

CABLELESS ELECTRONIC SURVEYING SYSTEMS FOR HORIZONTAL HOLES

prepared for

UNITED STATES DEPARTMENT OF THE INTERIOR
BUREAU OF MINES

by

ENSCO, INC.

EARTH SCIENCES and SYSTEMS DIVISION

5400 PORT ROYAL ROAD

SPRINGFIELD, VA 22151



Final Report

on Contract H0177069

CABLELESS ELECTRONIC SURVEYING SYSTEM
FOR HORIZONTAL HOLES

March, 1981

CABLELESS ELECTRONIC SURVEYING
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FINAL REPORT

Prepared for:

UNITED STATES DEPARTMENT OF INTERIOR
BUREAU OF MINES
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FORWARD

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DISCLAIMER

The views and conclusions contained in this document are those of the authors and should not be interpreted as necessarily representing the official policies or recommendations of the Interior Department's Bureau of Mines or the U.S. Government.

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1. EXECUTIVE SUMMARY

Throughout the history of coal mining, the dangers associated with elevated levels of methane gas within the mine environment has posed serious hazards. It has been directly responsible for the destruction of many mines as well as the death of many miners. In response to this, the United States government through the Bureau of Mines has undertaken many research projects whose purpose have been and are to develop methods by which the measurement of the level of this deadly mine hazard as well as the control of the level can be accomplished.

One of the control techniques which has been developed is the use of long horizontal boreholes being placed along a coal seam. Coal which is beneath the earth's surface tends to contain gas, much as a sponge will hold water. Research as well as industry practice shows that by the drilling of the boreholes in the coal seam permit the coal to release large amounts of the gas through the hole where it can be safely vented out of the mine. This technique is particularly beneficial because methane drainage can be done well ahead of the actual mining of the coal seam. Since modern mining methods and equipment expose virgin coal at such a rapid rate, the prerelease of entrapped gas almost becomes a requirement to keep methane levels below the danger point.

The drilling of these long (approx. 2000 feet) boreholes, however, is not without problems. Specifically, maintaining the drill within the coal seam during drilling coupled with the desire to know where the drill is located geographically are problems faced by the drill operator. Until recently, the most widely used technique for surveying during the drilling operation was the use of the Sperry Sun Multi-Shot tool. This tool is used by pumping it down the center of the drill string until it gets to the drill bit. Then a photo

of the internal compass and pendulum position is taken and the tool retrieved. After development of the photo, it is read and the drill operator is given the heading (bearing) and inclination of the drill position. The process is repeated at increments, such as when additional lengths of pipe are added, thereby providing a history and current location of the drill string. Each shot takes approximately 30 minutes to complete from the time the drill stops until drilling resumes.

In the early 70's the Bureau of Mines developed a system that would give the driller information within minutes. It featured radio communication between the drill and the driller, and the use of a computer on the surface to analyze the data and inform the driller of the results. This system provides information in less time than the earlier techniques. However, it did have operational disadvantages, as the computer operators on the surface had to phone the results to the driller in the mine.

With the development of microprocessors in the mid-70's, it became possible to develop a computer small enough to go into the mine, and designed for the driller to operate it. The Bureau of Mines then awarded a contract to ENSCO, Inc. to develop that computer and to enhance the downhole unit that transmits information. This report contains the results of this research project along with conclusions and recommendations for the continued operation and enhancement of the Cableless Survey System (CSS).

The resulting CSS tells the driller where his drill is very quickly following the stopping of the drill. Figure 1 shows the operational setup of the CSS. Time is saved over

previous survey techniques in that CSS remains "downhole" in the horizontal borehole during drilling operations. It is rugged enough to withstand the shock and vibration resulting from the drilling operation.

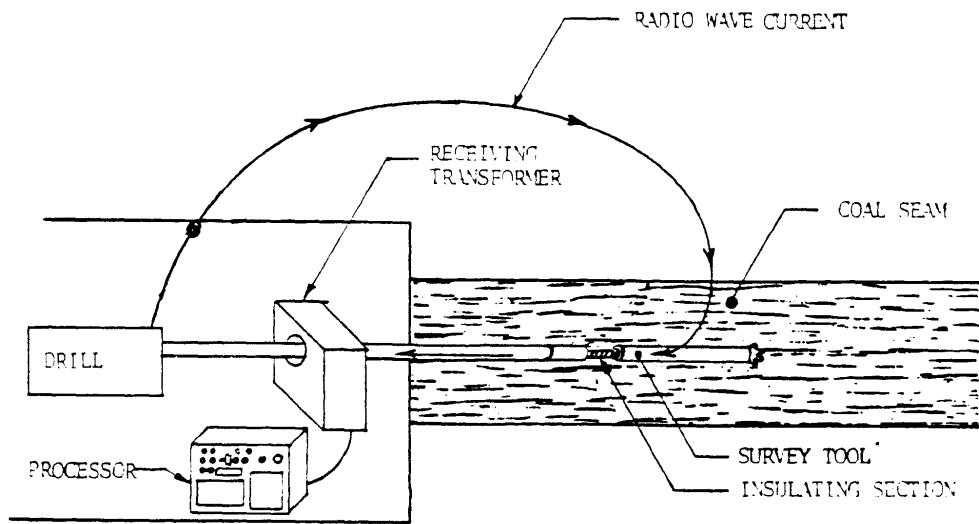


Figure 1. Cableless Survey System

The CSS works by measuring with its on-board sensors the position of the earth's magnetic and gravitational vectors. It then relays that data by induction of an electric current through the drill and the surrounding coal material to the "uphole" receiver/processor. The processor then computes the current position of the tool with respect to the vectors mentioned above and displays the results to the driller. In addition, the processor then adds the new data point to the survey as drill rods are added, thus giving survey information such as vertical and horizontal deviations from a straight line based on initial headings and inclinations at the beginning of the borehole.

Figure 2 is a photograph of the front panel drillers display of the CSS Processor. The keyboards are used to key in initial conditions as well as control the survey operations. Under a hinged panel on the right hand side is located a thermal printer where survey results are printed for reference and records the entire survey. As designed, the entire receiver, processor, display and printer are intrinsically safe. This now permits the driller to have all aspects of the survey system located at the drill site.

This research project which started in October of 1977, was conducted in three phases. A detailed description of the work accomplished in each phase is contained in this report. The three phases are as follows:

- Phase I: Repair and Evaluation of Existing System
- Phase II: Design and Fabrication of a Portable
Display and Processing Unit
- Phase III: Field Test and Upgraded System

During Phase I the initial downhole tool and receiver was repaired and field tested in the Mariana Mines to determine its capability. Results of this testing was the decision to upgrade and enhance the downhole tool to make it more reliable and operationally efficient. Additionally, sensors were added to improve system measurement capability.

Activities under Phase II were the design and fabrication of a portable, intrinsically safe receiver processor. Hardware was designed, developed and tested. Initial field calibration tests were conducted which indicated that the system worked within expected limits. Bearing and inclination errors were within the $\pm 0.5^\circ$ and $\pm 0.01^\circ$ respectively.

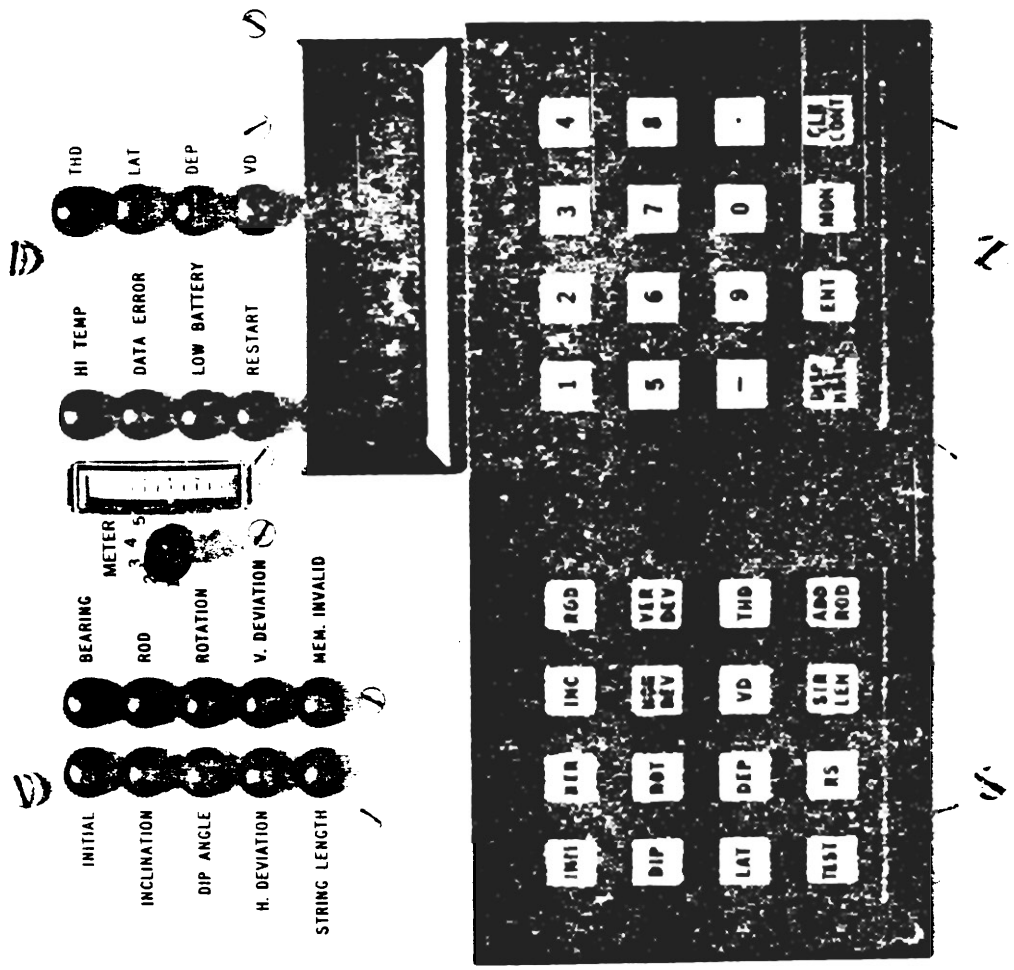
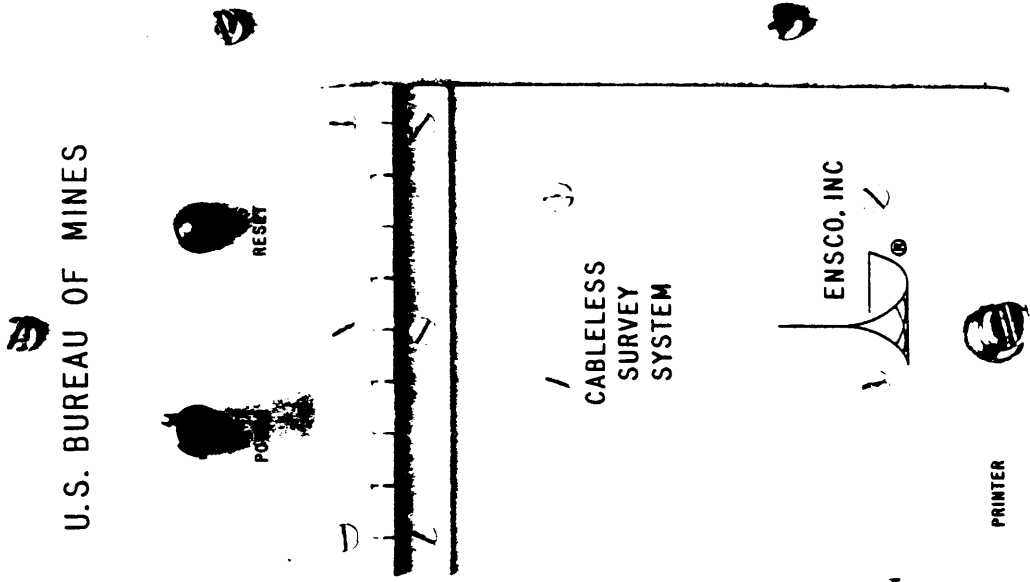


Figure 2. Front Panel of the Cableless Survey System Processor

Phase III work covered the in mine drilling tests and demonstrations. During this phase, the CSS was used during actual drilling operation in two different coal mines. Although, holes that were surveyed totaled slightly over 800 feet, the tool was in place for many redrilling and reaming operations which subjected it to a significant number of drilling hours. Operational problems were encountered during drilling. Most of the problems were associated with battery packs and connections. All were repaired but system availability was hampered by these problems. Other operational problems were in the area of the size and weight of the tool and its effects on drill guidance.

