## Recommendations for a New Rock Dusting Standard to Prevent Coal Dust Explosions in Intake Airways


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Kenneth L. Cashdollar, Michael J. Sapko, Eric S. Weiss, Marcia L. Harris, Chi-Keung Man, Samuel P. Harteis, and Gregory M. Green

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## ACRONYMS AND ABBREVIATIONS USED IN THIS REPORT

| \% TIC | Percentage of Total Incombustible Content |
| :--- | :--- |
| ASTM | American Society for Testing and Materials |
| BEM | Bruceton Experimental Mine |
| CFR | Code of Federal Regulations |
| D $_{\text {med }}$ | mass median diameter |
| D $_{s}$ | surface mean diameter |
| D $_{\text {w }}$ | mass or volume mean diameter |
| hvb | high volatile bituminous |
| hvCb | high volatile C bituminous |
| LLEM | Lake Lynn Experimental Mine |
| LLL | Lake Lynn Laboratory |
| LTA | low temperature ashing |
| Ivb | low volatile bituminous |
| MSHA | Mine Safety and Health Administration |
| mvb | medium volatile bituminous |
| NIOSH | National Institute for Occupational Safety and Health |
| NP | non-propagation |
| OMSHR | Office of Mine Safety and Health Research |
| P | Propagation |
| PC | personal computer |
| TIC | Total Incombustible Content |

## UNIT OF MEASURE ABBREVIATIONS USED IN THIS REPORT

| $\mathrm{Btu} / \mathrm{lb}$ | British thermal unit per pound |
| :--- | :--- |
| cm | centimeter |
| ${ }^{\circ} \mathrm{C}$ | degree Celsius |
| ft | foot |
| $\mathrm{g} / \mathrm{m}^{3}$ | gram per cubic meter |
| hr | hour |
| kPa | kilopascal |
| m | meter |
| $\mu \mathrm{m}$ | micrometer or micron |
| $\mathrm{mt} / \mathrm{yr}$ | million ton per year |
| ms | millisecond |
| $\%$ | percent |
| psi | pound-force per square inch |
| $\mathrm{sec}^{2}$ | second |
| $\mathrm{ft}^{2}$ | square foot |
| $\mathrm{m}^{2}$ | square meter |

## Dedication

This report was initially prepared by Kenneth L. Cashdollar and is dedicated to his memory. Ken passed away on March 4, 2009. Ken never wavered from his continuing commitment to conduct the highest quality, solution-oriented, scientific research focused on reducing the risk of explosion fatalities in the mining and chemical industries.


# Recommendations for a New Rock Dusting Standard to Prevent Coal Dust Explosions in Intake Airways 

Kenneth L. Cashdollar ${ }^{1}$, Michael J. Sapko ${ }^{2}$, Eric S. Weiss ${ }^{3}$, Marcia L. Harris ${ }^{4}$, Chi-Keung Man ${ }^{5}$, Samuel P. Harteis ${ }^{6}$, and Gregory M. Green ${ }^{7}$

## Executive Summary

The workings of a bituminous coal mine produce explosive coal dust for which adding rock dust can reduce the potential for explosions. Accordingly, guidelines have been established by the Mine Safety and Health Administration (MSHA) about the relative proportion of rock dust that must be present in a mine's intake and return airways. Current MSHA regulations require that intake airways contain at least $65 \%$ incombustible content and return airways contain at least $80 \%$ incombustible content. The higher limit for return airways was set in large part because finer coal dust tends to collect in these airways. Based on extensive in-mine coal dust particle size surveys and large-scale explosion tests, the National Institute for Occupational Safety and Health (NIOSH) recommends a new standard of $80 \%$ total incombustible content (TIC) be required in the intake airways of bituminous coal mines in the absence of methane.

MSHA inspectors routinely monitor rock dust inerting efforts by collecting dust samples and measuring the percentage of TIC, which includes measurements of the moisture in the samples, the ash in the coal, and the rock dust. These regulations were based on two important findings: a survey of coal dust particle size that was performed in the 1920s, and large-scale explosion tests conducted in the U.S. Bureau of Mines' Bruceton Experimental Mine (BEM) using dust particles of that survey's size range to determine the amount of inerting material required to prevent explosion propagation.

Mining technology and practices have changed considerably since the 1920s, when the original coal dust particle survey was performed. Also, it has been conclusively shown that as the size of coal dust particles decreases, the explosion hazard increases. Given these factors, NIOSH and MSHA conducted a joint survey to determine the range of coal particle sizes found in dust samples collected from intake and return airways of U.S. coal mines. Results from this survey show that the coal dust found in mines today is much finer than in mines of the 1920s. This increase in fine dust is presumably due to the increase in mechanization.

In light of this recent comprehensive dust survey, NIOSH conducted additional large-scale explosion tests at the Lake Lynn Experimental Mine (LLEM) to determine the degree of rock dusting necessary to abate explosions. The tests used Pittsburgh seam coal dust blended as $38 \%$ minus 200 mesh and referred to as medium-sized dust. This medium-sized blend was used to

[^0]represent the average of the finest coal particle size collected from the recent dust survey. Explosion tests indicate that medium-sized coal dust required 76.4\% TIC to prevent explosion propagation. Even the coarse coal dust ( $20 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ), representative of samples obtained from mines in the 1920 s , required approximately $70 \%$ TIC to be rendered inert in the larger LLEM, a level higher than the current regulation of $65 \%$ TIC.

Given the results of the extensive in-mine coal dust particle size surveys and large-scale explosion tests, NIOSH recommends a new standard of $80 \%$ TIC be required in the intake airways of bituminous coal mines in the absence of methane. The survey results indicate that in some cases there are no substantial differences between the coal dust particle size distributions in return and intake air courses in today's coal mines. The survey results indicate that the current requirement of $80 \%$ TIC in return airways is still appropriate in the absence of background methane.

## Introduction

Despite the worldwide research on coal mine safety, coal mine explosions involving fatalities and injuries still occur [Dobroski et al. 1996; McKinney et al. 2002; Light et al. 2007]. Experimental studies by the Office of Mine Safety and Health Research ${ }^{8}$ (OMSHR) and similar agencies in other countries have shown that inert rock dust acts as a heat sink, and mixing a sufficient quantity of inert rock dust with coal dust will prevent coal dust explosions [Cybulski 1975; Michelis et al. 1987, 1996; Reed et al. 1989; Lebecki 1991]. The U.S. mining law pertaining to rock dusting for the prevention of coal dust explosions was specified in the Federal Coal Mine Health and Safety Act of 1969 and was included in the Federal Mine Safety and Health Act of 1977 [U.S. Congress 1969 and 1977]. Current regulations are specified in Title 30, Part 75, Section 75.403 of the U.S. Code of Federal Regulations (CFR) [30 CFR ${ }^{9}$ 2010]. Current regulations state that U.S. bituminous coal mines must maintain an incombustible content of at least $65 \%$ in the non-return (intake) airways and at least $80 \%$ in the return airways. Return airways require more inert material because there is greater risk of accumulation of finer coal dust. The U.S. regulations also require an additional $1.0 \%$ incombustible by weight for each $0.1 \%$ of methane in the ventilating air inside intakes and $0.4 \%$ additional incombustible for each $0.1 \%$ of methane in returns.

The total incombustible content (TIC) includes measurements of the moisture in the samples, the ash in the coal, and the rock dust. The $65 \%$ TIC required for intake airways was adopted based on the results of two studies. First, coal dust samples were collected and measured to determine the average size of coal dust particles. Next, full-scale experimental mine tests were conducted to determine the amount of rock dust required for coal particles of the size collected in the survey to be rendered inert [Nagy 1981]. The term "mine-size dust" was adopted in the mid1920s and refers to coal dust that passes through a U.S. Standard 20-mesh sieve ( $850 \mu \mathrm{~m}$ ) and contains $20 \%$ minus 200 mesh ( $75 \mu \mathrm{~m}$ ). The justification for adopting this definition is given in Bureau of Mines Technical Paper 464 [Rice and Greenwald 1929]. Briefly, Technical Paper 464 indicates that coal dust samples collected from the mine floors had $5 \%$ to $40 \%$ of the material minus 200 mesh $(75 \mu \mathrm{~m})$ and that the values were weighted. For $80 \%$ of mines, the final values ranged from $15 \%$ to $25 \%$ through 200 mesh. Therefore, coal dust having $20 \%$ passing through 200 mesh was considered to be typical and termed "mine-size dust." The authors of Technical Paper 464 acknowledge that dust collected from ribs, roof, and timbers was finer, with $40 \%$ to $75 \%$ of the particles finer than 200 mesh, though they do not list the distribution of dust that would pass through sieves other than 200 mesh. Also missing from the report are details on the total number of mines surveyed and the total number of samples analyzed for coal particle size. Many years later, Public Law 552 ( $82^{\text {nd }}$ Congress, 1952) required $65 \%$ incombustible content for most mines entries but it did not differentiate between intake and return areas.

The quantities of rock dust required in the return airways in bituminous coal mines in the United States were increased to $80 \%$ by enactment of Public Law 91-173, the Federal Coal Mine Health and Safety Act of 1969. Section 304(a) mandated that coal dust shall be cleaned up and not permitted to accumulate in active workings or on electrical equipment. Paragraph (b) noted that when excessive dust is raised, water, water plus a wetting agent, or other no less effective

[^1]agent shall be applied to abate dust, especially in distances less than 40 feet from the face to minimize explosion hazards. Paragraph (c) required that all underground areas where the incombustible content is too low shall be rock dusted to within 40 feet of the face. All crosscuts that are less than 40 feet from a working face shall also be rock dusted. Section 304(d) reads as follows:

Where rock dust is required to be applied, it shall be distributed upon the top, floor, and sides of all underground areas of a coal mine and maintained in such quantities that the incombustible content of the combined coal dust, rock dust, and other dust shall be not less than 65 per centum, but the incombustible content in the return air courses shall be no less than 80 per centum. Where methane is present in any ventilating current, the per centum of incombustible of such combined dusts shall be increased 1.0 and 0.4 per centum for each 0.1 per centum of methane, where 65 and 80 per centum respectively, of incombustibles are required.

The aforementioned requirement of $80 \%$ TIC in return airways represents an increase over previous standards for return airways. The entire standard was based on earlier research with "mine-size dust." The incombustible content needed to prevent propagation given a particular coal dust size is also dependent, to a lesser extent, on the volatility content of the coal. The decision to require all coal dusts except anthracite to have $65 \%$ TIC was made in 1927 by the Mine Safety Board. Decision No. 5, relating to rock dusting [Rice 1927], was superseded and clarified by Decision No. 32 [Mine Safety Board, 1937]. All Federal mine codes and laws since the mid-1920s have contained the same requirement. The requirement to have a $65 \%$ incombustible content for all coals except anthracite was made to simplify rock dusting practices. Coals that have a volatile ratio [volatile ratio $=$ volatile content $/$ (volatile content + fixed carbon)] of less than 0.2 provide a greater margin of explosion protection than coals having a volatile ratio higher than 0.2 [Nagy 1981].

The effect of coal particle size on explosibility is illustrated in Figure 1 as adapted from Rice et al. [1922] and Rice and Greenwald [1929]. This figure shows the amount of incombustible dust required to prevent propagation of an explosion for Pittsburgh high volatile bituminous coal dust with $10 \%$ to $80 \%$ passing through a 200 mesh $(75 \mu \mathrm{~m})$ sieve. Each of the data points is an individual explosion test conducted in the NIOSH-OMSHR Bruceton Experimental Mine (BEM). The curve is the boundary between mixtures that can propagate an explosion (below line) and mixtures that cannot propagate an explosion (above line). These data were used to support the $65 \%$ incombustible requirement for intake and return airways based on "mine-size dust" of the time.


Figure 1. Effect of particle size of coal dust on the explosibility of Pittsburgh seam bituminous coal as tested within BEM.

## Comparison of International Rock Dusting Requirements

Rock dust has been used for about 100 years as a precautionary measure to protect against dust explosions. It is generally agreed that the effectiveness of rock dust lies in its ability to be simultaneously dispersed with coal dust, and, by serving as a heat sink, thus prevent flame propagation. Most leading coal-producing nations have similar requirements, some more stringent and some less stringent than those enforced in the United States. A partial listing of these requirements is given in Table 1. Passive barriers have been deployed in most leading coalproducing nations to provide supplemental protection against coal dust explosions. Conveyor belt entries have received emphasis. Barriers are designed to quench an explosion immediately on arrival at the location [Cybulski 1975, Liebman et al 1974, and Sapko et al 1989].

