1 by more than 90% (Fader, 1981).

**1.5-m (60-in.) roller mill duct.** The area near the ductwork of the 1.5-m (60-in.) roller mill (Fig. 7) was identified by an analysis of the baseline sound level measurements as a noisy area, Fig. 11 (a), > 94 dB(A). The baseline sound intensity measurements on the duct, shown as a sound intensity contour plot in Fig. 8, ranged from 82 to 98 dB(A). The calculated sound power level was 93 dB(A). Using a recommended noise control technique (Driscoll, 1996), the duct was wrapped with a sound barrier material. Figure 9 shows the duct after the treatment was applied. The sound intensity measurements on the treated duct ranged from 82 to 94 dB(A),

**FIGURE 7**

**Untreated roller mill duct.**



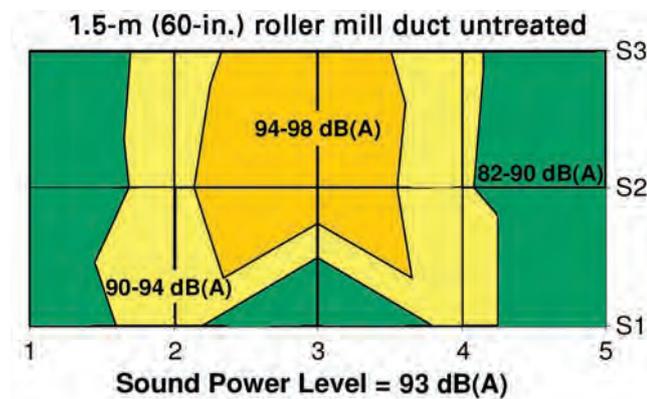
**FIGURE 9**

**Ductwork treated with a sound barrier material.**



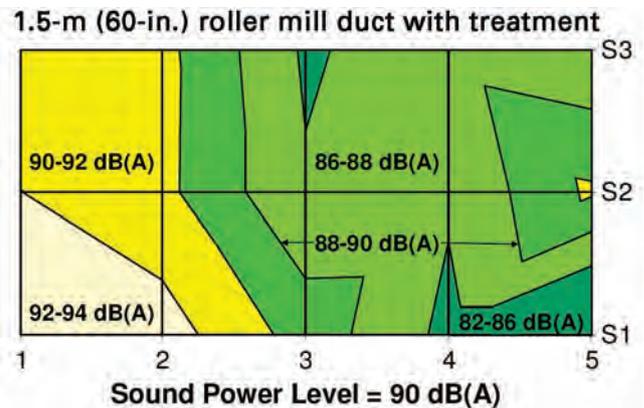
**FIGURE 8**

**Sound intensity measurement results on untreated 1.5-m (60-in.) roller mill duct.**



**FIGURE 10**

**Sound intensity measurement results on treated 1.5-m (60-in.) roller mill duct.**



as shown in Fig. 10. The calculated sound power level for the measurement surface was 90 dB(A). The reduction of the sound power level was 3 dB(A), contributing to the overall a sound level reduction of about 2 dB(A) in this area of the mill. It can be seen in Fig. 9 that the highest sound intensity levels were measured in the middle of the duct. The treatment reduced the sound intensity in this area by more than 10 dB(A). The reduction of the sound power level by 3 dB(A) would be attributed to reducing the sound energy of the noise source by 50% (Fader, 1981).

**All engineering noise controls installed.** The installed engineering noise controls consisted of:

- acoustic curtains around the FEM fans and the crushers;
- acoustic curtains in front of ACM 1 and 2 and absorptive noise control material inserted under the hood of ACM 2;

- a larger shroud for ACM 3, filled with a noise barrier and noise absorptive material; and
- 1.5-m (60-in.) roller mill duct wrapped with noise barrier material.

It must be noted that simple maintenance and repairs on ACM 3 reduced the sound level, measured at Location 20 in Fig. 1, by about 10 dB(A). Therefore, a second baseline was established (Table 1, operating Condition 7). This was before the followup test measurements with initial noise controls installed were taken. For the final test, the main mill area sound levels were again measured using the same 47 measurement points that were used during the initial visit. The second baseline sound level measurements ranged from 91 to 100 dB(A). After the implementation of controls the sound levels ranged from 90 to 94 dB(A) (Table 1). On average, the engineering noise controls reduced the sound level on the main mill floor by 4 dB(A).

Figure 11 shows four different operating conditions

during the noise control study. The following sound level measurements were taken in the mill: (a) baseline (no noise controls installed), (b) with initial acoustic curtains, (c) with additional acoustic curtains in front of the ACMs and (d) with fully installed noise controls.

A long-term goal of the mine officials to reduce in-plant sound levels was accomplished and this will subsequently reduce worker noise exposure. The remaining levels are still hazardous, so administrative controls and hearing protection devices (HPDs) are still needed to avoid the risk of hearing damage. It is more likely that HPDs will provide adequate protection for noise levels of 90 to 94 dB(A) than the precontrols levels exceeding 100 dB(A). Before the controls, worker overexposure to noise would occur in the loudest area of the mill in about one hour, now over-exposure would occur in about 5 hours, under MSHA criteria (CFR, 1999).