In conclusion, the newly enhanced and upgraded CSS provides critical survey information in a timely and efficient manner to the drill operator. The development of the permissible microprocessor subsystem has provided a system that can be tailored for future expansion of the CSS as well as other research applications requiring data acquisition and processing on site in the hazardous mine environment. The operational problems discovered during actual field use should be further examined and incorporated in future design. The research project has provided the industry with the capability of increased productivity in degassing operations.

2. PROGRAM ACTIVITIES

The objective of this program was to recondition the United States Bureau of Mines (USBM) cableless surveying system (CSS) and improve its operational capability. The program was divided into three separate phases. They are as follows:

- Phase I: Repair and Evaluate Existing System
- Phase II: Design and Fabricate a Portable Display and Processing Unit
- Phase III: Field Test of Upgraded System

Phase I

Phase I of the program started in October 1977 and culminated in May of 1978 with the submission of the Phase I report. During this phase, work consisted of the repair of the downhole unit to make it operational, field testing and an evaluation of its capability.

The repair of the downhole unit involved both mechanical and electrical aspects of the device. Some of the repair work actually involved minor modifications to improve previous known difficulties. The centralizers which support the inner canister in the outer driller collar as originally designed failed during previous testing. In addition, these centralizers did not properly support the inner unit which permitted it to flex and disturb proper sensor alignment. New centralizers were designed and fabricated by molding urethane to form a collar with spacers which fit around the inner canister. This later proved to be very successful. The new pieces slipped on and off with no direct attachment and could be easily replaced and spaced along the entire length of the canister.

Another activity that went beyond what would normally be considered as repair was a modification that permitted the batteries to be recharged without disassembly of the downhole unit as previously required. Circuitry was added to the power control circuit boards which permitted a modified audio power oscillator to be connected to the downhole transducer in a fresh air environment. This technique fully recharges the batteries in about sixteen hours and eliminates the requirement for disassembly of the tool.

Once the downhole unit was considered operational, it was subjected to pressure tests to ensure that the integrity of the explosion proof canister still met permissability requirements. The inner canister was subjected to a minimum pressure of 1500 psi over a 10 hour period. During the test a peak pressure of 1700 psi was experienced. After testing the unit was operated and then disassembled to determine if any leakage had occurred. The unit operated satisfactorily and no leaks had occurred.

Following the above repair and rehabilitation the CSS was taken to the mine for field testing and data acquisition. The mine chosen for the field testing was Marianna #58 in Pennsylvania. During the field tests the downhole unit operated satisfactorily when exposed to more than 25 hours of drilling operations including several hours of hole reaming activities. Only minor problems were encountered during this testing. They involved thermally induced drift of the system receiver, operational difficulties associated with mounting the up-hole toroid and excessive water pressure required to trigger the downhole unit. All of these problems were expected prior to testing and steps were already planned for Phase II that would correct them.

The data from the field test was tabulated and returned to ENSCO, Inc. for detailed analysis. In addition, survey data from the Sperry-Sun survey tool used to survey the same hole was gathered for comparison. Results of the comparison indicated that the CSS closely matched the survey results obtained with the Sperry Sun. For example, in a survey of a 830 foot hole, the two survey tools differed by approximately 2.3 feet in vertical deviation and less than 1 foot in lateral deviation. Further lab testing indicated that certain instrument biases associated with sensor mechanical alignment and electrical offsets did exist in the CSS. Also, an error analysis was done by feeding simulated data into a computer which indicated significant errors could exist with the CSS when it is directed along a northerly or southerly heading. It was determined that by adding two additional sensors to the downhole unit, these errors would be greatly reduced.

A report for Phase I which gives the details of all Phase I activities was prepared and submitted to the USBM. Results of the computer analysis are contained in Appendix A of this report.

Phase II

Program activities that were accomplished during Phase II of the contract were the modification and upgrade of the downhole tool, and the design and development of a new portable uphole receiver-processor.

As a result of Phase I activities, as well as previous drilling experience, a number of deficiencies with the downhole survey tool were outlined. They were as follows:

- Water pressure required for triggering downhole tool too high,
- Excessive errors caused by sensor ambiguities when operated along a northerly or southerly heading,

- Electronic components included originally which were no longer available,
- Transmit clock instability which prohibited receive tracking on a reliable basis.

The downhole tool was designed to send a transmission sequence when the water pressure in the drill collar is raised to a level greater than 100 psi. In actual field test operation this pressure was difficult to obtain. A number of factors were responsible such as too small or defective pump, lack of enough water volume, debris clogging the water way, etc. Since the pressure problem was still evident in Phase I of this program, it was decided to install a lower pressure trigger switch. An identical switch with a lower range which now activates the downhole tool with approximately 70 psi water pressure was installed.

In order to correct the anomalies associated with the north-south problem, it was decided to add two additional sensors. These sensors consisted of biaxial accelerometers oriented to detect the gravitational vector along the planes from side to side and top to bottom of the sensor canister. A single package was procured that contained both accelerometers mechanically aligned 90° apart from each other.

The addition of the new sensors required that the sensor canister be made longer. In order to make room for this extension while maintaining the original overall package length forced the repackaging of the electronics to provide the additional space. The requirement for repackaging also provided the opportunity to improve several other known deficiencies.

In the original design, the survey tool clock was controlled by resistor-capacitor timing. This proved to be unstable in the drilling environment and therefore required wide bandwidths in the receiver tracking circuits. The increased bandwidth also increases the susceptibility to noise problems. Therefore, a crystal controlled clock was installed in the survey tool. This will permit narrow bandwidths to be used in the telemetry receiver.

During the rehabilitation of the downhole package done in Phase I the A/D converter was found to be inoperative. Attempts to replace the unit led to the discovery that the particular part was no longer manufactured. Fortunately, one was found and installed for testing, but no spare units for future repair would be available.

In light of all of the above it was decided that the downhole survey tool electronics would be upgraded throughout with commercially available components. Further, the existing explosion proof canister would be retained unaltered so as to retain permissibility.

Appendix B gives the resulting mechanical layout of the upgraded tool along with its output specifications and sensors specifications.

The second aspect of the Phase II activity was the design and development of a permissible portable uphole receiver and processor. A system design was submitted that called for the use of low power CMOS circuitry. It was felt that the use of this low power integrated circuit technology would simplify the permissibility process because power requirements would fall within the intrinsically safe levels. Figure 2 shows the front panel of the resulting receiver/processor.

A detailed description of the system design is included in Section 3 of this report.

The final activity of Phase II was the testing and alignment of the system. Since this device uses the earth's magnetic field as its input and this field is disturbed in the proximity of magnetic materials, i.e., buildings, cars, pipes, etc., the system was taken to an open land area. The field tests consisted of rotating the package around each axis and plotting the output from each sensor to determine exact scale factor and offset. After exact scale factor and offsets for each sensor channel were determined new algorithm coefficients were calculated and incorporated in the processor programmable memory. The rotational tests were then repeated for verification.

It should be noted that vertical rotation of the package was not accomplished. This was due to the fact that the package was very long and heavy and would require a complicated and costly fixture to support the unit while providing precise alignment.

Following the alignment tests, the system was subjected to a simulated trajectory test. This was done by placing a pattern of nine holes in a board in the following arrangement.

●2	●3	●4
●9	●1	●5
●8	●7	●6

The coordinate distance between each hole was such that movement between any two adjacent holes vertically or horizontally repositioned the tool by 1° in bearing for horizontal and 1° in inclinations vertically. The simulated survey was performed

by entering the initial conditions for hole #1 at an initial string length of 20 feet. Then a survey of the first hole position was done and an assumed 10 foot drill rod added. The tool was then positioned sequentially in each hole and a survey done adding 10 foot rod sections for each hole until hole #1 was repeated. This resulted in a total simulated survey of 120 feet of string length. Figure 3A shows a comparison of calculated bearings versus tool measurements. Figure 3B gives the same comparison for inclination. Figure 3C compares the theoretical survey path to the computer results provided by the cableless survey system. As seen in Figures 3A and 3B the bearing and inclination readout fall very close to the expected accuracies for the transducers, i.e., $\pm 0.5^\circ$ for the magnetometer and $\pm 0.1^\circ$ for the accelerometers. Some of the inclination errors are slightly outside of the expected variance. This has been attributed to two factors. First, a buildup of tolerance and secondly a slight play in the interface of the holes in the target and the positioning pin. In addition, errors in the absolute position of the hole were not corrected or compensated.

The errors associated with sensor relative alignments were examined by repeating the simulated trajectory test twice. First, two readings separated by a 180° rotation were average for each hole and then repeated taking four readings separated by 90° rotations for each hole. The results of these tests are:

	2 Readings Per Hole	4 Readings Per Hole
Bearing errors: mean	0.149°	0.145°
Standard Deviation	1.12°	0.078°
Variance	1.20°	0.006°
Inclination errors:		
mean	0.003°	0.006°
Standard Deviation	0.084°	0.07°
Variance	0.007°	0.005°

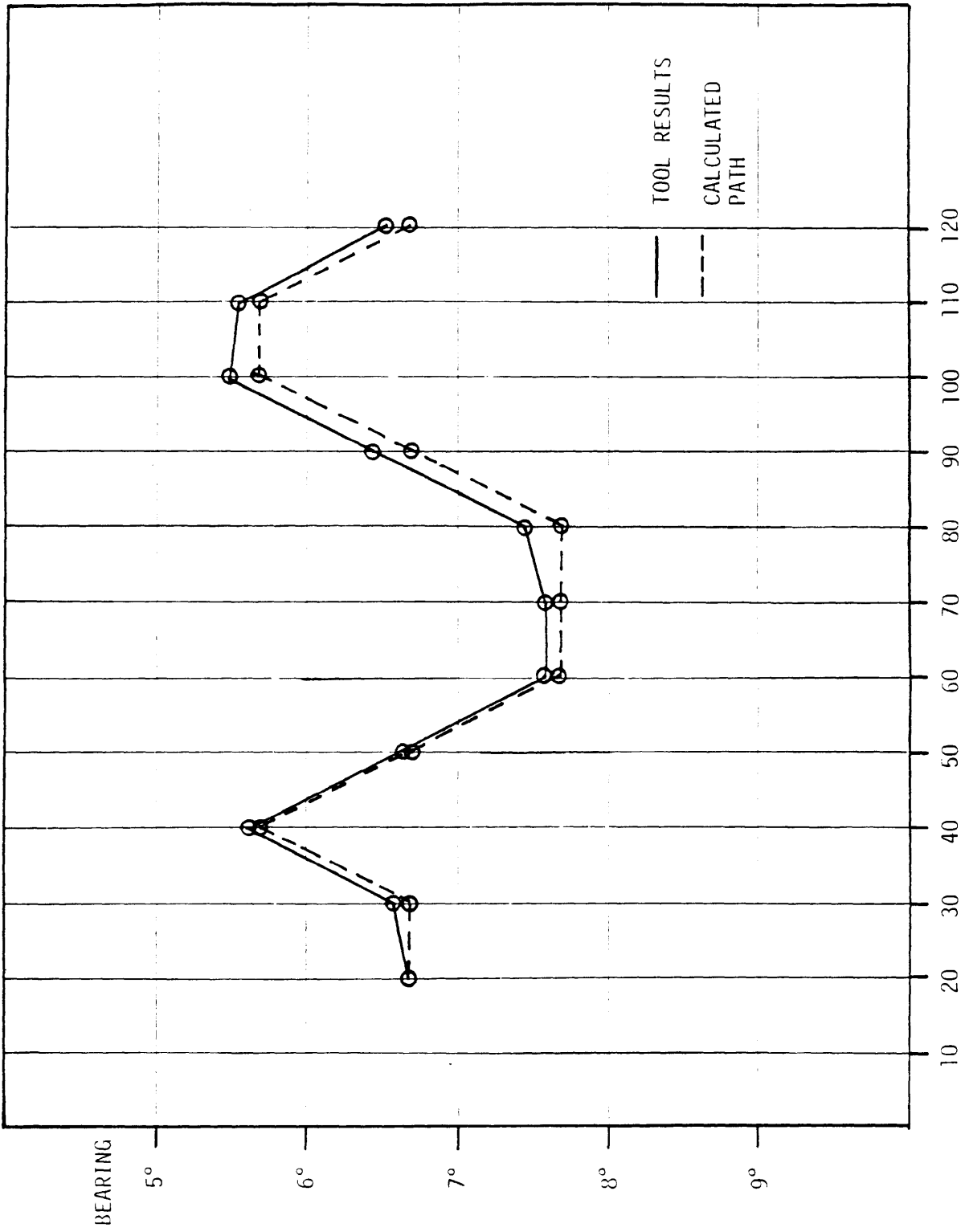


Figure 3A. Comparison of Calculated Survey Path vs. Measured Bearings for Simulated Trajectory Test