Table 1. Summary of rock dusting requirements for various nations

| Country | TIC \% | Volatile matter \% | Methane \% | Comments |
| :---: | :---: | :---: | :---: | :---: |
| Australia Queensland | 85-80 (return) <br> 85-70 (intake) | - |  | $85 \%$ TIC $\leq 200 \mathrm{~m}$ from the face $80 \%$ TIC > 200 m from the face $85 \%$ TIC $\leq 200 \mathrm{~m}$ from the face $70 \%$ TIC > 200 m from the face Supplemental protection-barriers |
| Australia NSW | 85-70 (return) <br> 80-70 (intake) | - |  | $85 \%$ TIC $\leq 200 \mathrm{~m}$ from the face $70 \%$ TIC $>200 \mathrm{~m}$ from the face $80 \%$ TIC $\leq 200 \mathrm{~m}$ from the face $70 \%$ TIC > 200 m from the face Supplemental protection—barriers |
| Canada (Nova Scotia) | 75 (intake) <br> 80 (return) | - | $\begin{aligned} & <1 \\ & >1 \end{aligned}$ |  |
| Czech Republic | 80 (intake/return) <br> 85 (intake/return) | - | $\begin{aligned} & <1 \\ & >1 \end{aligned}$ | Supplemental protection-barriers |
| Slovakia | 80 (intake/return) <br> 85 (intake/return) | - | $\begin{aligned} & <1 \\ & >1 \end{aligned}$ | Supplemental protection-barriers |
| Germany | 80 (intake/return) | - |  | Supplemental protection-barriers |
| Japan | 78 (intake/return) 83 (intake/return) | $\begin{aligned} & 35 \\ & 35 \end{aligned}$ | $\begin{aligned} & <1 \\ & >1 \end{aligned}$ | Specific requirements depend on ash, moisture and volatile content, the gassiness of the seam, and the fineness of the rock dust used. |
| Poland | 70 (intake/return) | $\begin{aligned} & >10 \\ & >10 \end{aligned}$ |  | $70 \%$ in "non-gassy" roadways 80\% in "gassy" roadways Supplemental protection-barriers |
| South Africa | 80 (intake) <br> 80 (return) | - - |  | $80 \%$ TIC $\leq 200 \mathrm{~m}$ from the face $65 \%$ TIC > 200 m from the face $80 \%$ TIC for 1000 m from the face Supplemental protection-barriers |
| United Kingdom | 50 (intake/return) 65 (intake/return) 72 (intake/return) 75 (intake/return) | $\begin{array}{r} 20 \\ 27 \\ 35 \\ >35 \end{array}$ |  | Supplemental protection—barriers |
| United States | 65 (intake) <br> 80 (return) | - | $\begin{aligned} & 1.0 / 0.1 \\ & 0.4 / 0.1 \end{aligned}$ | Add 1\% TIC / 0.1\% methane Add 0.4\% TIC / 0.1\% methane |

From 1985 through 2001, numerous coal dust explosion tests were conducted in the single entry D-drift at LLEM to determine the concentration of rock dust required to prevent explosion propagation of samples with varying coal dust particle sizes, volatilities, mine entry size, and other related properties. The LLEM drifts ( $20-\mathrm{ft}$ or $6-\mathrm{m}$ wide by $6.5-\mathrm{ft}$ or $2-\mathrm{m}$ high) are more representative of current U.S. underground coal mine geometries compared to the much smaller BEM entries ( $9-\mathrm{ft}$ or $2.7-\mathrm{m}$ wide by $6-\mathrm{ft}$ or $1.8-\mathrm{m}$ high).

The factors that can influence the amount of admixed rock dust required to make coal dust inert include coal and rock dust particle size distribution, coal dust volatile content, and the additional presence of methane. Much knowledge has been obtained from experimental mine and laboratory dust explosion research during the past 3 decades. Investigators have examined the effects of rock dust inerting requirements, the minimum explosible coal dust concentrations, the effect of volatile matter on the explosibility of coal dusts, the effect of the size of coal and rock dust particles, and the effect of background methane in full-scale experimental mines and in laboratory test vessels [Sapko et al. 1987a, b; 1989; 1998; 2000; Cashdollar 1996; Cashdollar and Hertzberg 1989; Cashdollar and Chatrathi 1993; Cashdollar et al. 1987; 1988; 1992a, b, c; 2007]. Further research evaluated the effects of pulverized versus coarse coal particle size [Weiss et al. 1989], coal volatility, extinguishment, and pyrolysis mechanisms [Hertzberg et al. 1987; 1988a, b; Conti et al. 1991; Greninger et al. 1991]. The clear cumulative consensus of these studies is that dust particle size emerges as the single most influential factor controlling coal dust explosion propagation. Therefore, the primary focus of this research was to examine the effect of coal particle size of Pittsburgh coal while holding other factors constant.

To determine compliance with current regulations, inspectors from MSHA periodically collect samples of deposited dust from various areas in a mine. The MSHA laboratory determines TIC and compares it with the TIC requirement. This TIC requirement is based on a mean coal particle size of $20 \%$ minus 200 mesh and assumed to be constant throughout the intake entries. The size of the coal dust component is not measured by MSHA laboratories as part of the explosibility assessment.

This report presents the results of extensive in-mine coal dust particle size surveys of dust samples collected from intake airways in 61 U.S. coal mines, representing all 10 MSHA bituminous Coal Mine Safety and Health Districts (Figure 2). MSHA District 1 covers anthracite mines in Pennsylvania, which do not require rock dusting. A preliminary version of this research with data from 50 mines was published by Sapko et al. [2007]. Samples from return airways in 36 mines were also size analyzed. A series of large-scale dust explosion tests was then conducted at the LLEM using the average of the finest coal particle size from the MSHA district intake survey results to determine the incombustible content necessary to prevent explosion propagation.


Figure 2. MSHA Coal Mine Safety and Health Districts, identified by number.

## Experimental Procedures

To assess current variations in coal particle size from various underground coal mining operations, MSHA coordinated the acquisition of mine dust samples from the 10 bituminous Coal Mine Safety and Health Districts. The dust samples were among those routinely collected by mine inspectors to assess compliance with 30 CFR 75.403. The detailed sampling protocols are summarized in the General Coal Mine Inspection Procedures and Inspection Tracking System [MSHA 2008]. The samples were sent to the MSHA laboratory at Mt. Hope, WV, and analyzed for total incombustible content (TIC). The TIC includes measurements of the moisture in the samples, the ash in the coal, and the rock dust. The incombustible analysis procedure [Montgomery 2005] begins by passing the sample through a 20 -mesh sieve $(850 \mu \mathrm{~m})$ and then oven drying the minus $20-$ mesh material for 1 hr at $105^{\circ} \mathrm{C}$. The weight lost during drying constitutes the as-received-moisture in the sample. Next, the dried sample is heated in an oven that is ramped up over 1.5 hr and held at $515^{\circ} \mathrm{C}$ for about 2.5 hr to burn off the combustible coal fraction, thereby leaving the ash and incombustible material. This low temperature ashing (LTA) burns off the coal but does not decompose the limestone rock dust. The amount of the remaining ash material plus the as-received-moisture divided by the initial weight is reported as \%TIC. Portions of each dust sample that were not needed for TIC measurement were sent to NIOSHOMSHR for the analyses of coal particle sizes.

At OMSHR, the limestone (or marble) rock dust was leached from the sample using hydrochloric acid. In this leaching method used in the laboratory, dilute hydrochloric acid was added to the dust sample in a beaker and heated on a hotplate. The acid reacted with the limestone or marble rock dust, producing foam while releasing carbon dioxide. Sufficient acid was added until all foaming stopped. The hotplate kept the slurry near its boiling point for about 1 hr . After the slurry cooled, the acid-insoluble residue was filtered from the acid. The solid residue was rinsed with water and isopropanol and then transferred to a large evaporating dish. The residue was dried at $110^{\circ} \mathrm{C}$ for 3 hr . Agglomerates were broken with a spatula. The residue consisted of coal plus other insoluble mineral matter.

The dried residue was then classified into the different size fractions using a sonic sieve, which provided particle separation by combining two motions-a vertical oscillating column of air, and a repetitive mechanical pulse. Occasionally the tops of the sieves were brushed to break up any remaining agglomerates. The sieves are 8 cm in diameter and include the following sizes: 20 mesh $(850 \mu \mathrm{~m}), 30 \operatorname{mesh}(600 \mu \mathrm{~m}), 40 \operatorname{mesh}(425 \mu \mathrm{~m}), 50 \operatorname{mesh}(300 \mu \mathrm{~m}), 70 \operatorname{mesh}(212$ $\mu \mathrm{m}), 100$ mesh $(150 \mu \mathrm{~m}), 140$ mesh $(106 \mu \mathrm{~m}), 200$ mesh $(75 \mu \mathrm{~m}), 270$ mesh $(53 \mu \mathrm{~m})$, and 400 mesh $(38 \mu \mathrm{~m})$. After the sieving was completed, the weight of sample on each sieve was recorded.

Because the residue from the leaching process contained other inert mineral matter that did not react with the acid, a correction to the size analysis had to be made. First, the residue was grouped into three size fractions: minus 200 mesh, $200-70$ mesh, and plus 70 mesh. At OMSHR, these three fractions were heated to $515^{\circ} \mathrm{C}$ to determine the incombustible or non-coal content, using an LTA method similar to that of the MSHA laboratory at Mt. Hope. The analyses of sieve size were then corrected for the non-coal content (insoluble mineral matter) in the three size groupings. The amount of this insoluble mineral matter in the samples varied greatly, but it was generally in the $20 \%$ to $50 \%$ range. For most of the samples analyzed, the insoluble mineral matter was finer than the coal particles. Therefore, after correction for the mineral matter, the corrected minus 200 -mesh amount would be less than the original minus 200-mesh amount determined by sonic sieving alone. There was a wide range of correction values, but a value of $39 \%$ minus 200 mesh from the original sieving data might typically be reduced to $\sim 31 \%$ minus 200 mesh after correcting for the mineral matter. Details of the size analyses, listing both original and corrected data, are included in the tables of Appendixes A and B.

The total size analysis procedure (acid leaching, sieving, and correction for remaining incombustible matter) was verified by using prepared mixtures of coal and rock dust. First, the particle size distribution of the coal sample was determined by sieving. Next, samples of coal and rock dust were mixed together, and the rock dust was leached from the mixture. The residue was then sieved and corrected via LTA for any remaining incombustible matter in the size fractions. Data for a mixture of $30 \%$ medium-sized Pittsburgh seam high volatile coal and $70 \%$ limestone rock dust are shown in Figure 3. Both the cumulative and differential size distributions (by mass) are shown. A gold dashed vertical line shows the 200 mesh ( $75 \mu \mathrm{~m}$ ) size and a dotdashed vertical orange line shows the 70 mesh $(212 \mu \mathrm{~m})$ size. Both the original coal (red data curves) and acid-leached residue from the mixture (blue data curves) had their size analyses corrected via LTA for any remaining incombustible matter. For this mixture, both the percentage through 200 mesh and the median size ( $50 \%$ point on the cumulative distribution curve) were almost identical for the original coal and the residue from the acid-leached mixture. Figure 4 shows similar data for a mixture of $30 \%$ medium-sized Pittsburgh seam coal, $60 \%$ limestone rock dust, and $10 \%$ kaolin clay (to simulate possible shale dust in the sample). The original coal data are shown by the red curves and the acid-leached residue data from the mixture are shown by the blue curves. Figure 4 also shows close agreement for the percentage through 200 mesh and almost identical median values from the two cumulative curves. Original and acid-leached Blue Creek seam and Pocahontas seam samples were compared, but without any added rock dust. In general, the size analyses after leaching were within $1 \%$ to $3 \%$ of the amount of minus 200 mesh material (data not shown). Therefore, there is no evidence that the acid-leaching procedure compromises the accuracy of the sieve analysis of the coal dust.


Figure 3. Original analyses of coal sieve size and analyses of sieve size of acid-leached mixture containing 30\% medium-sized Pittsburgh coal and 70\% limestone rock dust.


Figure 4. Original analyses of coal sieve size and analyses of sieve size of acid-leached mixture containing 30\% medium-sized Pittsburgh coal, $60 \%$ limestone rock dust, and $10 \%$ kaolin clay.

The large-scale explosion tests were conducted in the LLEM, which is shown in the plan view of Figure 5 [Triebsch and Sapko 1990]. This is a former limestone mine, and five new drifts (horizontal passageways in a mine) were developed to simulate the geometries of modern U.S. coal mines. The mine has four parallel drifts-A, B, C, and D. D-drift is a 1,640-ft-long ( $500-\mathrm{m}$ ) entry that can be separated from E-drift by an explosion-resistant bulkhead door. In order to simulate room and pillar workings, drifts $\mathrm{A}, \mathrm{B}$, and C can be used. These three drifts are approximately $1,600 \mathrm{ft}$ long ( $490-\mathrm{m}$ ), with seven crosscuts at the inby end. Drifts C and D are connected by E-drift, a 500 -ft-long ( $152-\mathrm{m}$ ) entry that simulates a longwall face. Explosion tests can be conducted in the single entry D-drift, the multiple entry area of A-, B-, and C-drifts, or various other configurations including the longwall E-drift. The entries are about 20 ft wide (6m ) by about 6.5 ft high ( $2-\mathrm{m}$ ), with cross-sectional areas of $130-140 \mathrm{ft}^{2}\left(12-13 \mathrm{~m}^{2}\right)$. The LLEM bulkhead door and some of the other infrastructure were designed to withstand explosion overpressures of up to $100 \mathrm{psi}(7 \mathrm{bar}$ or 700 kPa$)$. Higher pressures have been recorded at areas away from these structures. Previous publications described the LLEM coal dust explosion test procedures and the results of LLEM explosion research and post-explosion observations [Weiss et al. 1989; Greninger et al. 1991; Cashdollar et al. 1992b, c; Sapko et al. 1998; 2000].