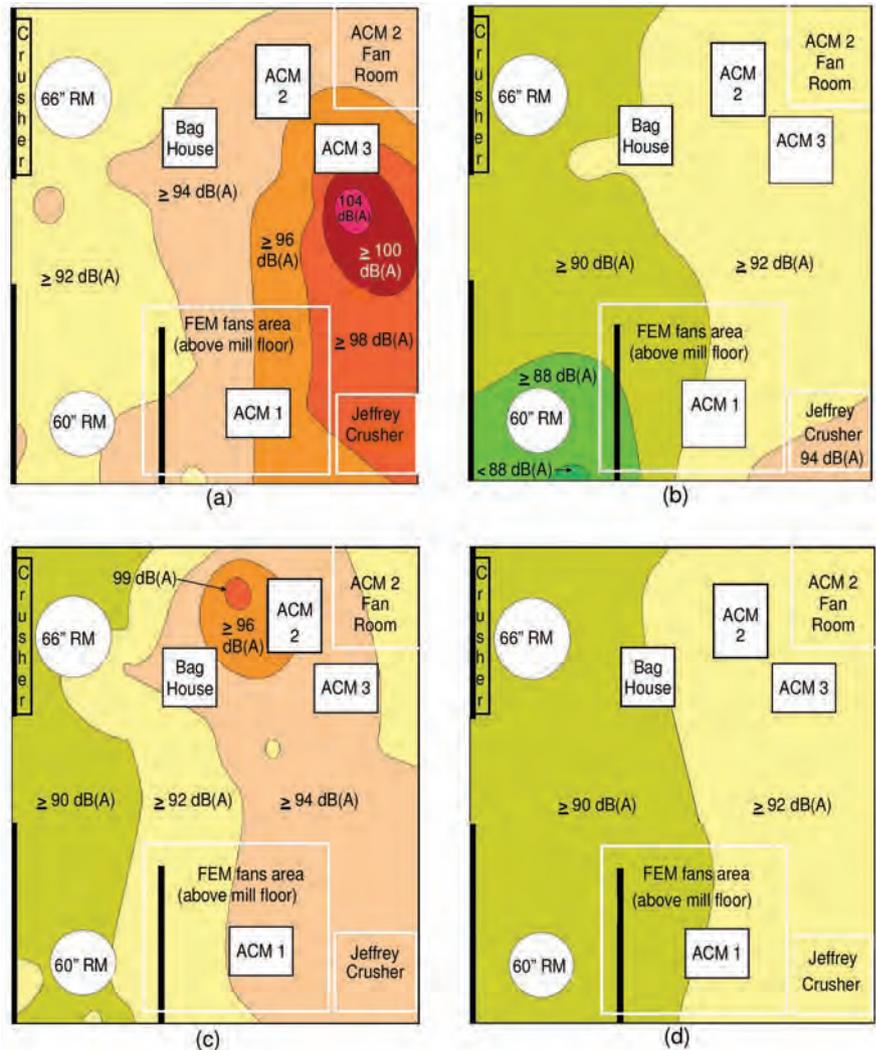
### Summary

With the cooperation of mine officials, the National Institute for Occupational Safety and Health (NIOSH) conducted a study to quantify sound levels and to determine the sound reduction provided by engineering noise controls installed in a talc processing plant. Sound intensity and sound level measurements were performed in the plant before and after installing noise controls.

The baseline sound level measurements ranged from 93 to 104 dB(A). The initial engineering noise controls consisted of acoustic curtains installed around the FEM fans and the Jeffrey crusher. Acoustic curtains were then used in front of the other crusher and the ACMs, sound-absorbing material was inserted under the hood of ACM 2, and maintenance and repairs on ACM 3 were completed. The sound levels measured after this work was completed ranged from 88 to 94 dB(A), a significant reduction of 10 dB(A) from the highest baseline sound level. For the loudest ACM, the noise controls consisted of building a larger shroud, lining the inside of the shroud with a sound barrier material, and filling the interior of the shroud with sound absorbing material. Sound intensity measured after the new shroud was in place ranged from 76 to 86 dB(A), and a remarkable reduction in the sound power level of 9 dB(A) was achieved on the measurement surface. The final control for this study was wrapping the duct of a 1.5-m (60-in.) roller mill with a sound barrier material. The highest sound intensity measurement of the duct was reduced by 6 dB(A), and the sound power level on the measurement surface was reduced by 3 dB(A). The main mill area second baseline sound level measurements taken after maintenance and

**FIGURE 11**

**Contour maps for (a) baseline, (b) acoustic curtains around the FEM fans and upper and lower levels of the Jeffrey crusher, (c) acoustic curtains around the FEM fans, upper and lower levels of the Jeffrey crusher and (d) in front of ACMs all engineering controls.**



repairs on ACM 3, ranged from 91 to 100 dB(A). The final noise control sound levels measurements were reduced to a range of 90 to 94 dB(A).

Using these or similar controls at the other U.S. non-metal processing plants could reduce the exposure of roughly 6,000 workers. Mine management would still have to use administrative controls or require the workers to wear hearing protection to reduce the risk of hearing damage, but the extent of overexposure was decreased significantly. MSHA's preferred method for assessment of miners' exposure and noise controls involve full shift dosimetry along with time-motion studies. While this method was not accomplished here, an assessment of the sound level reduction increases the time a worker can spend in the mill without being overexposed to noise by about 4 hours. The significant noise reductions that were obtained through noise controls and repairs would necessarily reduce exposure, especially in the unusual situation where workers needed to remain in the noisiest areas for prolonged periods. Capturing these atypical situations

through full-shift dosimetry was beyond the scope of the current study.

## Disclaimer

The findings and conclusions in this report have not been formally disseminated by the National Institute for Occupational Safety and Health (NIOSH) and should not be construed to represent any agency determination or policy.

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