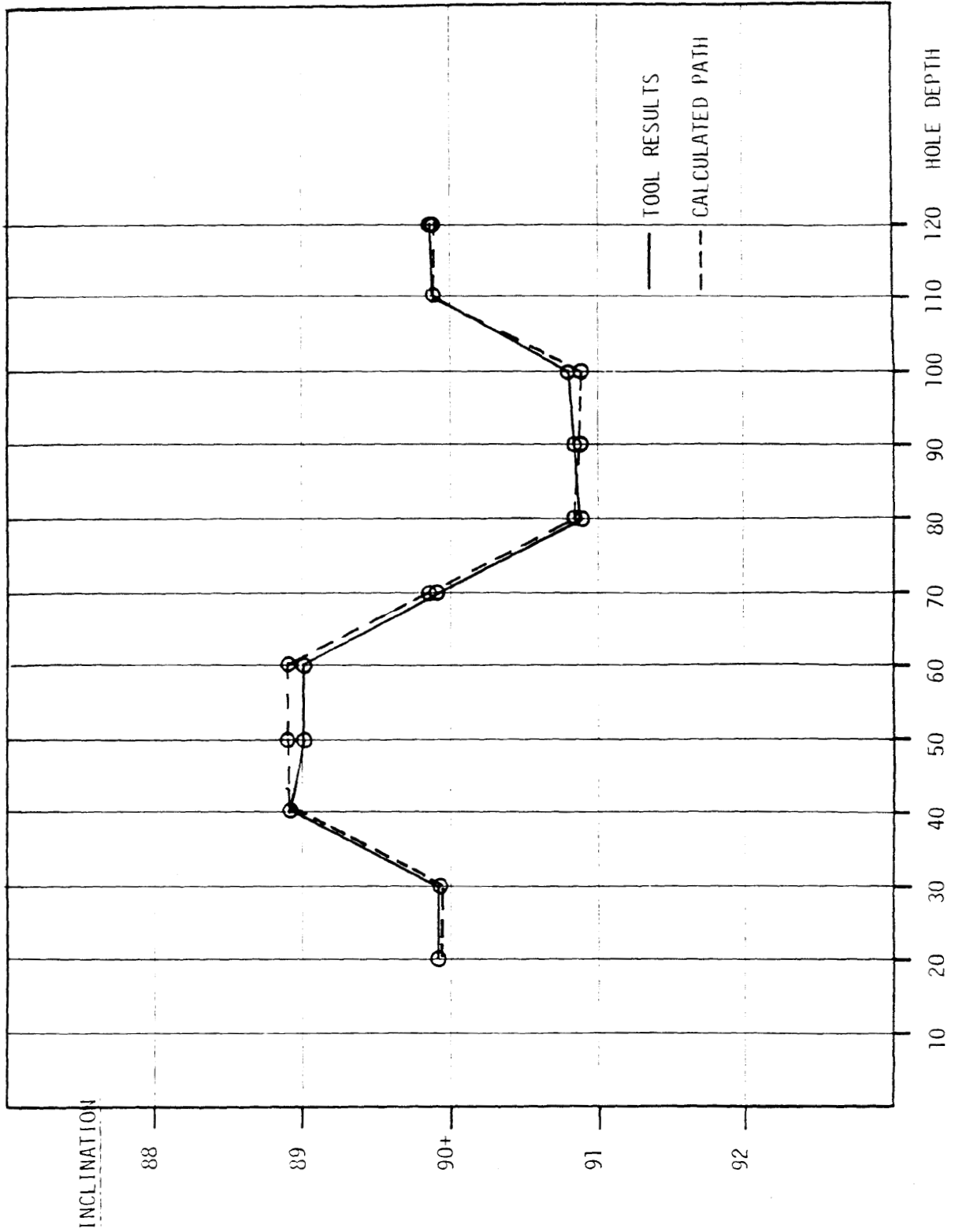


Figure 3B. Comparison of Calculated Survey Path vs. Measured Inclination for Simulated Trajectory Test

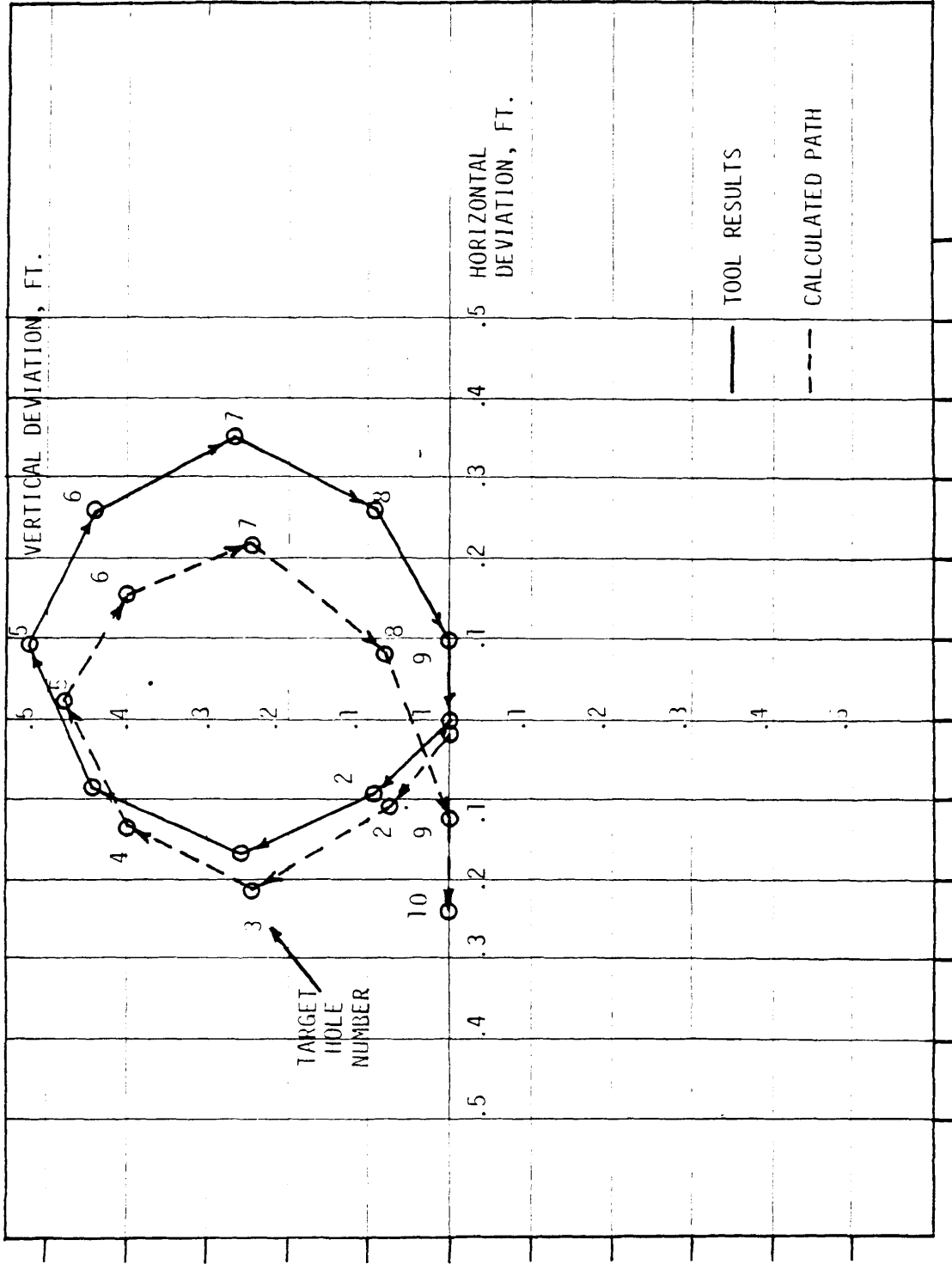


Figure 30. Comparison of Calculated Survey Path vs. Measured Survey Path for Simulated Trajectory Test

These results are interesting in that the errors associated with the accelerometers are fairly consistent in both cases and are well within the expected ranges. The bearing calculation is the result of combining the outputs of three orthogonally oriented magnetometers. The inclination is the result of a single accelerometer oriented axially within the package. Therefore, the bearing includes the combination of three independent errors whereas the inclination error is the result of a single transducer and thus the larger bearing errors and the statistical improvement with four readings.

Phase III

Phase III began in July of 1979 with the first in-mine drilling test of the upgraded system. Testing began in Eastern Coal Company's Federal #1 mine near Fairmont West Virginia. A series of problems with the drilling operation caused a one month delay in the field test activities. The problems were primarily associated with the drill motor itself and the water pump used.

Upon return to Federal #1 in mid August the USBM had installed a new drill motor and water pump system. The CSS was installed and drilling was begun. During the testing phase the only problem encountered with the CSS centered around two areas.

First was the batteries. In both the downhole tool as well as the uphole tool battery life seemed to be much less than the theoretical life should be. Later examination of the batteries revealed failed cells in the positive side of the downhole battery pak and failed cells in the receive side of the uphole processor. Batteries were replaced prior to future drilling operations.

The second problem deals with an intermittent contact on the downhole toroid connections. This was fairly a fairly severe problem in that the toroid connection is buried deep within the potted transducer. The connection was reconditioned and future drilling activities were accomplished without problems in this area. Another aspect with this same connector was discovered during this test series was the problem of debris in the water supply lodging against the connector and the result blockage of sufficient water flow and pressure. It was realized that a water supply filter must be used when the CSS is used to restrict particles greater than 1/16 inch from being pumped into the drill string.

Even with the above problems, the CSS was used successfully during actual drilling operation to survey from 35 feet to 320 feet in the hole. In addition, the Sperry Sun Tool was used to survey the same hole. Figure 4 shows a comparison of the CSS results and the Sperry Sun for vertical depth of the hole. The difference between the two surveys falls primarily in an initial reported offset. Although no specific reason for the difference was determined, the basic output of the two tool results does correlate.

A record of automatic receiver gain settings was kept and is given in Figure 5. As shown as string length increased, received gain also increased. This is especially true out to about 290 feet. Beyond 290 feet receiver gain started to decrease. This was due to an abandoned drill string which was seized in an adjacent hole. In fact the drill bit eventually hit the adjacent drill steel at 329 feet. Note that the readings taken while the two drill strings were in contact were 34dB and 10dB. These very low gain readings were due to the excellent conductivity of the return signal path provided by the seized drill string.