Each LLEM drift has 10 data-gathering stations inset in the rib, which houses a strain gauge transducer to measure the explosion pressure and an optical sensor to detect flame arrival. The wall pressure is perpendicular to the gas flow and is the pressure that is exerted in all directions. This quasi-static pressure is called the "static pressure" by Nagy [1981, p. 58] to differentiate it from the dynamic pressure, although the "static pressure" does vary with time during the explosion. The dynamic or wind pressure is directional. The total explosion pressure is the sum of the quasi-static pressure and the wind or dynamic pressure. Other instruments such as dynamic pressure sensors, heat flux gauges to measure explosion temperatures, optical probes to measure dust dispersion, and video cameras may be installed at various locations in the LLEM. During the explosion tests, a PC-based National Instruments data acquisition system collected the data from the various instruments at a sampling rate of 1,500 to 5,000 samples per second.

## Legend



Figure 5. Plan view of the Lake Lynn Experimental Mine (LLEM).

The LLEM dust explosion tests, described in this paper, were conducted in D-drift and more recently in a modified single entry section of A-drift. These drifts were isolated from E-drift by means of the explosion-resistant movable bulkhead doors (Figure 5). The tested coal dusts were prepared in the NIOSH coal grinding and pulverizing facilities located at the OMSHR facility at Bruceton. The coal and rock dust particle size data used in the LLEM explosion studies from the mid-1980s through 2008 are presented in Appendix C: Table C-1 and Table C-2, and coal analysis is presented in Table C-3. The size distributions of the limestone from the 1980s and from 2007 are similar, so comparisons of explosion inerting results from these periods are valid. The typical D-drift dust explosion test ignition zone (Figure 6) was located in the first 40-ft (12m ) as measured from the face (closed end). This $10 \%$ methane air zone was ignited by electric matches. In the rock dust inerting tests, the coal dust and limestone rock dust mixture was placed half on roof shelves made of expanded polystyrene and half on the floor as illustrated in Figure 7 and Figure 8 . These roof shelves were suspended $1.5 \mathrm{ft}(0.5 \mathrm{~m})$ from the mine roof on $10-\mathrm{ft}$ (3m ) increments throughout the dust zone. This dust distribution technique, developed through extensive testing at BEM and LLEM, is used to enable reproducibility of experimental conditions. The length of the dust zones during these inerting tests in D-drift varied as follows: $210,270,390,420,450$, and 600 ft long ( $64,82,119,128,137$, and 183 m ). These dust zones started just outby the end of the 40 -ft-long ignition zone, that is, the 210 - ft-long dust zone
extended from 40 to $250 \mathrm{ft}(12 \mathrm{~m}$ to 76 m$)$ as measured from the face. Although the majority of the dust zones were 210 ft long, the longer dust zones were used for several reasons that differed depending on the experiment. The extension of flame travel through and beyond the longer dust zones for a particular incombustible content was always compared to a similar $210-\mathrm{ft}$-long dust zone to verify that the flame propagation was not being overdriven by the methane ignition zone (which would typically travel $\sim 200 \mathrm{ft}$ or $\sim 61 \mathrm{~m}$ from the closed end). Non-propagation is defined as no sustained flame propagation of the dust mixture. Propagation is defined as flame propagation of the dust mixture.

The nominal dust loading reported for the LLEM tests assumes that all of the dust was dispersed uniformly throughout the cross-section. For the LLEM tests, the test drift was thoroughly washed down after each test. Dehumidified air was passed through the entry, and the entry was allowed to dry several days before dust was loaded for the next test.


Figure 6. Side view of LLEM A-drift and D-drift test zones for determining rock dust inerting requirements.


Figure 7. Placing coal and rock dust mixture on shelves in the LLEM.


Figure 8. Distributing test dust mixture at the LLEM.

## Size Data for Intake Airways

For this study, a total of 217 samples of mine dust from intake airways of 61 coal mines in the 10 MSHA bituminous districts were analyzed for particle size. For each mine, samples were usually collected from two or more entries. For most analyses, multiple samples from a mine entry were combined to give an average size distribution for that entry. Most of the samples were band samples, also known as perimeter samples, but some were floor and rib samples, floor and roof samples, or floor-only samples [MSHA, 2008, p. 60]. The detailed size data for each sample and each mine are listed in the tables of Appendix A. The mines are identified only as A, B, C, etc., so that the individual mines remain anonymous. Columns three and four of the tables in Appendix A list the incombustible percentage (from the MSHA Mt. Hope Laboratory) and the soluble in acid percentage, as measured at NIOSH-OMSHR. Columns five and six of the tables list the original size analyses. Column seven lists the weighted average of the ash or incombustible fraction of the acid-leached material. The remaining columns list the corrected size analyses. Table 2 lists the summary intake coal dust size data by the MSHA Coal Mine Safety and Health District. Column two lists the states within each MSHA District from which samples were obtained. There may be additional states within some districts from which there were no samples obtained. Columns three and four of the table list the number of mines and total number of combined samples per district. Columns five through twelve list the average percentage through the various sieves. The column for minus 200 mesh $(75 \mu \mathrm{~m})$ lists both the average value and the associated standard deviation. The standard deviations for the other sieve values are listed in the tables of Appendix A. The last column lists the average and standard deviation for the mass median particle diameter ( $50 \%$ point on the cumulative distribution curve), which was interpolated from the corrected sieving data. The cumulative size data for MSHA Districts 3, 9, and 11 are shown in Figure 9. MSHA District 11 has the finest dust, with $37 \%$ minus 200 mesh, and the western states (District 9) have the coarsest dust, with $27 \%$ minus 200 mesh. District 3 (northern WV, OH, and MD) has an intermediate size. The averages for all MSHA Districts are $31 \%$ minus 200 mesh, $61 \%$ minus 70 mesh, and a mass median particle diameter of $\sim 156 \mu \mathrm{~m}$. This is finer than particles measured in the 1920 s .

Table 2. Average coal sizes from intake airways in mines in 10 MSHA Safety and Health Districts

| District | States | Mines | Samples | $\begin{gathered} -270 \text { mesh } \\ \text { or } \\ <53 \mu \mathrm{~m} \\ \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or } \\ <75 \mu \mathrm{~m} \\ \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or } \\ <106 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or } \\ <150 \mu \mathrm{~m} \\ \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or } \\ <212 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or } \\ <300 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or } \\ <425 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or } \\ <600 \mu \mathrm{~m}, \\ \% \end{gathered}$ | Dmed, $\mu \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | PA | 6 | 20 | 23 | $29 \pm 4$ | 37 | 47 | 59 | 72 | 85 | 95 | $165 \pm 27$ |
| 3 | $\mathrm{OH}, \mathrm{MD}$, <br> No. WV | 7 | 22 | 26 | $33 \pm 9$ | 41 | 51 | 62 | 74 | 87 | 96 | $149 \pm 42$ |
| 4 | So. WV | 7 | 23 | 25 | $30 \pm 6$ | 38 | 48 | 60 | 73 | 87 | 97 | $165 \pm 39$ |
| 5 | VA | 6 | 20 | 25 | $31 \pm 8$ | 40 | 50 | 62 | 74 | 86 | 96 | $157 \pm 36$ |
| 6 | Eastern KY | 5 | 24 | 25 | $31 \pm 7$ | 39 | 49 | 59 | 72 | 85 | 96 | $160 \pm 37$ |
| 7 | Central KY | 5 | 19 | 29 | $34 \pm 10$ | 43 | 53 | 62 | 74 | 86 | 95 | $140 \pm 48$ |
| 8 | IN, IL | 6 | 18 | 24 | $29 \pm 5$ | 37 | 47 | 57 | 71 | 85 | 96 | $170 \pm 31$ |
| 9 | CO, NM, UT | 7 | 20 | 21 | $27 \pm 3$ | 36 | 46 | 57 | 71 | 85 | 96 | $172 \pm 26$ |
| 10 | Western KY | 5 | 28 | 23 | $29 \pm 4$ | 39 | 50 | 61 | 74 | 86 | 96 | $152 \pm 24$ |
| 11 | AL | 7 | 23 | 30 | $37 \pm 10$ | 48 | 60 | 73 | 84 | 92 | 97 | $128 \pm 46$ |
|  | 10 Districts Average |  | 217 | 25 | 31 | 40 | 50 | 61 | 74 | 86 | 96 | 156 |



Figure 9. Coal particle size by MSHA district.

Table 3 lists the average coal dust particle sizes for intake airways for various coal seams or groups of adjacent coal seams. The eastern bituminous coal seams are those in the Appalachian Mountains from Pennsylvania to Alabama. Only the seams that included samples from two or more mines are listed. The coal rank is also listed in the first column, with hvb, mvb, and lvb indicating high, medium, and low volatile bituminous coal, respectively [ASTM 2008]. The mideastern seams are those in Illinois, Indiana, and western Kentucky. These seams are known by different names in different states, as listed in the table. The western coal seams include various high volatile C bituminous (hvCb) coals in Colorado or Utah. The coal samples from the Hazard \#4 seam in Kentucky and the Blue Creek seam in Alabama are the finest, with $40 \%$ of the samples less than 200 mesh. However, the Hazard seam data are based on samples from only two mines and may not represent the area as well as the Blue Creek seam data. The Pittsburgh seam coal in OH, PA, and WV has $32 \%$ minus 200 mesh. The cumulative size data for the Blue Creek, Pittsburgh, and Herrin coal seams are shown in Figure 10.

Table 3. Average coal particle size from intake airways for various coal seams

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



Figure 10. Coal particle size by coal seam.

## Size Data for Return Airways

For this study, a total of 44 samples of mine dust was taken from return airways of 36 coal mines in the 10 MSHA bituminous districts and were analyzed for particle size. Samples were collected from one or more entries in each mine. Similar to the intake airways, multiple samples from a mine entry were combined to give an average size distribution for that entry. Most of the samples were band samples, but some were floor and rib samples, floor and roof samples, or floor-only samples. The detailed size data for the return airways are listed in Table B-1 in Appendix B. For the returns, there was a much larger variation in the coal dust size. Many samples had percentages of minus 200 mesh dust, which were similar to those of the intake samples. However, 8 of the 44 samples had $60 \%$ to more than $80 \%$ minus 200 mesh. The only coal seam for which there were sufficient samples to calculate a representative average size was the Pittsburgh coal seam. The coal samples had an average of $62 \%$ minus 200 mesh (Table B-2 in Appendix B), finer than the intake coal samples from the Pittsburgh seam.

## MSHA Dust Survey Results from Intake and Return Airways

MSHA, from January 2005 to February 2008, collected and determined the TIC for 65,536 intake and 60,663 return airway samples from underground coal mines. Each dust sample represents about $500 \mathrm{ft}(152 \mathrm{~m})$ of mine entry. The intake airways are currently required to contain at least $65 \%$ TIC. Approximately $87 \%$ contained $\geq 65 \%$ TIC, while $\sim 13 \%$ contained $<$ $65 \%$ TIC and thus were non-compliant. The fact that $\sim 13 \%$ of the samples collected were found
to be non-compliant illustrates the scope of the problem. Considering that each sample may represent up to $500 \mathrm{ft}(152 \mathrm{~m})$ of mine entry, these $\sim 13 \%$, or 8,323 samples, represent more than 788 miles ( $1,268 \mathrm{~km}$ ) of underground coal mine entries that were deficient. At the other extreme, $66 \%$ of the intake samples contained more than $80 \%$ TIC, and $\sim 54 \%$ contained more than $85 \%$ TIC. This indicates that rock dusting efforts exceed requirements in a majority of samples, because the average TIC among all samples was $\sim 82 \%$ TIC.

A similar TIC distribution is observed for return airway samples. Current MSHA regulations require $80 \%$ TIC for return airways. Analysis of 60,663 samples revealed that $\sim 72 \%$ of samples contained $\geq 80 \%$ TIC while $\sim 28 \%$ contained $<80 \%$ TIC. The average TIC for return samples was $85 \%$, which is $\sim 3 \%$ higher than the intake average of $\sim 82 \%$.

The MSHA dust survey data indicate that many areas have more than sufficient inert material. However, there are still a large number of areas where rock dusting efforts are insufficient to prevent coal dust explosions.

## Limestone Rock Dust Inerting

Prior to having recent access to the MSHA band samples collected from underground coal mines throughout the United States, there was growing evidence from limited dust surveys that the coal dust particle size had been decreasing since the promulgation of the existing rock dusting regulations. This decrease occurred as new mining technologies were adopted by the industry. Numerous coal dust explosion tests have been conducted in the LLEM to specifically quantify the concentration of rock dust required to prevent propagation of a high volatile coal as a function of coal dust particle size. Table C-4 shows a composite of these experiments. Details of these experiments can be found in Table C-4 in Appendix C along with a discussion highlighting the specific experimental results.


Figure 11. Effect of particle size of coal dust on the explosibility of Pittsburgh seam bituminous coal as tested within LLEM.

Following the coal dust survey, additional large-scale explosion experiments were conducted using medium-sized dust ( $38 \%$ minus 200 mesh or 75 microns-Table C-1) to better define the boundary between explosion propagation and non-propagation. Medium-sized dust was formulated with a blend of 2008 pulverized and 2008 coarse dust (Table C-1) of Pittsburgh seam coal to represent the average of the finer dusts collected from the survey. However, approximately $12 \%$ of the collected intake airway dust samples ( 26 of the 217 samples) ranged in size from 39 to $63 \%$ minus 200 mesh. These finer than medium-sized coal dust samples were collected from mines in 7 of the 10 MSHA Districts and represented approximately $26 \%$ of the overall mines sampled ( 16 of the 61 mines).

The results of the LLEM large-scale explosion tests including the medium-sized coal dust are shown in Figure 11. Given the experimental test conditions, the curve is the boundary between mixtures that did propagate an explosion (below line) and mixtures that did not propagate an explosion (above line). The coal dust particle size has a substantial impact on the propagation potential for coal dust. As the coal dust particle size decreases, increasing amounts of rock dust are necessary to render the coal/rock dust mixture inert. The greatest impact is evident between the particle size of the coarse ( $20 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ) coal dust and the pulverized ( $80 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ) coal dust. To ensure non-propagation within the LLEM, the coarse coal dust required at least $70 \% \mathrm{TIC}$ and the pulverized coal dust required greater than a $79 \%$ TIC and less than a $81.5 \%$ TIC. Once the $80 \%$ minus 200 mesh benchmark had been reached, no additional TIC was required to prevent flame propagation with further decrease in coal dust particle size. One can clearly see when comparing Figure 1 with the earlier BEM data to Figure 11 of the recent LLEM data that the TIC increases from about $60 \%$ to $70 \%$ TIC at the coarse coal particle size end of the figures, while TIC remains at about $80 \%$ at the fine coal particle size end of both figures.

The $80 \%$ limit is also consistent with explosion temperature thermodynamic limit models for coal and rock dust put forward by Richmond et al. [1975; 1979], Hertzberg et al. [1988], Conti et al. [1991], and Sapko et al. [2000]. The models were essentially based on a thermal balance between the heat generated during the combustion of coal dust and heat absorbed by the incombustible material.

LLEM inerting studies using a medium-sized coal dust showed that at least 76.4\% TIC (Table C-4) is required to prevent explosion propagation. If one considers the finest size intake air way dust collected during the recent survey ( $63 \%$ minus 200 mesh from Table A-2), data in Figure 11 indicates that approximately $80 \%$ TIC would be required to prevent explosion propagation.

## Summary

Dust explosibility is strongly dependent on the size distribution of the coal particles in a coal and rock dust mixture. Underground coal mining technology has changed since the 1920s; that is, coal mining has become highly mechanized, creating coal dust with more small size fractions than those of the 1920s. Despite this change in technology, particle size surveys from the early 1900s are still being used as the basis for current rock dusting regulations. Although total incombustible content is an important determinant of explosion propagation, coal dust particle size also needs to be considered as an essential part of an explosibility assessment in underground coal mines. The present coal size study indicates that the coal dust in intake airways of U.S. mines is finer than that measured by Rice and Greenwald [1929] in the 1920s. Moreover, particle size distributions can vary with coal seam and rank, as shown in Table 2. Current rock dust regulations mandating a $65 \%$ TIC dust mixture do not fully protect miners since LLEM tests have shown that even a $\sim 68 \%$ TIC dust mixture with coarse Pittsburgh seam coal dust ( $20 \%$ minus 200 mesh) will propagate dust explosions. LLEM inerting experiments also demonstrated that at least $76.4 \%$ TIC is required to prevent explosion propagation for medium-sized coal dust ( $38 \%$ minus 200 mesh ) - that is, an average of the finer dust found in modern intake areas. For return airways, the current requirement of at least $80 \%$ TIC is still sufficient in the absence of methane.

LLEM experiments for high volatile coals have also shown that the TIC required to prevent flame propagation becomes much less dependent on coal particle size as the TIC approaches and exceeds $80 \%$. Therefore, experimental results support at least an $80 \%$ TIC requirement for both intake and return airways in the absence of methane.

## Recommendation

Large-scale explosion testing in the Bruceton and Lake Lynn Experimental Mines confirm intake airways require more incombustible content to render the coal dust inert than the $65 \%$ TIC specified in current regulations.

NIOSH recommends an 80\% TIC in intake airways based on:

- Explosion temperature thermodynamic limit models for coal and rock dust mixtures,
- Extensive in-mine coal dust particle size surveys, and
- Multiple explosion experiments at the Lake Lynn Laboratory.


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## Appendix A:

## Analyses of Size of Coal Dust Particles

 from Mine Intake AirwaysTable A-1. Analyses of size of coal dust particles from intake airways in six MSHA District 2 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | Ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \mu \mathrm{~m}, \\ \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -140 \mathrm{mesh} \\ \text { or }<106 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh or } \\ <212 \mu \mathrm{~m} \\ \% \end{gathered}$ | $\begin{aligned} & -50 \text { mesh or } \\ & <300 \mu \mathrm{~m}, \\ & \% \end{aligned}$ | $\begin{gathered} -40 \text { mesh or } \\ <425 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh or } \\ <600 \mu \mathrm{~m}, \\ \% \end{gathered}$ | $\begin{gathered} D_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 74 | 55 | 35 | 64 | 40 | 21 | 25 | 33 | 44 | 56 | 69 | 83 | 92 | 178 |
|  |  | 81 | 73 | 43 | 70 | 42 | 27 | 34 | 44 | 53 | 64 | 76 | 89 | 97 | 136 |
| B | >1 | 54 | 52 | 38 | 71 | 22 | 25 | 32 | 43 | 55 | 68 | 80 | 91 | 97 | 130 |
|  |  | 60 | 42 | 31 | 61 | 27 | 19 | 25 | 35 | 45 | 57 | 70 | 84 | 95 | 173 |
|  |  | 82 | 69 | 41 | 72 | 40 | 25 | 31 | 41 | 52 | 64 | 76 | 89 | 97 | 143 |
|  |  | 56 | 24 | 37 | 60 | 37 | 25 | 29 | 36 | 45 | 55 | 67 | 82 | 94 | 180 |
|  |  | 72 | 61 | 33 | 59 | 30 | 22 | 27 | 34 | 44 | 54 | 67 | 82 | 94 | 186 |
|  |  | 85 | 40 | 48 | 79 | 73 | 22 | 31 | 40 | 50 | 60 | 77 | 89 | 97 | 151 |
| C | >1 | 86 | 58 | 31 | 62 | 23 | 21 | 26 | 35 | 44 | 57 | 72 | 85 | 95 | 176 |
|  |  | 88 | 79 | 46 | 74 | 46 | 26 | 32 | 43 | 55 | 67 | 77 | 87 | 95 | 130 |
|  |  | 75 | 48 | 35 | 62 | 47 | 23 | 27 | 35 | 44 | 57 | 70 | 86 | 97 | 177 |
|  |  | 64 | 30 | 27 | 50 | 49 | 18 | 21 | 27 | 35 | 46 | 60 | 79 | 94 | 237 |
| D | >1 | 70 | 51 | 39 | 65 | 36 | 23 | 30 | 36 | 44 | 55 | 68 | 82 | 93 | 184 |
|  |  | 93 | 85 | 35 | 71 | 39 | 23 | 28 | 38 | 50 | 63 | 73 | 84 | 94 | 150 |
|  |  | 67 | 42 | 34 | 59 | 38 | 24 | 28 | 34 | 44 | 55 | 70 | 85 | 96 | 182 |
|  |  | 50 | 24 | 46 | 71 | 30 | 33 | 38 | 44 | 54 | 66 | 78 | 90 | 98 | 130 |
| E | <1 | 75 | 66 | 38 | 64 | 21 | 30 | 36 | 43 | 53 | 63 | 73 | 84 | 95 | 135 |
| F | <1 | 90 | 57 | 30 | 65 | 70 | 17 | 24 | 33 | 43 | 55 | 69 | 80 | 90 | 186 |
|  |  | 90 | 73 | 28 | 61 | 58 | 15 | 22 | 31 | 41 | 54 | 70 | 86 | 96 | 191 |
|  |  | 88 | 69 | 39 | 66 | 58 | 23 | 31 | 38 | 48 | 58 | 71 | 85 | 96 | 159 |
|  |  |  |  | average for MSHA District 2 standard deviation |  |  | 23 | 29 | 37 | 47 | 59 | 72 | 85 | 95 | 165 |
|  |  |  |  |  |  |  | 4 | 4 | 5 | 5 | 5 | 5 | 3 | 2 | 27 |