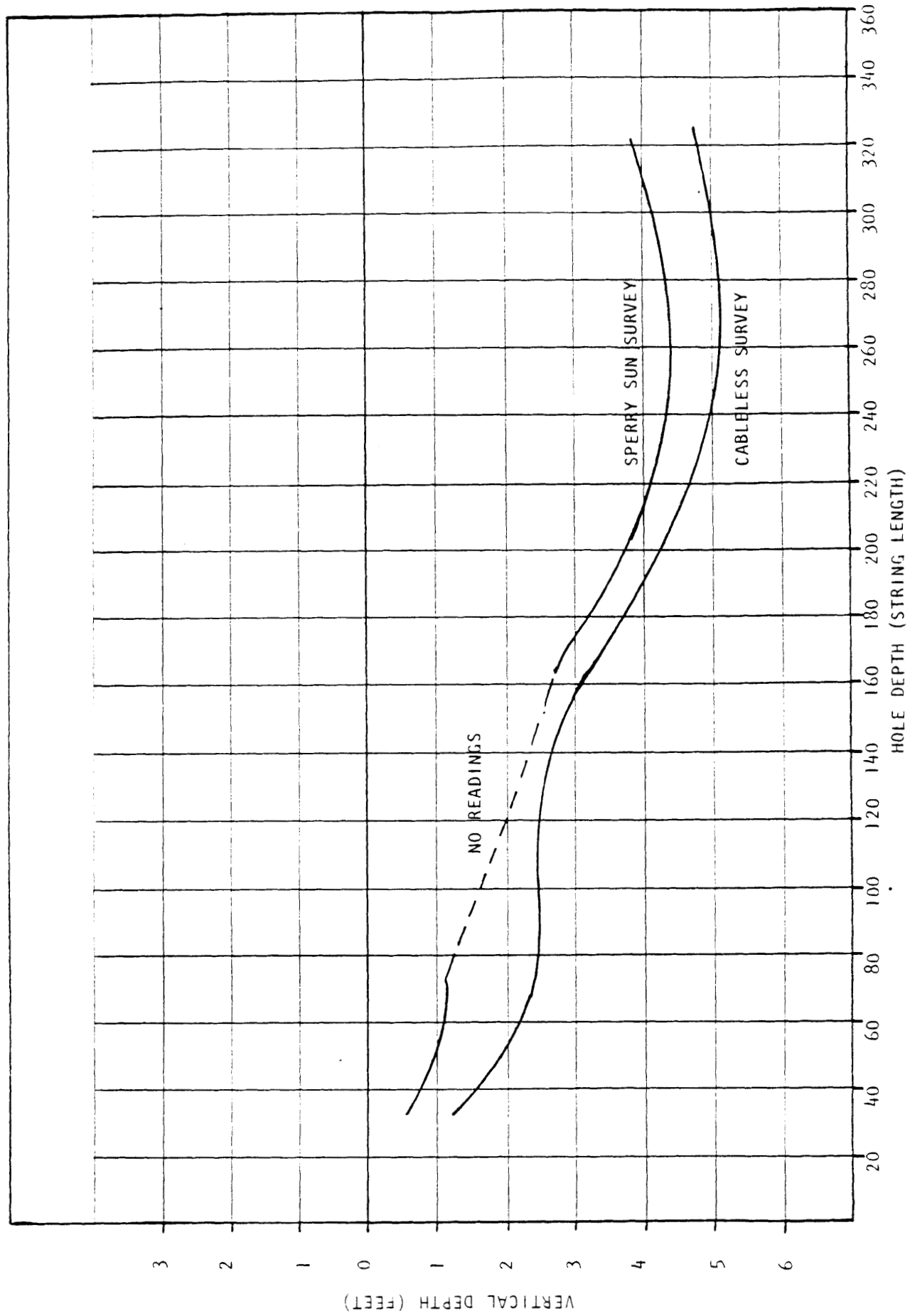


Figure 4. Vertical Survey of Horizon #1 Drill Hole Using Sperry Sun Tool and CSS

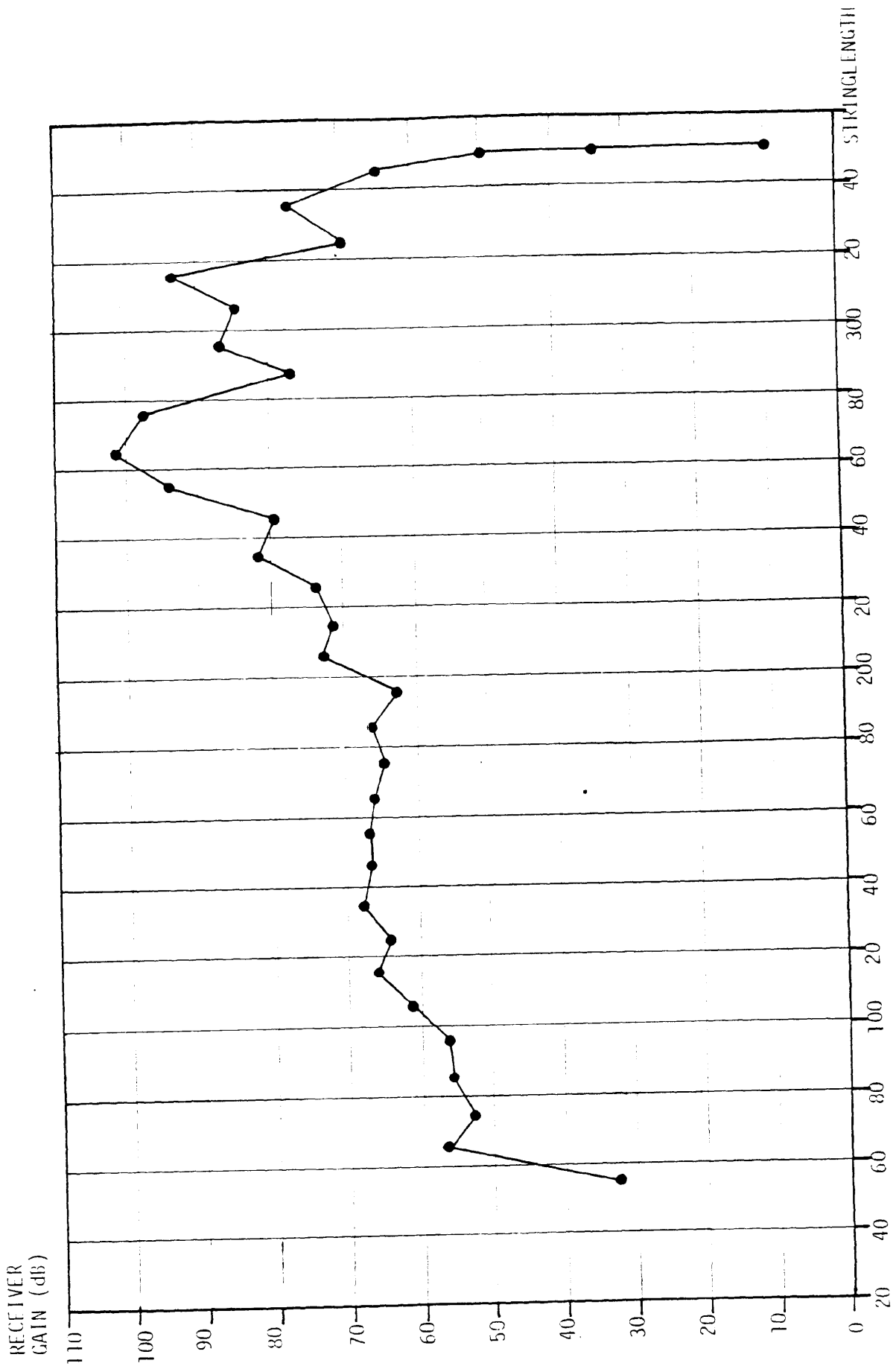


Figure 5 . Receiver Gain vs. String Length

The readings which were taken out at 245 feet and 255 feet were higher than expected and were actually getting close to the limit of the receive capability. Later testing showed that these high readings were the result of the "dirty" hole. For example, in hole depths on the order of 400 to 500 feet receiver gains of 40 to 50dB were common provided the hole had been washed clean of cuttings prior to the transmission.

Hole #2 was abandoned after several attempts to redirect the drill had failed. A third hole was started but had to be abandoned when the drill could not be kept in the hole. Therefore, no other survey tests were conducted at Federal Mine #1.

The tool was returned to ENSCO while the next drilling site was being prepared. While at ENSCO, adjustments were made to improve the operational characteristics of the system. These improvements were based on experience gained during the Federal #1 mine drillings. These changes occurred primarily in the area of monitoring capability and operating signalling via the front panel to indicate what operation the system is performing. These changes were most beneficial in removing the "mystery" of the electronic survey system.

The next drilling activity occurred in December of 1979 at the Mariana #58 Mine in Pennsylvania. During the drilling program the CSS was successfully used to survey the drilling operation to a depth of 490 feet.

While drilling at the Mariana Mine the survey system worked fairly well. On several occasions when the survey indicated that drilling was approaching regions known to contain slate binder layers within the coal seam, cuttings indicated that

the layers were hit within 5 feet along the drill path. This was at a string length of 454 feet. Records of the receiver gains attained in this field trial indicated that with a clean hole, good ground and good bit to coal thrust pressure, numbers on the order of 40 to 60dB of gain were common through this drilling from 55 feet to 490 feet.

As with the previous testing exercise, batteries continued to be less than adequate. The problem was traced to be the interconnections within the battery cansiter and the relays used to activate the system. These items were all repaired and no further debilitating problems occurred. Another less serious problem that occurred throughout the testing was the triggering of the down hole unit. This is done by raising the water pressure to at least 70 psi and then permitting it to fall below 60 psi. The various pumps used and available water supplies were often not capable of not delivering the required levels unless orifices were installed in the bit to restrict flow.

The final aspect of Phase III was the development of an O&M Manual and a classroom training session given at the Bruceton Research Center. Personnel from the Bureau and from the independent drilling contractor were trained in this operation and maintenance of the system.

3. SYSTEM DESCRIPTION

The Cableless Survey System (CSS) is designed to provide near real time data during degasing operations in coal mines. Degasing is performed by drilling long (up to 2000 feet) horizontal boreholes into a virgin coal seam. The survey or downhole tool is attached directly behind the drill bit. This is shown in Figure 6 below.

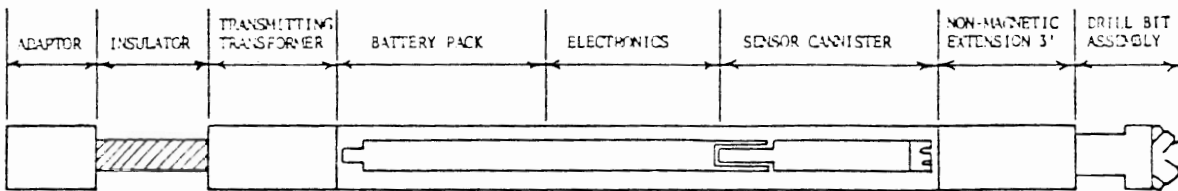


Figure 6. Survey Tool and Drill Bit

In the survey tool, the transmitter and battery are separate assemblies which join together in a pressure-tight tube. The sensors are in a separate pressure-tight tube which joins to the first. This pressure tube assembly is then enclosed in an outer tube with an annular space between them for water passage. The transmitting transformer joins the main package with a water-tight electrical fitting and has a hole through its center for water flow. A short non-magnetic extension of the same size as the outer tube is added at the sensor end of the unit to isolate the effects of magnetism which might exist in the drill bits and subs. The downhole unit mounts close behind the drill bit. Figure 7 is a block diagram of the survey tool electronics.

The sensor outputs are sampled in a time division multiplex technique in which each sample is converted from analog to digital form and used to modulate the phase shift transmitter.