## Notes:

The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-2. Analyses of size of coal dust particles from intake airways in seven MSHA District 3 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 55 | 27 | 29 | 61 | 21 | 20 | 27 | 35 | 46 | 60 | 75 | 90 | 98 | 165 |
| B | >1 | 68 | 47 | 41 | 68 | 37 | 26 | 30 | 37 | 47 | 59 | 74 | 88 | 97 | 164 |
|  |  | 70 | 44 | 31 | 61 | 46 | 17 | 22 | 30 | 40 | 53 | 70 | 86 | 97 | 199 |
| C | >1 | 82 | 57 | 39 | 66 | 56 | 24 | 31 | 38 | 47 | 57 | 71 | 86 | 96 | 169 |
|  |  | 97 | 96 | 42 | 71 | 35 | 28 | 38 | 48 | 58 | 70 | 75 | 85 | 93 | 113 |
|  |  | 95 | 95 | 67 | 84 | 25 | 52 | 63 | 71 | 77 | 81 | 86 | 93 | 98 | 50 |
|  |  | 90 | 81 | 47 | 77 | 44 | 28 | 36 | 45 | 57 | 66 | 78 | 89 | 97 | 123 |
|  |  | 87 | 73 | 51 | 77 | 55 | 26 | 32 | 39 | 49 | 56 | 69 | 82 | 94 | 160 |
|  |  | 86 | 72 | 37 | 71 | 47 | 23 | 32 | 41 | 52 | 63 | 78 | 91 | 98 | 141 |
|  |  | 88 | 77 | 45 | 74 | 47 | 32 | 40 | 46 | 54 | 63 | 77 | 89 | 97 | 125 |
| D | >1 | 83 | 81 | 45 | 76 | 20 | 32 | 39 | 49 | 61 | 72 | 82 | 91 | 97 | 108 |
|  |  | 77 | 68 | 52 | 82 | 23 | 38 | 45 | 55 | 66 | 78 | 88 | 94 | 98 | 89 |
|  |  | 91 | 74 | 40 | 72 | 55 | 20 | 25 | 35 | 47 | 59 | 73 | 87 | 95 | 164 |
|  |  | 72 | 55 | 42 | 67 | 30 | 27 | 32 | 39 | 49 | 60 | 72 | 86 | 96 | 156 |
|  |  | 46 | 11 | 37 | 62 | 33 | 24 | 29 | 36 | 45 | 56 | 69 | 84 | 96 | 175 |
|  |  | 41 | 10 | 34 | 62 | 32 | 23 | 28 | 36 | 46 | 57 | 71 | 87 | 97 | 171 |
| E | >1 | 80 | 59 | 46 | 82 | 44 | 27 | 34 | 46 | 60 | 74 | 86 | 95 | 99 | 117 |
|  |  | 79 | 63 | 32 | 66 | 33 | 20 | 26 | 35 | 47 | 62 | 75 | 86 | 93 | 161 |
| F | >1 | 83 | 75 | 43 | 75 | 40 | 25 | 32 | 43 | 54 | 66 | 78 | 89 | 97 | 134 |
|  |  | 75 | 67 | 43 | 69 | 50 | 25 | 31 | 41 | 49 | 60 | 70 | 83 | 94 | 155 |
| G | >1 | 58 | 39 | 29 | 55 | 23 | 21 | 28 | 34 | 43 | 54 | 65 | 79 | 92 | 189 |
|  |  | 72 | 63 | 20 | 44 | 19 | 13 | 18 | 24 | 32 | 42 | 56 | 75 | 92 | 259 |
|  |  |  |  | average for MSHA District 3 standard deviation |  |  | $26$ | $33$ | $41$ | $51$ | $62$ | $74$ | $87$ | $96$ | $149$ |
|  |  |  |  |  |  |  | $8$ | $9$ | $10$ | $10$ | $9$ | $7$ | 5 | 2 | $42$ |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-3. Analyses of size of coal dust particles from intake airways in seven MSHA District 4 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med, }} \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 65 | 51 | 42 | 70 | 30 | 26 | 34 | 44 | 54 | 64 | 75 | 86 | 96 | 131 |
|  |  | 68 | 54 | 36 | 59 | 26 | 22 | 28 | 35 | 43 | 52 | 65 | 80 | 94 | 195 |
|  |  | 64 | 35 | 45 | 69 | 43 | 29 | 36 | 44 | 54 | 64 | 75 | 87 | 97 | 133 |
|  |  | 70 | 61 | 33 | 63 | 25 | 22 | 29 | 37 | 48 | 61 | 73 | 87 | 97 | 160 |
|  |  | 89 | 83 | 52 | 80 | 35 | 34 | 41 | 50 | 62 | 74 | 85 | 95 | 99 | 106 |
|  |  | 85 | 81 | 43 | 68 | 25 | 29 | 35 | 42 | 52 | 64 | 77 | 90 | 98 | 138 |
| B | <1 | 82 | 40 | 40 | 63 | 61 | 24 | 30 | 36 | 45 | 55 | 68 | 82 | 94 | 181 |
|  |  | 75 | - | 37 | 65 | 65 | 23 | 28 | 36 | 45 | 56 | 70 | 85 | 96 | 176 |
| C | <1 | 68 | 18 | 30 | 54 | 59 | 21 | 25 | 32 | 41 | 52 | 65 | 82 | 96 | 199 |
|  |  | 70 | 15 | 38 | 59 | 61 | 25 | 28 | 35 | 43 | 53 | 66 | 81 | 95 | 192 |
|  |  | 69 | 21 | 32 | 56 | 57 | 18 | 22 | 27 | 36 | 47 | 61 | 79 | 94 | 231 |
|  |  | 81 | 35 | 34 | 60 | 70 | 20 | 25 | 33 | 42 | 53 | 69 | 85 | 97 | 196 |
|  |  | 78 | 33 | 38 | 60 | 68 | 26 | 29 | 35 | 44 | 56 | 67 | 83 | 96 | 179 |
| D | <1 | 79 | 38 | 38 | 60 | 63 | 24 | 28 | 34 | 44 | 54 | 66 | 82 | 95 | 186 |
| E | <1 | 47 | 9 | 47 | 82 | 37 | 29 | 36 | 47 | 61 | 75 | 88 | 95 | 99 | 114 |
|  |  | 57 | 30 | 25 | 54 | 29 | 16 | 21 | 28 | 37 | 48 | 63 | 79 | 94 | 224 |
|  |  | 37 | 3 | 32 | 59 | 27 | 20 | 25 | 33 | 43 | 54 | 67 | 81 | 94 | 188 |
|  |  | 53 | 18 | 24 | 59 | 40 | 12 | 16 | 23 | 33 | 48 | 68 | 86 | 97 | 221 |
| F | >1 | 77 | 58 | 45 | 71 | 48 | 31 | 36 | 44 | 55 | 65 | 78 | 91 | 98 | 129 |
|  |  | 87 | 73 | 44 | 70 | 52 | 29 | 34 | 43 | 53 | 63 | 77 | 91 | 98 | 137 |
| G | <1 | 40 | 23 | 45 | 84 | 23 | 35 | 43 | 53 | 67 | 83 | 93 | 97 | 99 | 98 |
|  |  | 37 | 16 | 43 | 75 | 22 | 29 | 36 | 45 | 57 | 71 | 85 | 95 | 99 | 123 |
|  |  | 49 | - | 33 | 69 | 29 | 24 | 30 | 39 | 51 | 67 | 83 | 93 | 98 | 147 |
|  |  |  |  | average for MSHA District 4 standard deviation |  |  | 25 | 30 | 38 | 48 | 60 | 73 | 87 | 97 | 165 |
|  |  |  |  |  |  |  | 6 | 6 | 7 | 9 | 10 | 9 | 6 | 2 | 39 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-4. Analyses of size of coal dust particles from intake airways in six MSHA District 5 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -70 mesh or < 212 $\mu \mathrm{m}, \%$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | $<1$ | 64 | 43 | 32 | 58 | 34 | 25 | 31 | 39 | 49 | 60 | 72 | 84 | 95 | 156 |
|  |  | 57 | 28 | 26 | 52 | 44 | 23 | 29 | 36 | 45 | 57 | 68 | 82 | 94 | 173 |
|  |  | 68 | 60 | 38 | 61 | 32 | 28 | 34 | 41 | 50 | 59 | 71 | 85 | 96 | 150 |
| B | >1 | 66 | 57 | 47 | 72 | 30 | 27 | 30 | 39 | 49 | 61 | 73 | 86 | 96 | 154 |
|  |  | 63 | 63 | 52 | 78 | 20 | 40 | 47 | 55 | 65 | 75 | 83 | 92 | 98 | 87 |
|  |  | 87 | 85 | 31 | 56 | 39 | 18 | 26 | 33 | 42 | 51 | 64 | 81 | 94 | 203 |
|  |  | 48 | 43 | 37 | 62 | 26 | 24 | 31 | 39 | 50 | 60 | 72 | 85 | 95 | 151 |
|  |  | 35 | 24 | 23 | 48 | 26 | 16 | 21 | 27 | 37 | 47 | 61 | 78 | 92 | 227 |
|  |  | 65 | 56 | 36 | 62 | 32 | 27 | 33 | 40 | 51 | 62 | 75 | 88 | 97 | 145 |
| C | <1 | 83 | 73 | 60 | 94 | 29 | 40 | 54 | 70 | 86 | 93 | 96 | 98 | 99 | 68 |
|  |  | 69 | 54 | 38 | 77 | 28 | 26 | 32 | 42 | 56 | 75 | 88 | 95 | 98 | 132 |
|  |  | 78 | 61 | 44 | 83 | 32 | 30 | 36 | 48 | 64 | 80 | 90 | 95 | 98 | 110 |
| D | <1 | 52 | 29 | 33 | 59 | 31 | 21 | 28 | 35 | 45 | 56 | 69 | 83 | 95 | 176 |
|  |  | 57 | 28 | 34 | 62 | 34 | 21 | 27 | 34 | 45 | 57 | 70 | 84 | 96 | 175 |
| E | >1 | 82 | 76 | 35 | 62 | 27 | 23 | 29 | 36 | 46 | 57 | 68 | 81 | 93 | 173 |
|  |  | 72 | 58 | 32 | 65 | 21 | 22 | 28 | 36 | 46 | 62 | 76 | 89 | 98 | 164 |
|  |  | 67 | 52 | 26 | 62 | 25 | 21 | 22 | 36 | 45 | 58 | 70 | 84 | 96 | 172 |
| F | $<1$ | 77 | 58 | 38 | 61 | 43 | 27 | 32 | 38 | 47 | 58 | 69 | 84 | 96 | 166 |
|  |  | 80 | 67 | 35 | 60 | 43 | 25 | 30 | 37 | 46 | 57 | 69 | 83 | 96 | 170 |
|  |  | 76 | 63 | 30 | 58 | 33 | 16 | 26 | 34 | 44 | 55 | 67 | 81 | 94 | 183 |
|  |  |  |  | average for MSHA District 5 standard deviation |  |  | $25$ | $31$ | $40$ | $50$ | $62$ | $74$ | $86$ | $96$ | $157$ |
|  |  |  |  |  |  |  | $6$ | $8$ | $9$ | $11$ | $11$ | 9 | $5$ | 2 | 36 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR. The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-5. Analyses of size of coal dust particles from intake airways in five MSHA District 6 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, <br> \% | Size analysis |  | ash, \% |  |  |  | Correcte | size analys |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -70 mesh or < 212 $\mu \mathrm{m}, \%$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -40 mesh or $<425$ $\mu \mathrm{m}, \%$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 63 | 31 | 37 | 64 | 41 | 20 | 25 | 33 | 42 | 53 | 66 | 83 | 96 | 195 |
|  |  | 54 | 26 | 38 | 61 | 35 | 23 | 28 | 35 | 43 | 54 | 66 | 81 | 95 | 188 |
|  |  | 51 | 14 | 33 | 58 | 45 | 21 | 26 | 33 | 42 | 53 | 66 | 82 | 95 | 193 |
| B | $<1$ | 36 | 17 | 28 | 56 | 18 | 19 | 25 | 31 | 41 | 52 | 65 | 82 | 96 | 200 |
|  |  | 40 | 22 | 28 | 56 | 20 | 18 | 23 | 29 | 37 | 50 | 65 | 82 | 96 | 214 |
|  |  | 37 | 20 | 38 | 63 | 17 | 27 | 33 | 40 | 48 | 58 | 69 | 82 | 94 | 164 |
|  |  | 35 | 21 | 40 | 64 | 17 | 29 | 35 | 42 | 50 | 60 | 71 | 85 | 96 | 150 |
|  |  | 35 | 19 | 35 | 62 | 18 | 23 | 29 | 36 | 46 | 57 | 70 | 83 | 94 | 173 |
|  |  | 37 | 20 | 38 | 64 | 19 | 27 | 32 | 39 | 48 | 58 | 72 | 87 | 97 | 160 |
|  |  | 73 | 60 | 42 | 70 | 27 | 27 | 33 | 41 | 51 | 62 | 75 | 87 | 96 | 145 |
| C | >1 | 77 | 50 | 30 | 55 | 56 | 17 | 22 | 28 | 37 | 48 | 64 | 81 | 95 | 220 |
|  |  | 73 | 20 | 42 | 65 | 65 | 28 | 32 | 39 | 50 | 61 | 73 | 86 | 97 | 150 |
|  |  | 73 | 24 | 35 | 59 | 64 | 18 | 24 | 30 | 39 | 49 | 64 | 81 | 96 | 215 |
| D | >1 | 76 | 25 | 46 | 82 | 67 | 25 | 29 | 38 | 51 | 63 | 77 | 89 | 97 | 145 |
|  |  | 76 | 29 | 47 | 72 | 69 | 27 | 34 | 45 | 56 | 64 | 73 | 85 | 97 | 124 |
|  |  | 74 | 21 | 42 | 75 | 67 | 22 | 30 | 38 | 48 | 61 | 78 | 89 | 97 | 161 |
|  |  | 71 | 17 | 50 | 77 | 65 | 28 | 33 | 41 | 52 | 62 | 74 | 84 | 95 | 142 |
|  |  | 72 | 12 | 52 | 83 | 67 | 29 | 34 | 45 | 59 | 69 | 79 | 87 | 96 | 120 |
| E | <1 | 84 | 81 | 60 | 79 | 30 | 45 | 55 | 63 | 70 | 77 | 83 | 92 | 98 | 64 |
|  |  | 84 | 75 | 50 | 79 | 34 | 34 | 42 | 51 | 62 | 71 | 81 | 90 | 97 | 102 |
|  |  | 64 | 47 | 40 | 64 | 26 | 29 | 34 | 41 | 50 | 59 | 70 | 84 | 96 | 151 |
|  |  | 86 | 77 | 36 | 69 | 42 | 23 | 29 | 37 | 49 | 61 | 75 | 88 | 97 | 155 |
|  |  | $56$ | $41$ | 37 | 67 | 21 | 26 | 32 | 39 | 50 | 62 | 77 | 90 | 98 | 150 |
|  |  | 56 | 41 | 36 | 62 | 23 | 26 | 32 | 39 | 48 | 59 | 71 | 85 | 96 | 162 |
|  |  |  |  | average for MSHA District 6 standard deviation |  |  | 25 | 31 | 39 | 49 | 59 | 72 | 85 | 96 | 160 |
|  |  |  |  |  |  |  | 6 | 7 | 8 | 8 | 7 | 6 | 3 | 1 | 37 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-6. Analyses of size of coal dust particles from intake airways in five MSHA District 7 mines

| Mine | Production, Mt/yr | Incombustible,$\%$ | Soluble, <br> \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\mathrm{med}}, \\ \mu \mathrm{~m} \end{gathered}$ |
| A | <1 | 79 | 65 | 41 | 67 | 51 | 23 | 29 | 37 | 46 | 55 | 68 | 82 | 95 | 175 |
|  |  | 79 | 65 | 44 | 74 | 50 | 24 | 29 | 39 | 51 | 60 | 74 | 87 | 96 | 147 |
|  |  | 81 | 62 | 41 | 68 | 52 | 22 | 29 | 38 | 48 | 58 | 72 | 85 | 96 | 164 |
|  |  | 78 | 60 | 37 | 65 | 46 | 21 | 27 | 35 | 45 | 55 | 69 | 84 | 95 | 179 |
| B | $<1$ | 92 | 80 | 62 | 78 | 63 | 52 | 56 | 63 | 69 | 75 | 80 | 84 | 90 | 46 |
|  |  | 92 | 83 | 66 | 82 | 63 | 49 | 54 | 62 | 69 | 76 | 82 | 88 | 94 | 59 |
|  |  | 92 | 78 | 63 | 83 | 62 | 48 | 54 | 61 | 69 | 78 | 82 | 88 | 94 | 60 |
| C | $<1$ | 89 | 62 | 44 | 77 | 65 | 20 | 27 | 37 | 50 | 61 | 74 | 87 | 97 | 149 |
|  |  | 87 | 66 | 55 | 83 | 59 | 29 | 37 | 47 | 59 | 71 | 84 | 93 | 98 | 117 |
|  |  | 96 | 87 | 45 | 74 | 74 | 24 | 28 | 37 | 52 | 63 | 72 | 85 | 95 | 143 |
|  |  | 90 | 78 | 59 | 86 | 61 | 29 | 36 | 43 | 58 | 69 | 81 | 90 | 97 | 124 |
|  |  | 91 | 78 | 45 | 70 | 59 | 22 | 29 | 42 | 51 | 59 | 71 | 85 | 96 | 144 |
| D | $<1$ | 61 | 24 | 39 | 64 | 49 | 22 | 27 | 35 | 45 | 55 | 69 | 84 | 95 | 179 |
|  |  | 74 | 28 | 36 | 63 | 60 | 20 | 26 | 33 | 42 | 53 | 67 | 82 | 95 | 195 |
|  |  | 77 | 38 | 38 | 66 | 58 | 19 | 25 | 32 | 40 | 52 | 66 | 82 | 95 | 200 |
| E | <1 | 88 | 69 | 59 | 85 | 59 | 31 | 35 | 47 | 58 | 67 | 78 | 88 | 96 | 117 |
|  |  | 91 | 74 | 64 | 83 | 62 | 36 | 41 | 49 | 58 | 66 | 76 | 87 | 96 | 110 |
|  |  | 82 | 70 | 34 | 61 | 39 | 19 | 23 | 29 | 39 | 49 | 65 | 81 | 94 | 215 |
|  |  | 84 | 64 | 57 | 75 | 53 | 33 | 37 | 44 | 53 | 62 | 74 | 86 | 96 | 136 |
|  |  |  |  | average for MSHA District 7 standard deviation |  |  | 29 | 34 | 43 | 53 | 62 | 74 | 86 | 95 | 140 |
|  |  |  |  |  |  |  | 10 | 10 | 10 | 9 | 8 | 6 | 3 | 2 | 48 |

[^2]Table A-7. Analyses of size of coal dust particles from intake airways in six MSHA District 8 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, <br> \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -40 mesh or $<425$ $\mu \mathrm{m}, \%$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 92 | 81 | 27 | 54 | 64 | 14 | 18 | 25 | 35 | 47 | 59 | 76 | 92 | 234 |
|  |  | 97 | 93 | 38 | 66 | 52 | 21 | 27 | 37 | 48 | 60 | 70 | 83 | 95 | 160 |
| B | >1 | 82 | 49 | 49 | 69 | 51 | 23 | 27 | 34 | 42 | 51 | 64 | 80 | 94 | 208 |
|  |  | 81 | 49 | 53 | 77 | 57 | 24 | 29 | 39 | 48 | 58 | 70 | 83 | 95 | 161 |
| C | >1 | 75 | 45 | 42 | 71 | 46 | 24 | 27 | 35 | 45 | 58 | 73 | 86 | 97 | 171 |
|  |  | 68 | 30 | 43 | 79 | 56 | 22 | 27 | 38 | 51 | 65 | 78 | 91 | 98 | 145 |
| D | >1 | 67 | 32 | 50 | 68 | 46 | 29 | 33 | 39 | 47 | 57 | 68 | 84 | 96 | 167 |
|  |  | 78 | 57 | 53 | 74 | 46 | 33 | 38 | 45 | 54 | 65 | 77 | 90 | 98 | 130 |
|  |  | 65 | 21 | 41 | 63 | 51 | 20 | 26 | 33 | 41 | 52 | 68 | 84 | 96 | 198 |
|  |  | 68 | 33 | 46 | 69 | 45 | 25 | 30 | 39 | 48 | 58 | 70 | 84 | 95 | 162 |
| E | >1 | 84 | 19 | 47 | 73 | 77 | 26 | 30 | 37 | 49 | 59 | 73 | 89 | 98 | 156 |
|  |  | 82 | 23 | 41 | 66 | 75 | 25 | 30 | 36 | 46 | 56 | 71 | 86 | 97 | 175 |
|  |  | 76 | 22 | 43 | 67 | 66 | 25 | 29 | 36 | 46 | 57 | 69 | 85 | 96 | 172 |
|  |  | 79 | 23 | 49 | 70 | 68 | 27 | 30 | 37 | 46 | 55 | 68 | 83 | 96 | 178 |
| F | >1 | 86 | 63 | 55 | 80 | 63 | 30 | 33 | 43 | 54 | 65 | 78 | 89 | 96 | 132 |
|  |  | 73 | 43 | 50 | 74 | 43 | 27 | 32 | 41 | 50 | 60 | 72 | 85 | 95 | 149 |
|  |  | 88 | 63 | 54 | 83 | 57 | 24 | 30 | 44 | 56 | 67 | 81 | 92 | 98 | 127 |
|  |  | 67 | 25 | 36 | 61 | 44 | 15 | 17 | 24 | 34 | 47 | 62 | 80 | 95 | 230 |
|  |  |  |  | average for MSHA District 8 standard deviation |  |  | 24 | 29 | 37 | 47 | 57 | 71 | 85 | 96 | 170 |
|  |  |  |  |  |  |  | 5 | 5 | 5 | 6 | 6 | 6 | 4 | 2 | 31 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-8. Analyses of size of coal dust particles from intake airways in seven MSHA District 9 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 84 | 74 | 42 | 71 | 48 | 21 | 28 | 36 | 47 | 56 | 69 | 83 | 94 | 170 |
|  |  | 59 | 27 | 35 | 62 | 40 | 19 | 26 | 34 | 44 | 54 | 67 | 82 | 94 | 187 |
|  |  | 88 | 77 | 39 | 71 | 49 | 23 | 31 | 40 | 51 | 61 | 75 | 88 | 97 | 147 |
|  |  | 81 | 65 | 44 | 70 | 44 | 27 | 33 | 42 | 53 | 61 | 74 | 87 | 96 | 135 |
| B | >1 | 83 | 70 | 32 | 62 | 26 | 19 | 26 | 34 | 45 | 56 | 70 | 85 | 97 | 176 |
| C | $>1$ | 92 | 85 | 46 | 74 | 45 | 23 | 30 | 42 | 52 | 61 | 74 | 87 | 97 | 139 |
|  |  | 60 | 53 | 35 | 63 | 25 | 20 | 26 | 34 | 44 | 57 | 71 | 87 | 97 | 178 |
|  |  | 71 | 53 | 45 | 71 | 38 | 25 | 31 | 41 | 51 | 63 | 75 | 89 | 97 | 146 |
|  |  | 53 | 25 | 42 | 66 | 33 | 24 | 28 | 36 | 46 | 56 | 70 | 84 | 95 | 173 |
|  |  | 85 | 81 | 40 | 68 | 39 | 21 | 27 | 39 | 49 | 59 | 72 | 86 | 96 | 153 |
| D | >1 | 81 | 87 | 34 | 63 | 36 | 16 | 22 | 30 | 40 | 49 | 62 | 77 | 92 | 220 |
|  |  | 78 | 72 | 37 | 64 | 22 | 23 | 30 | 37 | 47 | 58 | 70 | 84 | 95 | 166 |
|  |  | 78 | 72 | 38 | 70 | 21 | 25 | 31 | 41 | 52 | 64 | 78 | 90 | 98 | 141 |
|  |  | 82 | 77 | 33 | 61 | 23 | 20 | 26 | 33 | 43 | 54 | 66 | 82 | 95 | 190 |
| E | >1 | 76 | 68 | 35 | 61 | 15 | 25 | 30 | 37 | 46 | 57 | 68 | 83 | 94 | 172 |
|  |  | 53 | 53 | 25 | 50 | 12 | 17 | 21 | 28 | 36 | 47 | 60 | 78 | 93 | 232 |
| F | <1 | 40 | 31 | 26 | 55 | 9 | 17 | 24 | 31 | 41 | 53 | 68 | 84 | 95 | 196 |
|  |  | 56 | 49 | 30 | 63 | 11 | 20 | 28 | 36 | 48 | 61 | 75 | 90 | 99 | 159 |
|  |  | 47 | 34 | 29 | 59 | 10 | 20 | 27 | 34 | 44 | 56 | 70 | 86 | 97 | 179 |
| G | $<1$ | 54 | 55 | 26 | 64 | 12 | 16 | 21 | 30 | 43 | 60 | 79 | 92 | 98 | 174 |
|  |  |  |  | average for MSHA District 9 standard deviation |  |  | 21 | 27 | 36 | 46 | 57 | 71 | 85 | 96 | 172 |
|  |  |  |  |  |  |  | 3 | 3 | 4 | 4 | 4 | 5 | 4 | 2 | 26 |