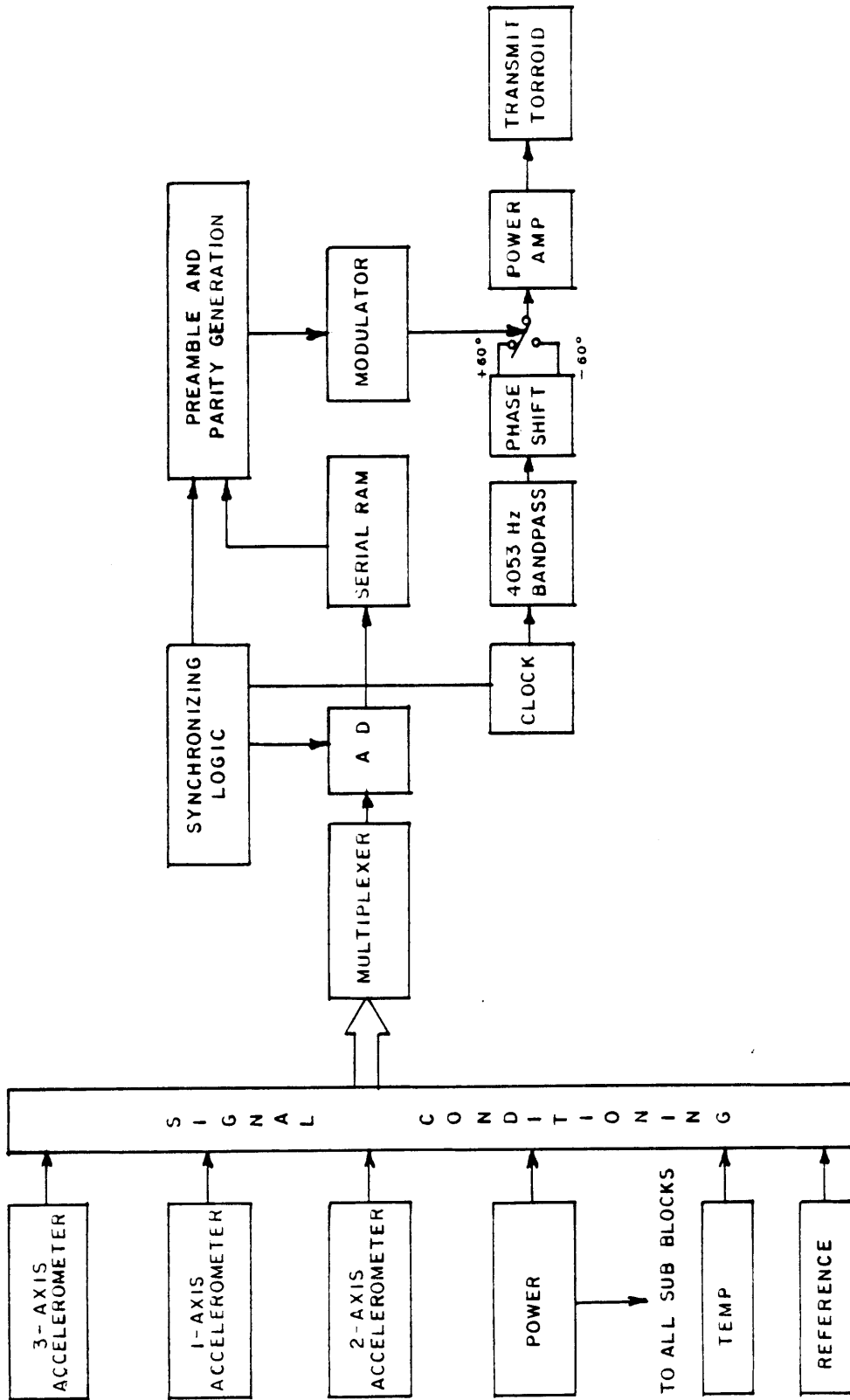


Figure 7. Block Diagram of Downhole Survey Tool

The sensor data transmission is preceded by a long pulse of the carrier followed by a fixed message for receiving synchronization. The exact message and data format of the survey tool are contained in Appendix B. The transmitter output is efficiently coupled to the drill string by the transmitting transformer. The transmitting transformer is oriented such that it induces a true electric field into the drill string. The return path for the electric current is through the surrounding coal.

The signal on the drill string is picked up at the surface by the Receiving Transformer, Figure 8, and then passed via the toriod cable.

The receiving Transformer is mounted on the drill rig at the surface so that the drill pipe passes through it. The Processor, which includes the computer and receiver, is adjacent to the drill rig.

As mentioned before the survey tool contains a triaxial magnetometer, a biaxial accelerometer, and a single axis accelerometer. These sensors are used to measure the vector relationship in each axis to the earth's magnetic field and the earth's gravitation vector. Figure 9 shows graphically the directions of the earth's vector.

The Processor utilizes an automatic gain ranging, variable bandwidth phase lock technique for maximum separation of the signal from the noise. The Processor then calculates the bearing and inclination of the downhole unit.

When given the length of drill pipe sections, the Processor calculates the location of the bit and its deviation from the desired course.

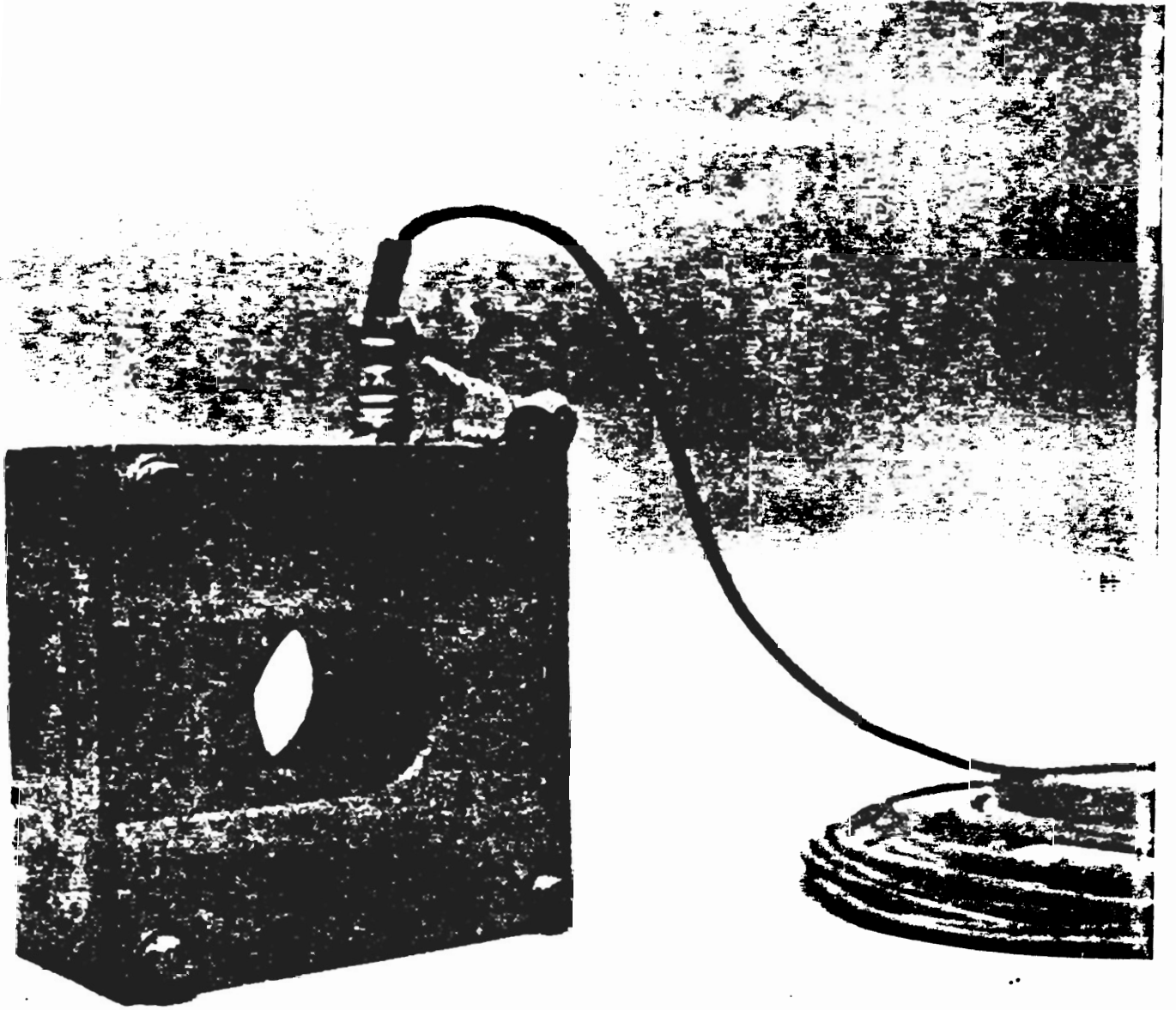


Figure 8. Receiving Transformer

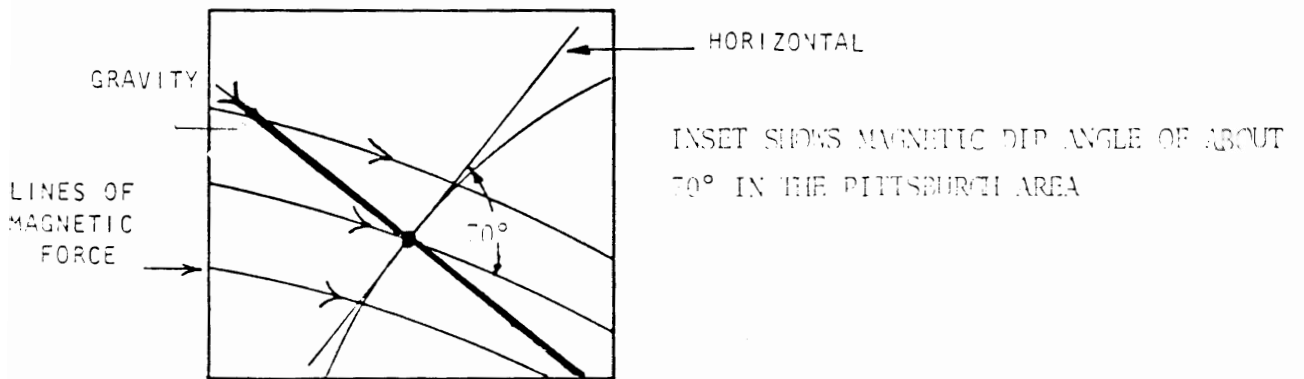
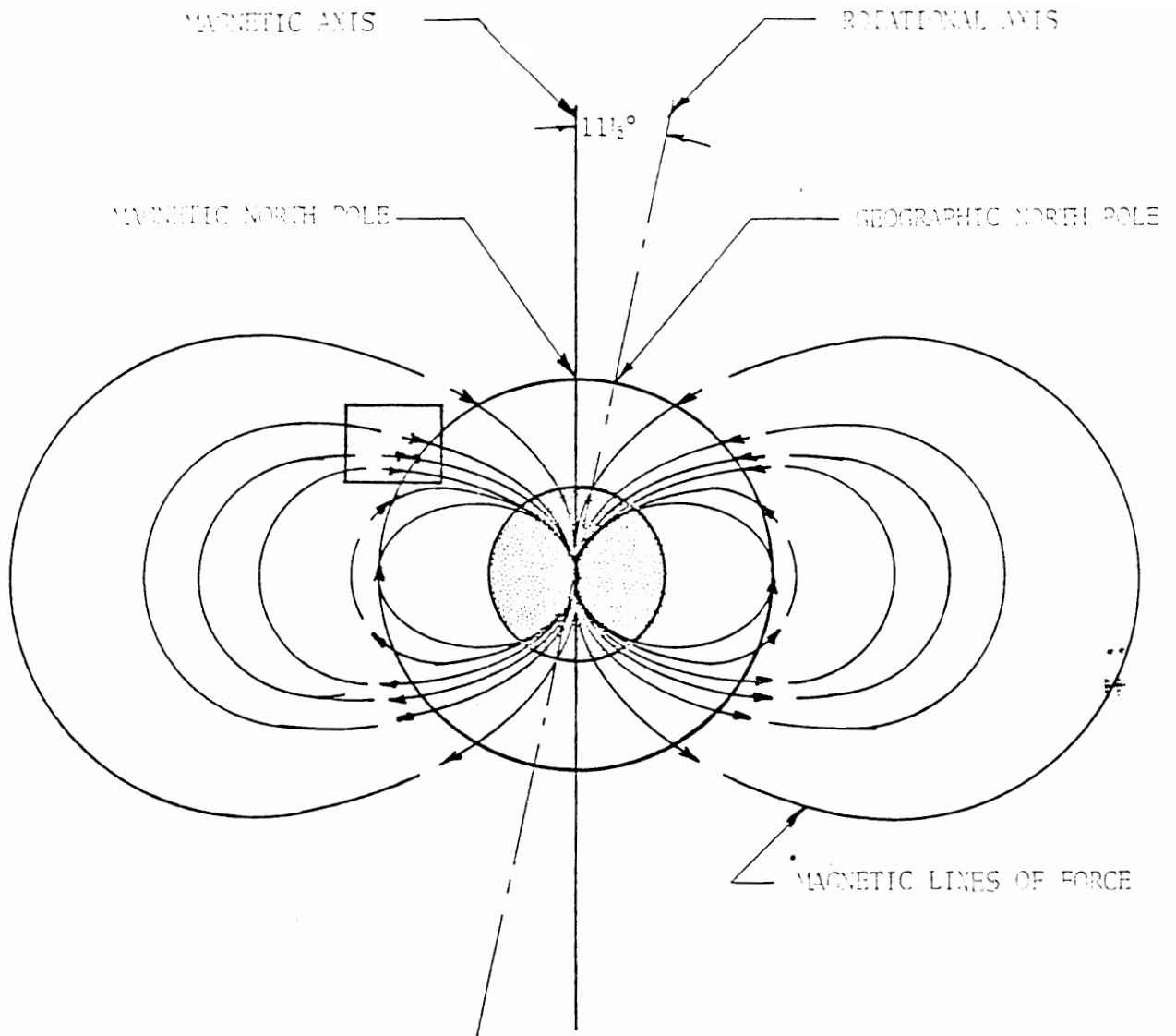


Figure 9. Direction of Earth's Magnetic and Gravataional Vectors

Figure 10 is a block diagram of the system receiver. Figure 11 is a block diagram of the microprocessor based processor and display unit.