[^3]Table A-9. Analyses of size of coal dust particles from intake airways in five MSHA District 10 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -40 mesh or < 425 $\mu \mathrm{m}, \%$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med },} \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 67 | 49 | 42 | 73 | 41 | 25 | 30 | 39 | 50 | 62 | 77 | 90 | 98 | 148 |
|  |  | 89 | 76 | 44 | 80 | 47 | 26 | 31 | 43 | 57 | 70 | 83 | 94 | 99 | 126 |
|  |  | 72 | na | 42 | 73 | 41 | 23 | 29 | 39 | 50 | 59 | 71 | 84 | 95 | 147 |
|  |  | 62 | 39 | 43 | 69 | 35 | 26 | 31 | 40 | 49 | 58 | 71 | 85 | 95 | 154 |
|  |  | 74 | 52 | 41 | 72 | 44 | 23 | 27 | 37 | 48 | 58 | 74 | 88 | 96 | 161 |
|  |  | 67 | 57 | 37 | 71 | 35 | 23 | 28 | 38 | 50 | 62 | 74 | 86 | 96 | 150 |
|  |  | 89 | 82 | 52 | 82 | 41 | 29 | 41 | 56 | 66 | 75 | 85 | 94 | 99 | 93 |
|  |  | 58 | 27 | 42 | 78 | 43 | 25 | 31 | 41 | 54 | 66 | 80 | 91 | 98 | 135 |
|  |  | 56 | 32 | 50 | 81 | 40 | 14 | 22 | 37 | 52 | 65 | 79 | 90 | 97 | 144 |
|  |  | 66 | 34 | 45 | 72 | 49 | 23 | 27 | 35 | 45 | 52 | 65 | 80 | 93 | 195 |
| B | >1 | 86 | 74 | 37 | 71 | 41 | 21 | 27 | 36 | 48 | 60 | 73 | 85 | 94 | 159 |
|  |  | 85 | 75 | 35 | 67 | 37 | 22 | 27 | 37 | 49 | 61 | 72 | 85 | 96 | 154 |
|  |  | 84 | 72 | 37 | 71 | 35 | 25 | 30 | 41 | 51 | 62 | 75 | 87 | 96 | 145 |
|  |  | 89 | 80 | 35 | 71 | 37 | 21 | 26 | 36 | 48 | 61 | 76 | 87 | 96 | 159 |
|  |  | 87 | 78 | 36 | 69 | 29 | 22 | 27 | 37 | 48 | 60 | 73 | 86 | 96 | 159 |
|  |  | 82 | 68 | 31 | 67 | 37 | 18 | 24 | 32 | 43 | 55 | 69 | 83 | 94 | 184 |
| C | >1 | 75 | 52 | 35 | 63 | 38 | 21 | 26 | 33 | 43 | 53 | 66 | 81 | 94 | 196 |
|  |  | 83 | 67 | 47 | 76 | 42 | 26 | 31 | 41 | 53 | 64 | 75 | 86 | 96 | 137 |
|  |  | 89 | 77 | 54 | 80 | 45 | 27 | 38 | 52 | 60 | 67 | 77 | 87 | 96 | 100 |
|  |  | 68 | 34 | 43 | 77 | 44 | 25 | 32 | 43 | 55 | 66 | 78 | 88 | 96 | 129 |
|  |  | 79 | 47 | 33 | 70 | 56 | 17 | 24 | 32 | 43 | 53 | 68 | 81 | 94 | 195 |
|  |  | 92 | 78 | 44 | 78 | 54 | 23 | 30 | 40 | 52 | 62 | 75 | 88 | 97 | 140 |
| D | >1 | 86 | 74 | 36 | 67 | 42 | 22 | 28 | 38 | 49 | 59 | 71 | 83 | 92 | 156 |
|  |  | 75 | 59 | 37 | 68 | 37 | 21 | 28 | 39 | 48 | 59 | 72 | 85 | 96 | 159 |
|  |  | 86 | 70 | 34 | 70 | 42 | 19 | 25 | 38 | 49 | 59 | 72 | 87 | 96 | 153 |
|  |  | 83 | 64 | 39 | 73 | 45 | 21 | 28 | 40 | 51 | 62 | 76 | 88 | 96 | 145 |
| E | >1 | 75 | 51 | 48 | 71 | 51 | 27 | 31 | 38 | 47 | 57 | 69 | 82 | 94 | 168 |
|  |  | 71 | 42 | 46 | 69 | 43 | 27 | 30 | 37 | 46 | 56 | 70 | 83 | 94 | 171 |
|  |  |  |  | average for MSHA District 10 standard deviation |  |  | 23 | 29 | 39 | 50 | 61 | 74 | 86 | 96 | 152 |
|  |  |  |  |  |  |  | 3 | 4 | 5 | 5 | 5 | 5 | 4 | 2 | 24 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table A-10. Analyses of size of coal dust particles from intake airways in seven MSHA District 11 mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -70 mesh or < 212 $\mu \mathrm{m}, \%$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | -40 mesh or < 425 $\mu \mathrm{m}, \%$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med }}, \\ \mu \mathrm{m} \end{gathered}$ |
| A | >1 | 90 | 78 | 46 | 72 | 53 | 23 | 27 | 35 | 44 | 55 | 69 | 83 | 95 | 185 |
|  |  | 91 | 79 | 47 | 79 | 57 | 25 | 31 | 41 | 52 | 66 | 80 | 91 | 98 | 141 |
| B | >1 | 89 | 82 | 35 | 62 | 31 | 23 | 28 | 35 | 45 | 55 | 69 | 83 | 95 | 180 |
|  |  | 54 | 30 | 31 | 57 | 32 | 21 | 28 | 35 | 44 | 55 | 67 | 81 | 94 | 184 |
| C | >1 | 85 | 77 | 49 | 80 | 39 | 34 | 40 | 50 | 62 | 75 | 89 | 96 | 99 | 106 |
|  |  | 86 | 80 | 51 | 83 | 33 | 35 | 42 | 52 | 65 | 78 | 90 | 96 | 99 | 99 |
| D | >1 | 94 | 92 | 61 | 97 | 25 | 41 | 53 | 69 | 88 | 96 | 98 | 99 | 100 | 70 |
|  |  | 58 | 41 | 40 | 71 | 28 | 29 | 36 | 45 | 55 | 68 | 84 | 95 | 99 | 128 |
| E | >1 | 71 | 63 | 55 | 91 | 21 | 40 | 50 | 63 | 78 | 90 | 96 | 98 | 99 | 76 |
|  |  | 89 | 78 | 42 | 73 | 25 | 29 | 36 | 45 | 56 | 70 | 84 | 94 | 99 | 126 |
|  |  | 84 | 77 | 51 | 91 | 25 | 34 | 45 | 60 | 77 | 90 | 95 | 97 | 98 | 86 |
|  |  | 91 | 84 | 43 | 66 | 38 | 26 | 31 | 38 | 47 | 57 | 68 | 81 | 93 | 168 |
|  |  | 90 | 83 | 34 | 56 | 32 | 19 | 23 | 30 | 38 | 48 | 60 | 75 | 90 | 224 |
| F | >1 | 68 | 63 | 47 | 93 | 10 | 33 | 45 | 60 | 79 | 92 | 98 | 99 | 100 | 85 |
|  |  | 72 | 64 | 56 | 94 | 20 | 41 | 52 | 68 | 83 | 93 | 97 | 98 | 99 | 71 |
|  |  | 62 | 55 | 47 | 85 | 16 | 35 | 45 | 59 | 74 | 86 | 93 | 97 | 99 | 85 |
|  |  | 55 | 43 | 43 | 80 | 20 | 35 | 44 | 48 | 63 | 78 | 91 | 97 | 99 | 112 |
|  |  | 66 | 64 | 28 | 70 | 7 | 19 | 27 | 36 | 50 | 69 | 90 | 98 | 99 | 149 |
|  |  | 45 | 31 | 54 | 92 | 18 | 42 | 51 | 63 | 77 | 91 | 98 | 99 | 99 | 72 |
| G | <1 | 47 | 28 | 35 | 64 | 22 | 24 | 29 | 37 | 46 | 58 | 75 | 90 | 98 | 169 |
|  |  | 59 | 44 | 36 | 67 | 25 | 23 | 29 | 38 | 49 | 61 | 77 | 92 | 98 | 156 |
|  |  | 58 | 38 | 50 | 87 | 29 | 33 | 42 | 55 | 71 | 84 | 94 | 98 | 99 | 94 |
|  |  | 40 | 16 | 32 | 56 | 31 | 23 | 28 | 35 | 44 | 54 | 67 | 82 | 94 | 185 |
|  |  |  |  | average for MSHA District 11 standard deviation |  |  | 30 | 37 | 48 | 60 | 73 | 84 | 92 | 97 | 128 |
|  |  |  |  |  |  |  | 7 | 10 | 12 | 15 | 15 | 12 | 7 | 3 | 46 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

## Appendix B:

## Analyses of Size of Coal Dust Particles from Mine Return Airways

Table B-1. Analyses of size of coal dust particles from return airways in $\mathbf{3 6}$ mines

| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med, }} \\ \mu \mathrm{m} \end{gathered}$ |
| 1 | >1 | 86 | 74 | 83 | 92 | 24 | 74 | 83 | 87 | 90 | 93 | 95 | 97 | 98 | $\sim 30$ |
|  |  | 80 | 74 | 63 | 80 | 34 | 55 | 62 | 66 | 73 | 79 | 86 | 94 | 99 | 44 |
|  |  | 87 | 76 | 72 | 88 | 41 | 62 | 69 | 74 | 79 | 83 | 88 | 93 | 98 | 42 |
| 2 | >1 | 68 | 53 | 40 | 62 | 45 | 33 | 37 | 42 | 48 | 58 | 71 | 87 | 97 | 155 |
| 3 | >1 | 63 | 40 | 57 | 72 | 35 | 44 | 47 | 52 | 59 | 66 | 75 | 85 | 95 | 91 |
|  |  | 75 | 54 | 76 | 85 | 43 | 68 | 71 | 74 | 77 | 82 | 89 | 95 | 99 | ~20-25 |
| 4 | $<1$ | 77 | 69 | 28 | 55 | 19 | 22 | 27 | 33 | 42 | 54 | 66 | 81 | 94 | 188 |
| 5 | >1 | 82 | 79 | 85 | 93 | 12 | 78 | 84 | 88 | 90 | 93 | 95 | 98 | 99 | ~36 |
| 6 | >1 | 80 | 75 | 59 | 76 | 15 | 52 | 58 | 63 | 68 | 75 | 82 | 90 | 97 | 49 |
| 7 | >1 | 91 | 75 | 52 | 82 | 65 | 46 | 52 | 58 | 67 | 76 | 87 | 96 | 99 | 67 |
| 8 | >1 | 72 | 45 | 63 | 78 | 43 | 52 | 57 | 62 | 68 | 75 | 82 | 91 | 98 | 45 |
| 9 | >1 | 85 | 78 | 42 | 72 | 26 | 29 | 36 | 45 | 57 | 69 | 80 | 91 | 97 | 122 |
| 10 | <1 | 46 | 14 | 38 | 83 | 32 | 24 | 30 | 40 | 55 | 79 | 95 | 99 | 100 | 135 |
| 11 | >1 | 75 | 60 | 33 | 62 | 38 | 22 | 26 | 34 | 44 | 57 | 72 | 88 | 98 | 176 |
| 12 | <1 | 37 | 24 | 27 | 54 | 18 | 19 | 24 | 32 | 42 | 53 | 66 | 80 | 93 | 193 |
| 13 | <1 | 70 | 58 | 38 | 64 | 36 | 30 | 35 | 42 | 52 | 64 | 75 | 88 | 97 | 140 |
| 14 | >1 | 71 | 75 | 42 | 68 | 22 | 30 | 35 | 43 | 53 | 63 | 75 | 87 | 96 | 137 |
| 15 | >1 | 83 | 83 | 47 | 73 | 32 | 31 | 37 | 45 | 56 | 67 | 78 | 89 | 97 | 124 |
| 16 | >1 | 76 | 54 | 41 | 64 | 49 | 24 | 27 | 34 | 42 | 54 | 68 | 84 | 96 | 190 |
| 17 | >1 | 72 | 19 | 42 | 63 | 61 | 26 | 30 | 36 | 44 | 55 | 67 | 82 | 95 | 184 |
| 18 | <1 | 50 | 29 | 32 | 56 | 27 | 24 | 30 | 37 | 45 | 55 | 67 | 82 | 95 | 178 |
| 19 | <1 | 92 | 78 | 75 | 90 | 62 | 60 | 64 | 69 | 77 | 83 | 90 | 96 | 99 | 30 |
| 20 | <1 | 89 | 68 | 36 | 62 | 60 | 20 | 25 | 33 | 43 | 54 | 68 | 85 | 97 | 189 |
| 21 | <1 | 81 | 14 | 43 | 75 | 79 | 27 | 33 | 38 | 47 | 57 | 76 | 90 | 98 | 171 |
| 22 | <1 | 86 | 62 | 56 | 75 | 65 | 32 | 35 | 43 | 52 | 61 | 72 | 84 | 94 | 141 |
| 23 | >1 | 83 | 53 | 53 | 74 | 59 | 27 | 31 | 37 | 46 | 57 | 72 | 88 | 97 | 170 |
| 24 | >1 | 64 | 40 | 38 | 63 | 132 | 22 | 29 | 36 | 45 | 56 | 69 | 83 | 95 | 178 |
| 25 | >1 | 62 | 22 | 42 | 63 | 40 | 24 | 28 | 34 | 42 | 52 | 66 | 83 | 96 | 199 |
|  |  | 56 | 22 | 43 | 65 | 37 | 25 | 29 | 35 | 44 | 55 | 69 | 87 | 97 | 182 |
| 26 | >1 | 89 | 79 | 82 | 93 | 59 | 64 | 71 | 77 | 81 | 84 | 90 | 95 | 99 | 30 |
|  |  | 70 | 70 | 47 | 69 | 28 | 33 | 40 | 47 | 56 | 64 | 75 | 87 | 95 | 121 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Continued on | Next Page |  |


| Mine | Production, Mt/yr | Incombustible, \% | Soluble, \% | Size analysis |  | ash, \% | Corrected size analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ |  | $\begin{gathered} -270 \text { mesh } \\ \text { or }<53 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -200 \text { mesh } \\ \text { or }<75 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -140 \text { mesh } \\ \text { or }<106 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -100 \text { mesh } \\ \text { or }<150 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -70 \text { mesh } \\ \text { or }<212 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -50 \text { mesh } \\ \text { or }<300 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -40 \text { mesh } \\ \text { or }<425 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} -30 \text { mesh } \\ \text { or }<600 \\ \mu \mathrm{~m}, \% \end{gathered}$ | $\begin{gathered} \mathrm{D}_{\text {med, }}, \\ \mu \mathrm{m} \end{gathered}$ |
| 27 | >1 | 79 | 69 | 46 | 73 | 29 | 31 | 37 | 45 | 56 | 67 | 80 | 91 | 98 | 124 |
| 28 | >1 | 77 | 74 | 36 | 60 | 19 | 23 | 28 | 35 | 44 | 53 | 66 | 81 | 93 | 189 |
| 29 | <1 | 66 | 53 | 30 | 54 | 12 | 21 | 26 | 32 | 40 | 50 | 63 | 80 | 94 | 211 |
| 30 | <1 | 61 | 40 | 35 | 57 | 34 | 23 | 28 | 33 | 41 | 51 | 64 | 80 | 94 | 208 |
|  |  | 62 | 16 | 39 | 66 | 54 | 25 | 30 | 37 | 46 | 57 | 73 | 88 | 97 | 171 |
| 31 | >1 | 88 | 81 | 36 | 62 | 39 | 20 | 26 | 35 | 44 | 51 | 64 | 79 | 93 | 201 |
| 32 | <1 | 65 | 21 | 44 | 70 | 52 | 25 | 29 | 35 | 44 | 54 | 69 | 83 | 95 | 186 |
| 33 | <1 | 96 | 95 | 81 | 89 | 60 | 65 | 71 | 76 | 80 | 83 | 88 | 93 | 98 | ~25-30 |
| 34 | >1 | 94 | 90 | 58 | 79 | 36 | 40 | 46 | 54 | 62 | 72 | 82 | 91 | 97 | 91 |
|  |  | 93 | 88 | 50 | 79 | 26 | 33 | 40 | 49 | 61 | 74 | 87 | 95 | 99 | 109 |
|  |  | 88 | 82 | 47 | 66 | 42 | 27 | 32 | 38 | 45 | 54 | 66 | 80 | 92 | 183 |
| 35 | >1 | 39 | 25 | 38 | 66 | 17 | 28 | 33 | 41 | 50 | 62 | 77 | 91 | 98 | 148 |
| 36 | <1 | 41 | 26 | 26 | 55 | 16 | 18 | 23 | 30 | 39 | 52 | 69 | 87 | 97 | 203 |
|  |  |  |  | average for | all MSHA Di | tricts | 35 | 41 | 47 | 55 | 65 | 76 | 88 | 97 | 132 |
|  |  |  |  |  | tandard dev |  | 17 | 17 | 16 | 14 | 12 | 10 | 6 | 2 | 62 |

Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone rock dust), as measured at OMSHR.
The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

Table B-2. Analyses of size of coal dust particles from return airways for seven Pittsburgh seam coal mines

| States | Mines | Samples | -270 mesh <br> or $<53$ <br> $\mu \mathrm{~m}, \%$ | -200 mesh <br> or $<75$ <br> $\mu \mathrm{~m}, \%$ | -140 <br> mesh or $<$ <br> $106 \mu \mathrm{~m}, \%$ | -100 mesh <br> or $<150$ <br> $\mu \mathrm{~m}, \%$ | -70 mesh <br> or $<212$ <br> $\mu \mathrm{~m}, \%$ | -50 mesh <br> or $<300$ <br> $\mu \mathrm{~m}, \%$ | -40 mesh <br> or $<425$ <br> $\mu \mathrm{~m}, \%$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PA,WV | 7 | 10 | 56 | $62 \pm 15$ | 67 | 72 | 78 | 85 | $D_{\text {med }}$ <br> $\mu \mathrm{m}$ |

## Appendix C: <br> Discussion of the Coal Dust and Rock Dust Properties and Experiments

## Limestone Rock Dust Inerting Discussion

From 1985 through 2001, numerous LLEM coal dust explosion tests were conducted in the single entry D-drift, and more recently in A-drift (2008), to determine the concentration of rock dust required to prevent explosion propagation as a function of coal dust particle size, volatility, and other related issues (Table C-1 through Table C-3).

During the LLEM tests with the pulverized Pittsburgh seam coal dust ( $\sim 80 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ), the total incombustible content (TIC) required to prevent an explosion propagation was greater than $79 \%$ but less than $81.5 \%$. This determination was based on a series of 12 explosion tests (Table C-4) [Cashdollar et al. 1987; 1992a,c; Weiss et al. 1989; Greninger et al. 1991; Sapko et al. 1989; 1998; 2000]. In two of these tests (LLEM tests \#51 and \#401), the flame ended well within the dust zone. In the three tests (LLEM tests \#70, \#255, and \#386) where the TIC was $79 \%$, the flame travel extended to or slightly beyond the end of the dust zone. The other 7 tests resulted in flame travel well beyond the dust zone. Non-propagation is defined as no sustained flame propagation of the dust mixture. Propagation is defined as flame propagation of the dust mixture.

During the LLEM tests with the coarse Pittsburgh seam coal dust ( $\sim 20 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ) [Sapko et al. 1989; Weiss et al. 1989; Greninger et al. 1991], a 70\% TIC dust mixture prevented an explosion propagation (LLEM test \#191). A TIC of $\sim 68 \%$ resulted in a propagating explosion (LLEM test \#71).

Prior to having recent access to the MSHA band samples collected from underground coal mines throughout the country, there was growing evidence from limited dust surveys that the coal dust particle size had been decreasing since the promulgation of the existing rock dusting regulations. This decrease occurred as new mining technologies were adopted by the industry (e.g., mining methods involving increased mechanization). For this reason, several explosion tests involving intermediate-sized coal dust particles were conducted within the LLEM. One test (LLEM test \#88) involved the use of medium-sized Pittsburgh seam coal dust ( $\sim 45 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ). To achieve this coal dust blend, pulverized coal dust was added to the coarse dust. For this single test, the medium-sized coal dust was mixed with rock dust to result in a $\sim 67 \%$ TIC for the coal/rock dust mixture. Upon ignition of the methane zone, this mixture resulted in a propagating explosion.

Additional tests were later conducted with a blend of pulverized and fine coal dust to provide an average coal dust particle size ranging from $83 \%$ to $85 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$. This pulverized-fine dust mixture, when mixed with rock dust to result in a $\sim 79 \%$ TIC dust mixture, resulted in a propagation (LLEM test \#357 and \#387). A non-propagation resulted using an $81.6 \%$ TIC pulverized-fine coal dust mixture (LLEM test \#353). The results from these tests were similar to the tests with the pulverized coal ( $80 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ).

One additional test (LLEM test \#388) was conducted with a finer Pittsburgh seam coal dust ( $95 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ). A propagation resulted after using a $\sim 79 \%$ TIC fine coal dust mix.

Based on the LLEM explosion tests, the coal dust particle size has a substantial impact on the propagation potential for a coal dust. As the coal dust particle size decreases, increasing amounts of rock dust are necessary to render the coal/rock dust mixture inert. The greatest impact is evident between the particle size of the coarse ( $20 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ) coal dust and the pulverized ( $80 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ) coal dust. To ensure non-propagation within the

LLEM, the coarse coal dust required at least $70 \% \mathrm{TIC}$ and the pulverized coal dust required greater than $79 \%$ and less than $81.5 \%$ TIC.

During the first test (LLEM test \#517) with the medium-sized coal dust ( $38 \%$ minus 200 mesh or $75 \mu \mathrm{~m}$ ), a $74 \%$ TIC dust mixture resulted in a propagation. Two tests (LLEM tests \#518 and \#522) were conducted with a $\sim 76 \%$ TIC dust mixture and resulted in a non-propagation. The results of these medium-sized coal dust inerting tests are summarized in Table C-4.

Table C-1. Pittsburgh seam coal dust sizes


Table C-2. Limestone rock dust sizes

| Size | Year | $\begin{aligned} & -400 \mathrm{mesh} \text { or } \\ & <38 \mu \mathrm{~m}, \% \end{aligned}$ | $\begin{aligned} & -200 \mathrm{mesh} \text { or } \\ & <75 \mu \mathrm{~m}, \% \end{aligned}$ | $\begin{aligned} & -100 \text { mesh or } \\ & <150 \mu \mathrm{~m}, \% \end{aligned}$ | $\begin{aligned} & -50 \text { mesh or } \\ & <300 \mu \mathrm{~m}, \% \end{aligned}$ | $\begin{aligned} & -30 \mathrm{mesh} \text { or } \\ & <600 \mu \mathrm{~m}, \% \end{aligned}$ | $\mathrm{D}_{\mathrm{s},} \mu \mathrm{m}$ | $\mathrm{D}_{\mathrm{w},} \mu \mathrm{m}$ | $\mathrm{D}_{\text {med, }} \mu \mathrm{mm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pulverized | 1980s | 62 | 76 | 95 | 100 | 100 | 14 | 47 | 24 |
| Pulverized | 2007 | 54 | 72 | 98 | 100 | 100 | 10 | 51 | 26 |

Table C-3. Average proximate and ultimate analyses of coal used in the LLEM experiments

|  | Pittsburgh Coal <br> As received, $\%$ |
| :--- | :---: |
| Proximate analysis |  |
| Moisture | 1.7 |
| Volatile matter | 36.5 |
| Fixed carbon | 55.6 |
| Ash | 6.2 |
| Total | 100.0 |
| Ultimate analysis | 5.4 |
| Hydrogen | 77.4 |
| Carbon | 1.5 |
| Nitrogen | 8.1 |
| Oxygen | 1.4 |
| Silfur | 6.2 |
| Ash | 100.0 |
| Total |  |
| Heating value $=13,803$ Btu/lb |  |

Table C-4. LLEM inerting tests for Pittsburgh seam coal dust and limestone rock dust using a 40 ft long ignition zone

| LLEM test no. -entry | Date | Coal dust |  |  |  | Rock dust, \% | Total Incombustible, \% | Flame travel, ft | Result |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Size | -200 Mesh, \% | Zone, ft | Conc., g/m ${ }^{3}$ |  |  |  |  |
| 49-D | 7/17/85 | pulverized | $\sim 80$ | 40-250 | 200 | 70.0 | 72.3 | 750 | P |
| 50-D | 7/25/85 | pulverized | $\sim 80$ | 40-250 | 200 | 75.0 | 77.1 | 500 | P |
| 51-D | 8/1/85 | pulverized | $\sim 80$ | 40-250 | 200 | 80.0 | 81.5 | 200 | NP |
| 53-D | 9/4/85 | pulverized | $\sim 80$ | 40-640 | 200 | 75.0 | 77.1 | 750 | P |
| $69-$ D | 4/24/86 | pulverized | $\sim 80$ | 40-250 | 200 | 73.0 | 75.2 | 600 | P |
| 70-D | 5/1/86 | pulverized | $\sim 80$ | 40-250 | 200 | 77.0 | 78.8 | 300 | P |
| 71-D | 5/8/86 | coarse | $\sim 20$ | 40-250 | 200 | 65.0 | 67.8 | 390 | P |
| 77-D | 8/6/86 | coarse | $\sim 20$ | 40-250 | 200 | 50.0 | 54.0 | 500 | P |
| 83-D | 10/9/86 | pulverized | $\sim 80$ | 40-250 | 200 | 65.0 | 67.8 | 750 | P |
| 87-D | 11/20/86 | coarse | $\sim 20$ | 40-250 | 200 | 60.0 | 63.2 | 600 | P |
| 88-D | 11/25/86 | medium | $\sim 45$ | 40-250 | 200 | 65.0 | 67.2 | 750 | P |
| $90-\mathrm{D}$ | 1/8/87 | pulverized | $\sim 80$ | 40-430 | 200 | 65.0 | 67.8 | 750 | P |
| 190-D | 6/21/89 | coarse | $\sim 20$ | 40-310 | 200 | 73.0 | 75.0 | 175 | NP |
| 191-D | 7/12/89 | coarse | $\sim 20$ | 40-310 | 200 | 67.7 | 70.0 | 200 | NP |
| 255-D | 1/16/91 | pulverized | $\sim 80$ | 40-490 | 200 | 77.2 | 79.0 | 445 | P |
| 352-D | 9/30/97 | pulv/fine | $\sim 83$ | 40-250 | 200 | 83.0 | 84.4 | 150 | NP |
| 353-D | 10/27/97 | pulv/fine | $\sim 83$ | 40-250 | 200 | 80.0 | 81.6 | 200 | NP |
| 357-D | 12/17/97 | pulv/fine | $\sim 83$ | 40-250 | 200 | 77.0 | 78.8 | 300 | P |
| 386-D | 9/8/99 | pulverized | 72 | 40-310 | 200 | 77.0 | 78.8 | 300 | P |
| 387-D | 9/15/99 | pulv/fine | 85 | 40-310 | 150 | 77.0 | 78.8 | 300 | P |
| 388-D | 9/23/99 | fine | 95 | 40-310 | 150 | 77.0 | 78.8 | 300 | P |
| 398-D | 3/1/01 | pulverized | $\sim 80$ | 40-460 | 200 | 65.0 | 67.2 | 750 | P |
| 401-D | 3/28/01 | pulverized | ~80 | 40-460 | 200 | 80.0 | 81.6 | 200 | NP |
| 512-A | 1/9/08 | pulverized | 69 | 40-340 | 200 | 75.0 | 77.0 | 355 | P |
| 513-A | 1/15/08 | pulverized | 69 | 40-340 | 200 | 80.0 | 81.5 | 230 | NP |
| 514-A | 1/23/08 | coarse | 20 | 40-340 | 200 | 64.0 | 66.9 | 355 | P |
| 516-A | 2/6/08 | coarse | 20 | 40-340 | 200 | 69.0 | 71.5 | 280 | NP |
| 517-A | 2/13/08 | medium | 38 | 40-340 | 200 | 71.7 | 74.0 | 355 | P |
| 518-A | 2/27/08 | medium | 38 | 40-340 | 200 | 74.4 | 76.4 | 280 | NP |
| $520-\mathrm{A}$ | 3/12/08 | medium | 38 | 40-340 | 200 | 68.5 | 71.0 | 550 | P |
| 522-A | 3/26/08 | medium | 38 | 40-340 | 200 | 74.4 | 76.4 | 280 | NP |

## Effect of Particle Size on Coal Dust Explosibility

The effect of coal dust particle size on explosibility is illustrated in Figure C-1, which contains data collected from large-scale explosions conducted in the LLEM from the 1985 through 2008. This curve shows the amount of incombustible material required to prevent propagation for coal dust containing $20 \%$ to $85 \%$ particles passing a no. 200 sieve ( $<75 \mu \mathrm{~m}$ ). Given the experimental test conditions, the curve is the boundary between mixtures that did propagate an explosion (below line) and mixtures that did not propagate an explosion (above line). Experimental results also show that the TIC required to prevent flame propagation becomes much less dependent on coal particle size as the TIC approaches $80 \%$.


Figure C-1. Effect of particle size of coal dust on the explosibility of Pittsburgh seam bituminous coal as tested within LLEM.


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[^1]:    ${ }^{8}$ The Pittsburgh Research Center was part of the U.S. Bureau of Mines until 1996, when it was transferred to the National Institute for Occupational Safety and Health (NIOSH) and became known as the Pittsburgh Research Laboratory. Since 2009, it is referred to as OMSHR.
    ${ }^{9}$ Code of Federal Regulations. See CFR in references.

[^2]:    Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
    The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
    The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

[^3]:    Notes: The incombustible content is the value measured by the MSHA Mt. Hope laboratory.
    The soluble content is the percentage that is soluble in hydrochloric acid (i.e., the calcium carbonate content of the limestone or marble rock dust), as measured at OMSHR.
    The ash includes the ash in the coal plus the insoluble mineral material, as measured at OMSHR.