When the processor receives data from the system receiver it performs several functions. First, it does data error testing by examining that data parity is correct and that the raw data values are within reasonable limits. Following the data checking, the processor then processes the received data to calculate the necessary parameters for the survey. Finally, the processor displays on its front panel those parameters that the drill operator needs to know such that he can initiate drill actions to guide the drill within the coal seam. Appendix D contains the detailed schematics of the survey tool, receiver and processor. Also included are the software program listings employed by the processor. Appendix E contains a discussion of the computer algorithms that are employed by the processor.

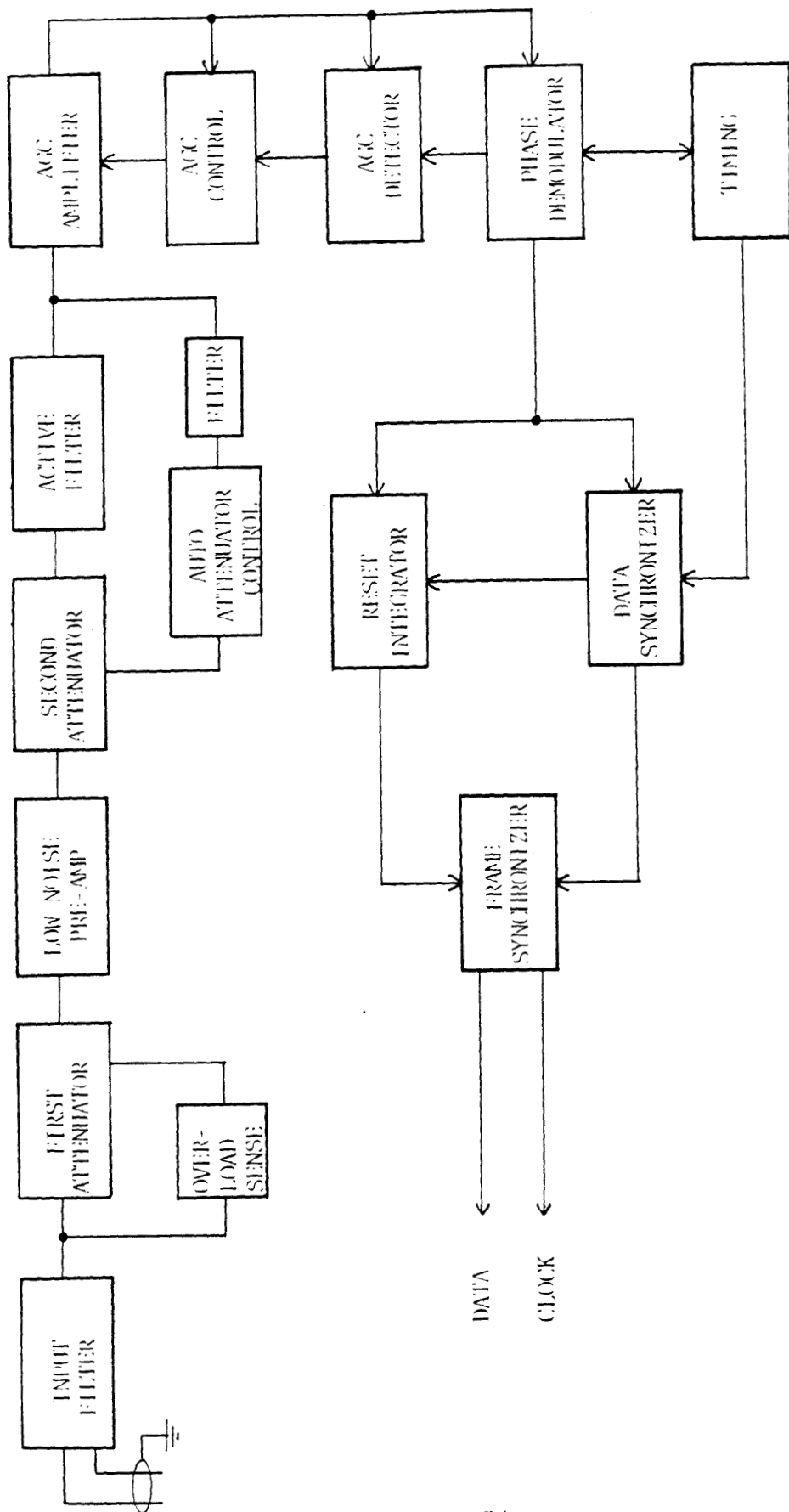


Figure 10. Telemetry Receiver Block Diagram

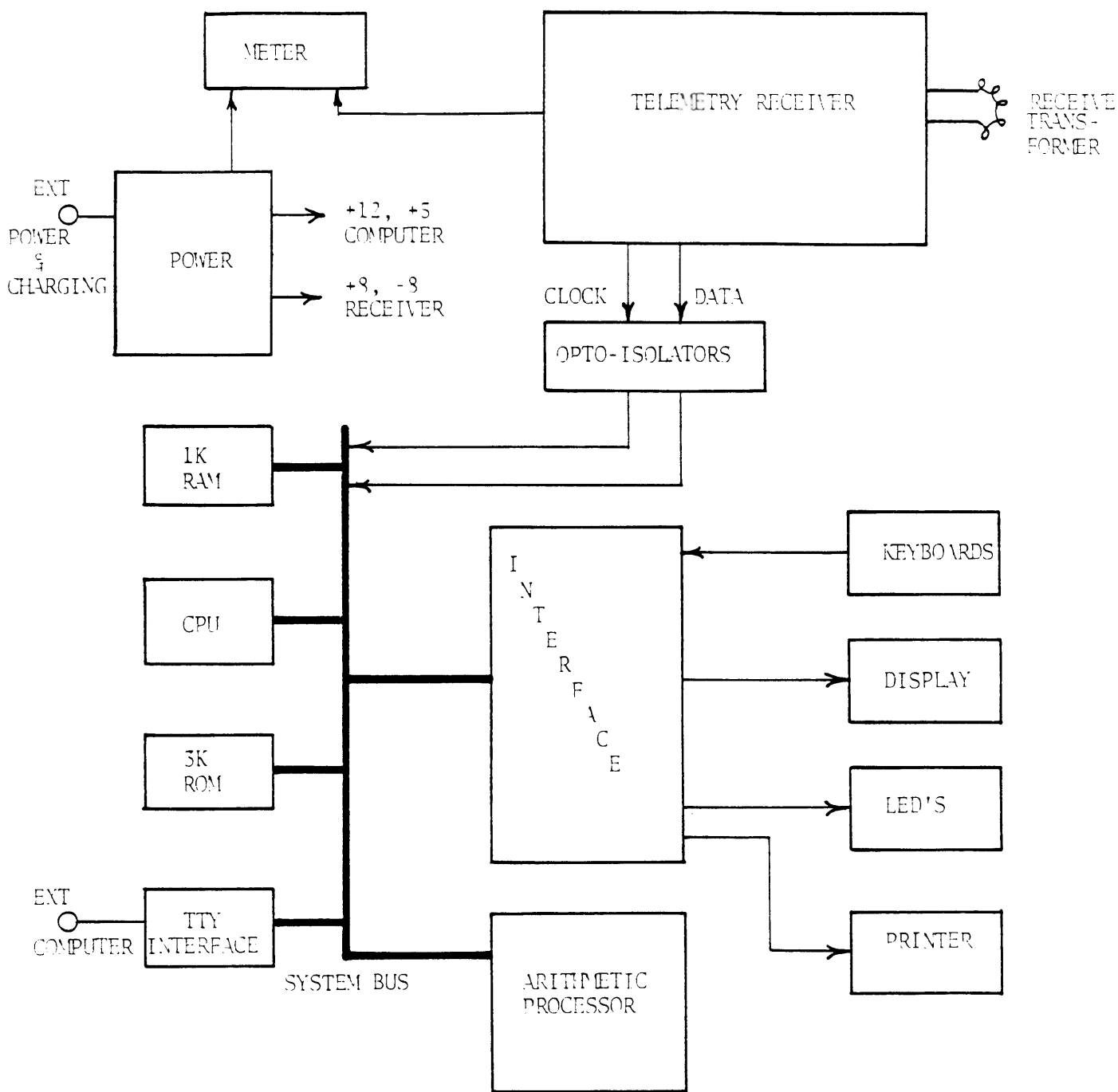


Figure 11. Block Diagram of Uphole Processor and Display Unit

4. CONCLUSIONS AND RECOMMENDATIONS

The Cableless Survey System developed in this project has proved that drilling efficiency can be enhanced when detailed drill bit position is made available to the drill operator in near real time environment. Field tests have shown the CSS is as accurate as previous methods for borehole surveying and saves time in that the survey tool can withstand the drilling shock and vibration. The uphole receiver processor has proven to be reliable and most importantly portable.

As with any project of this nature, looking back over the final design as it related to operational use there are, of course, some recommendations that ENSCO, Inc. feels would significantly enhance the tools operation. Efforts to further utilize, upgrade and improve the system should be continued.

The following is a list of recommendations by subsystem that should be explored in any further development.

PROCESSOR

- Access to the values of average inclination and bearing that the Processor uses for advancing the survey will allow projection of hypothetical surveys.
- Allow initial values for seam dip angle and vertical depth in the seam so the computer will read out (on demand) the current vertical seam depth.
- Extend the memory by 2K-4K to allow for program expansion.
- Change the batteries used to take advantage of recent improvements in sealed lead acid cells.

SURVEY TOOL

- Break the package about 10 feet back from the front end so a stabilizer can be put at a more effective distance from the front and to make the package more manageable.
- Change the batteries to lead acid. They are more durable and need fewer inter-cell connections.
- Use a pumpable battery pack or downhole water turbine generator (could also be used to measure water flow).
- Develop sensors to read thrust, RPM and torque.
- Lighten the inner canister.
- Operate the tool as radio source to get attenuation curves in coal and other media.
- Reduce the outside diameter of the downhole package to allow more drilling control.
- Provide two way radio communication to eliminate the need for water pressure triggering.
- Design a new means for lengthwise compensation of the inner sections. The existing rubber cushions take a set and are difficult to install.

APPENDIX A

PHASE I - COMPUTER ANALYSIS OF SURVEY RESULTS

ERROR ANALYSIS OF DOWNHOLE TOOL

SURVEY RESULTS

During Phase I the CSS was field tested by surveying a horizontal borehole. The hole was also surveyed with the Sperry-Sun device. The results of both surveys were fed into a computer and comparisons made between the two. Since the Sperry-Sun device is subject to reader interpretation, the films were interpreted by two readers and their results averaged.

An obvious discrepancy in survey depth between the Sperry-Sun and ENSCO surveys is evident in Figures 12a and 12b. Figure 12a compares the two surveys without a depth correction, while the comparison in Figure 12b includes a 10 ft. depth reduction in the ENSCO survey at the 200 ft. point. The greatly improved correlation between surveys in Figure 12b indicates that an error in survey depth was made and comparison of the ENSCO and Driller's logs reveals that the first survey point on March 16 was taken at 200 ft. but was improperly entered in the ENSCO log as 210 ft., creating the 10 ft. offset. The depth correction was made before final survey data was processed in the computer and is included in the data used in the following discussion.

The inclinations of the two surveys are represented graphically in Figure 13 and the correlation between the surveys is excellent, especially when standard deviation of 1.134° between the two readers of the Sperry-Sun survey is considered. There does exist however a consistent negative bias between the ENSCO and the Sperry-Sun surveys. This bias becomes more apparent when the plots of vertical deviation for the two surveys are compared in Figure 14. The accompanying plot of the difference between the vertical deviation of the two surveys depicts an ENSCO survey bias of about $+0.106^\circ$. Since the ENSCO procedure of taking two readings, separated in rotation at 180° , at each survey point would have removed any internal bias errors, the difference must be attributed to external factors such as the bit rise created by the use of only a front stabilizer or a sag in the non-magnetic extension between the bit

DEPTH CORRELATION COMPARISON

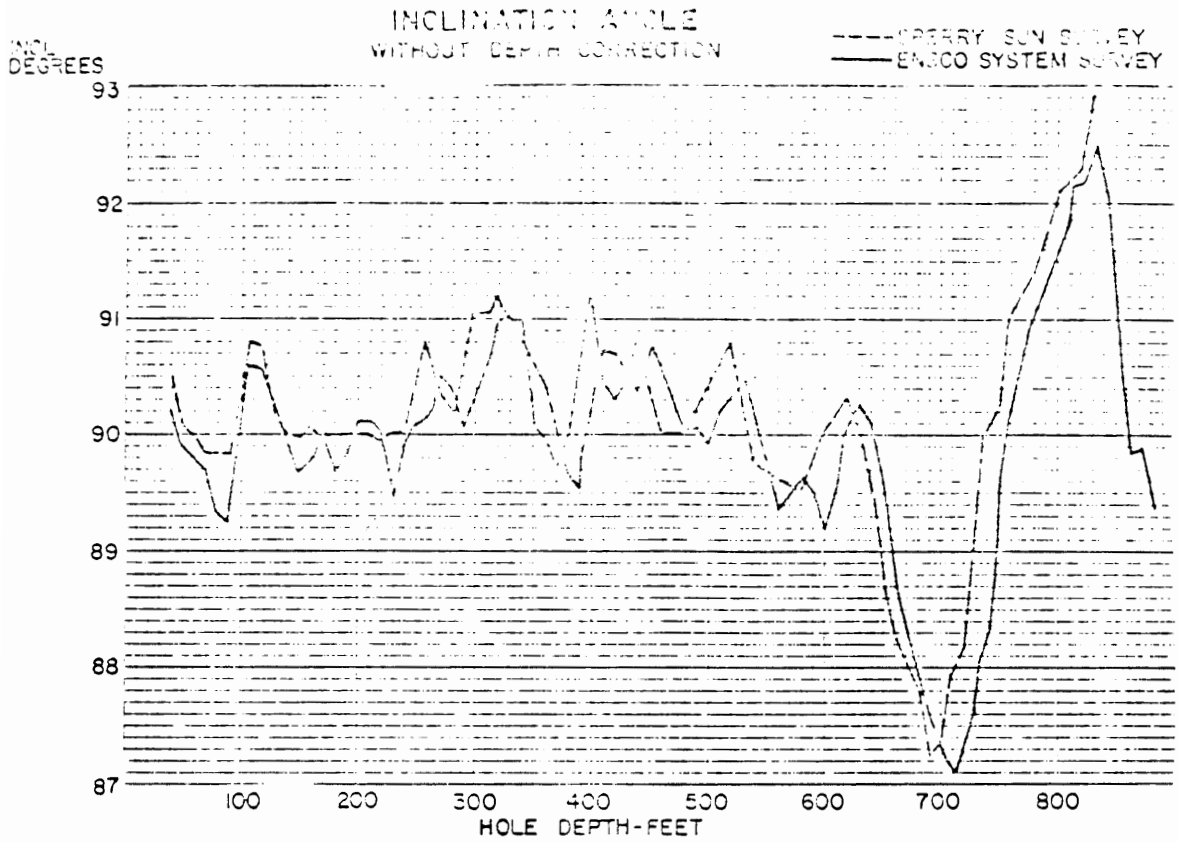


Figure 12a.

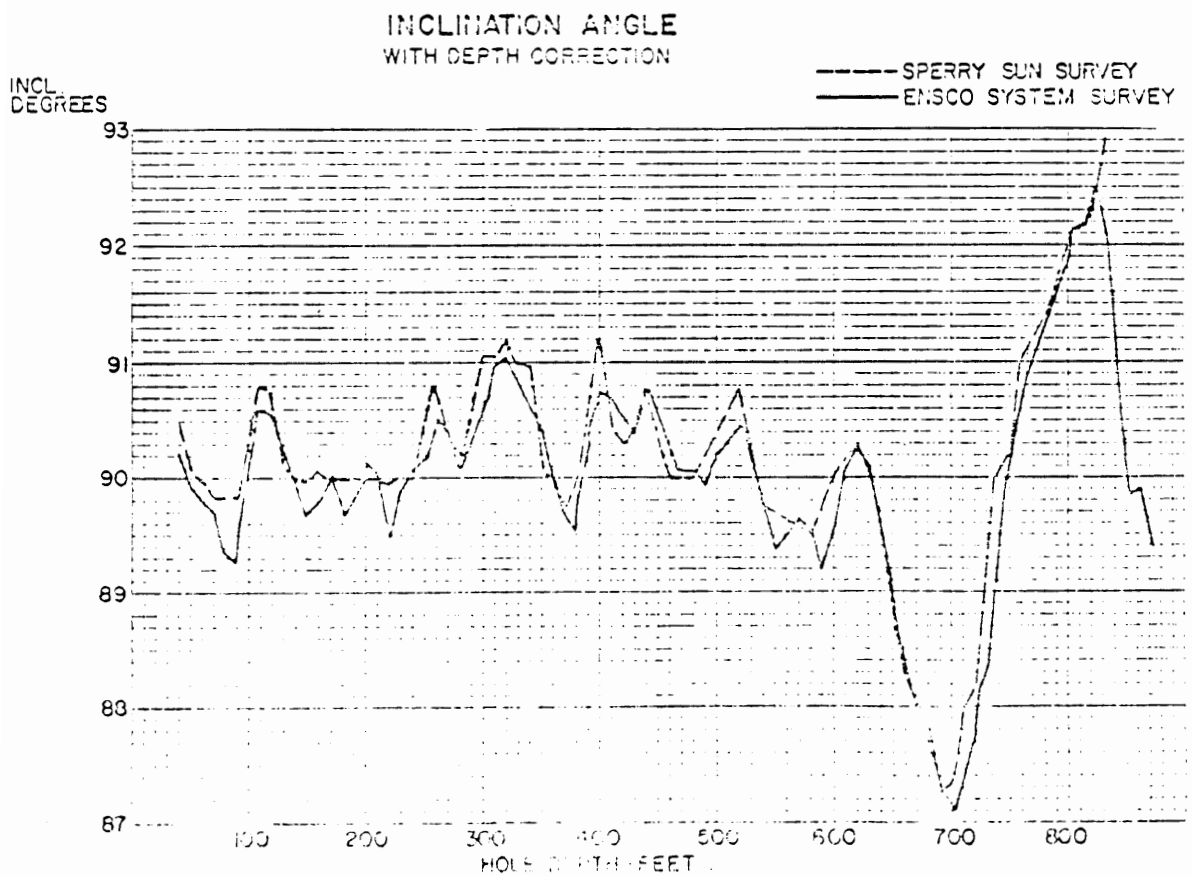


Figure 12b.

INCLINATION ANGLE
ENSCO SYSTEM SURVEY

INCL. 93-
DEGREES

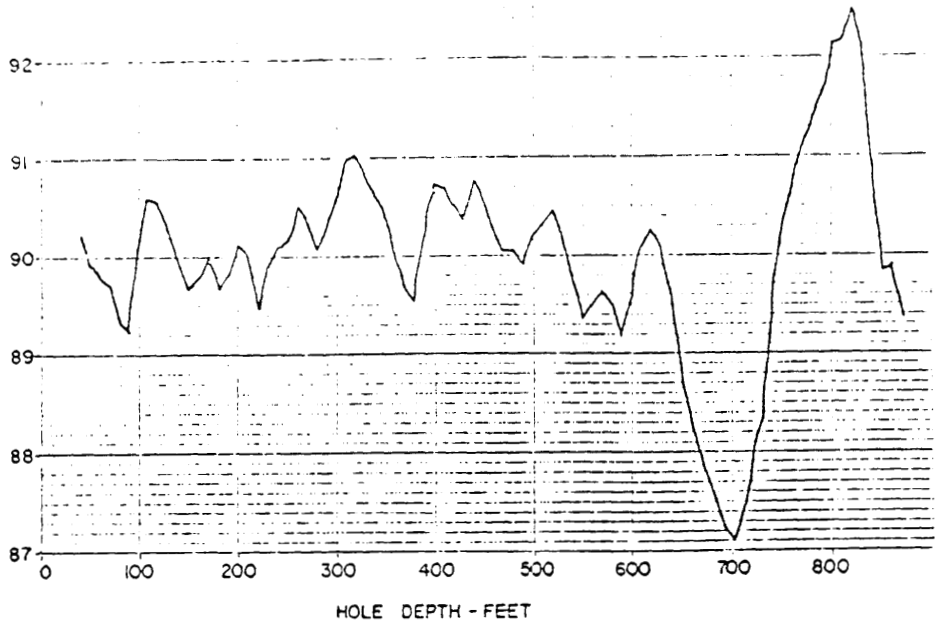


Figure 13a.

INCLINATION ANGLE
SPERRY SUN SURVEY

INCL. 93
DEGREES

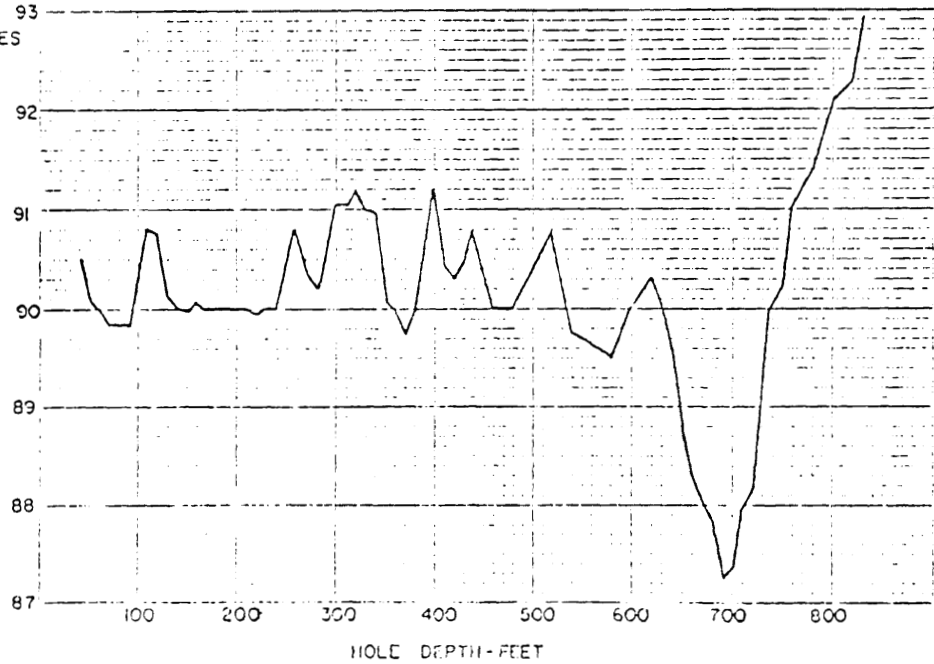
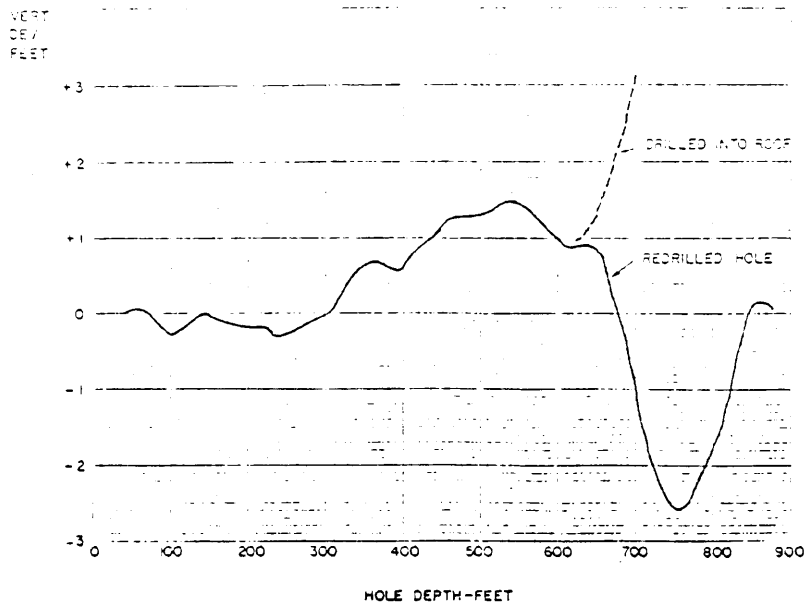
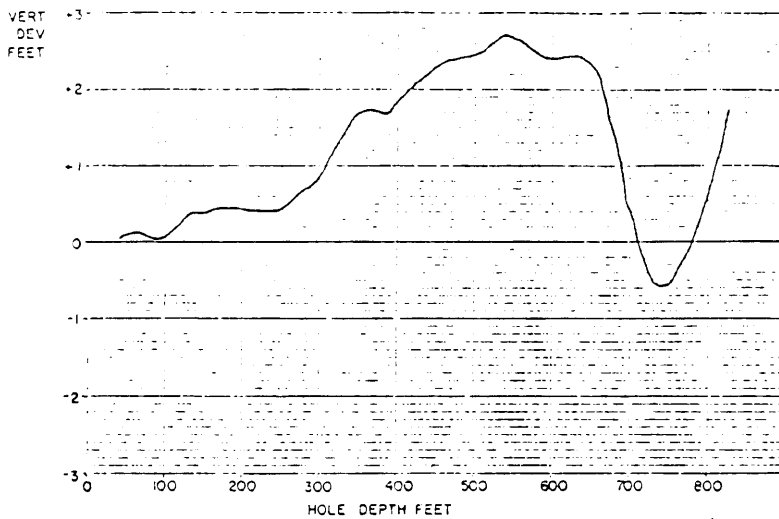


Figure 13b.

VERTICAL DEVIATION OF BOREHOLE
ENSCO SYSTEM SURVEY



VERTICAL DEVIATION OF BOREHOLE
SPERRY SUN SURVEY



VERTICAL DEVIATION
DIFFERENCE BETWEEN ENSCO SYSTEM
AND SPERRY SUN SURVEYS

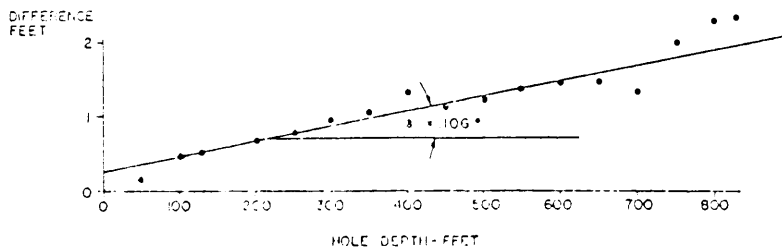


Figure 14

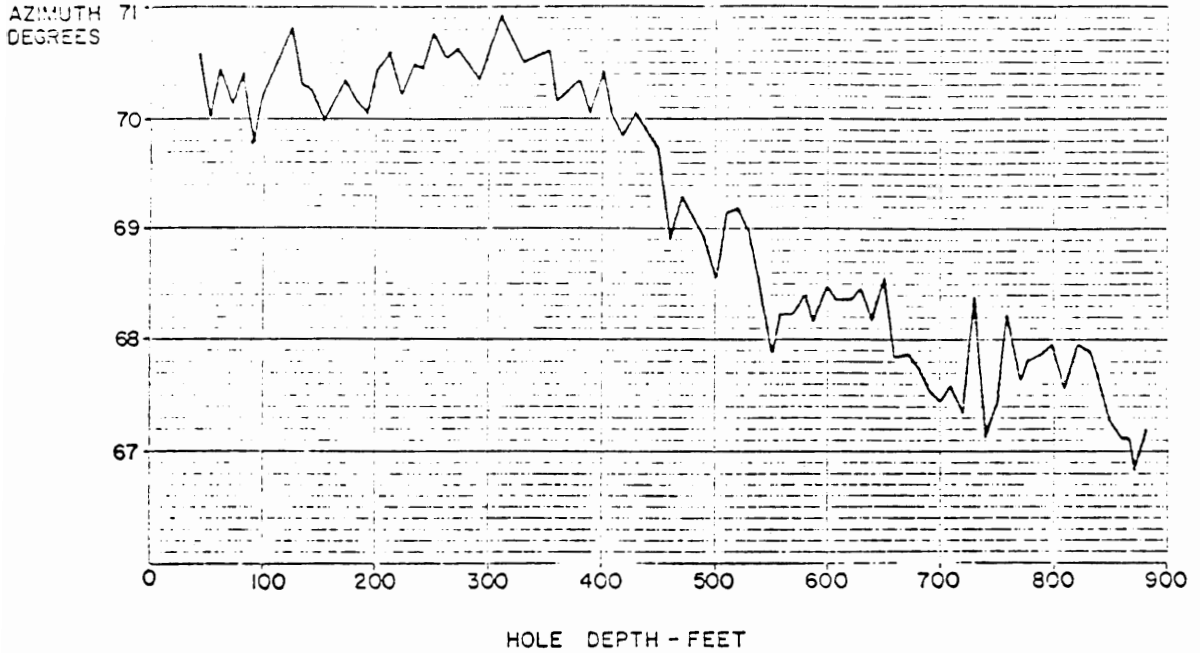
and the sensor system. Even with the bias, the surveys still compare very well with discrepancy of only 2.38 ft. in a 830 ft. hole. The ENSCO plot of vertical deviation includes the plot of the survey when the drill went into the roof and the hole was redrilled.

Azimuth plots for the two survey systems are shown in Figure 15. The Sperry-Sun graph includes a plot of the first survey taken March 17th and a plot of the average of two readers for the final survey. The surveys have some points of discrepancy, but once again excellent overall correlation exists. The lateral deviation plots (Figure 16) are very close with a maximum difference of only 1.17 feet and a difference of only .76 feet at the 830 ft. depth. Only the two reader averages of the final Sperry-Sun survey were used in the deviation plots. It should be noted that a standard deviation of 0.78° exists between the first and second Sperry-Sun surveys and standard deviation of 0.18° exists between the two readers of the final Sperry-Sun survey. The ENSCO survey was also the average of two different survey points as shown in Figure 17. The ENSCO survey procedure was designed to cancel errors by taking two survey points at each depth with an angular package rotation of 180° between points.

The source of the differences between the ENSCO and Sperry-Sun surveys is not clear and the correlation between the two seems more than adequate for this application. It will be noted that the two Sperry-Sun surveys have an initial bias difference between them of approximately 1° . The survey tool was initially aligned against the first Sperry-Sun survey. Since all three runs (2 Sperry-Sun and one Survey Tool run) agree very well except for this bias difference, we are inclined to believe that there is an offset error in the Sperry-Sun tool.

AZIMUTHAL ANGLES

ENSCO SURVEY



AZIMUTHAL ANGLES

SPERRY SUN 2 SURVEYS

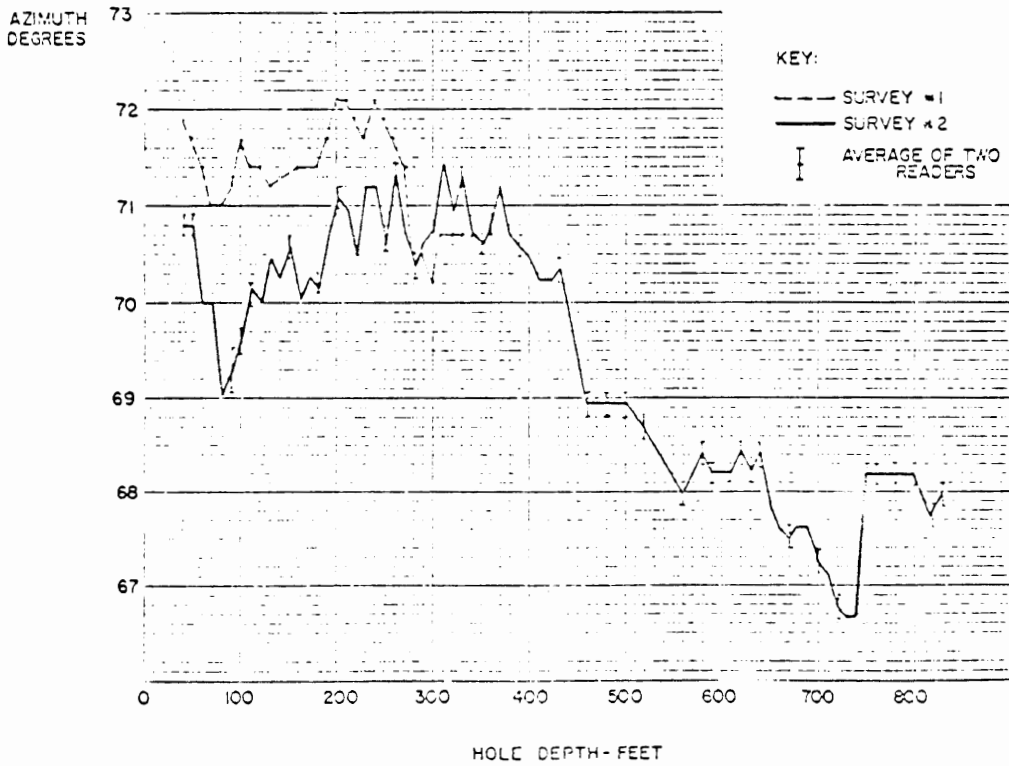
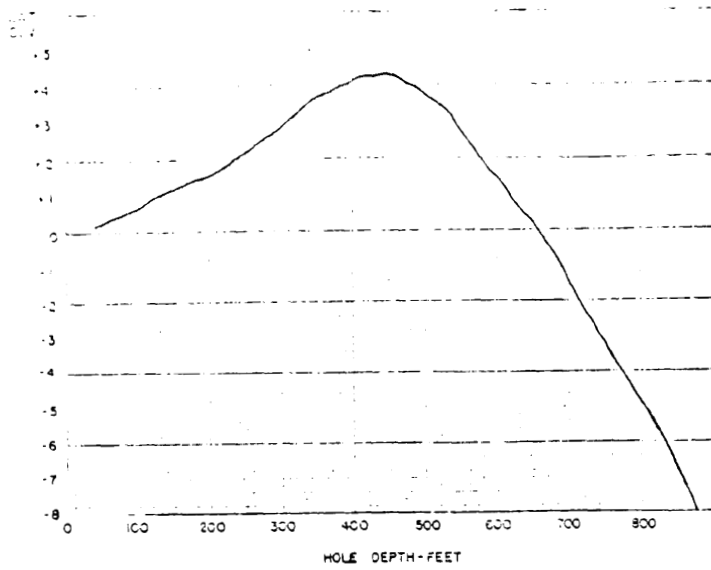
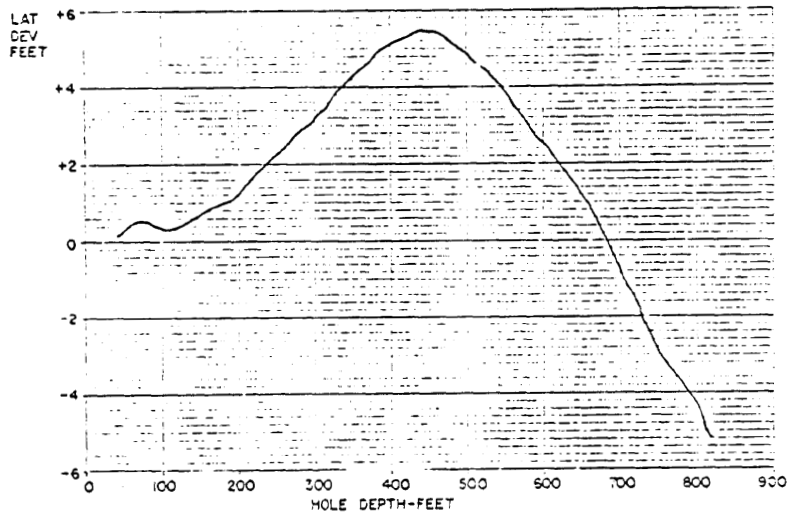


Figure 15

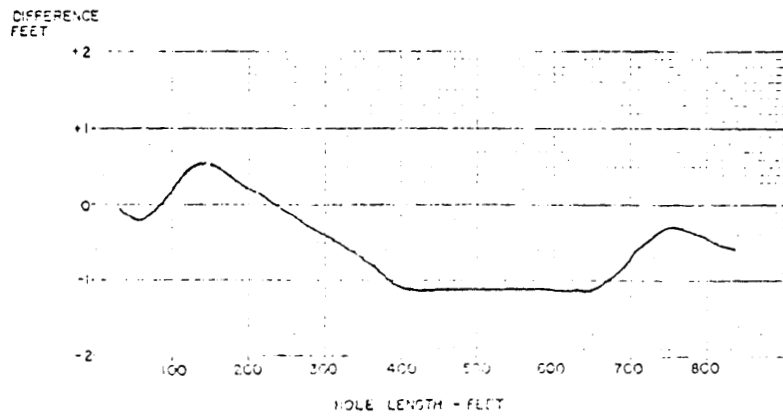
ENSCO SYSTEM SURVEY



LATERAL DEVIATION
SPERRY SUN SURVEY



DIFFERENCE IN LATERAL DEVIATION
BETWEEN
ENSCO SYSTEM SURVEY AND SPERRY SUN SURVEY



SURVEY SYSTEM AZIMUTH

74

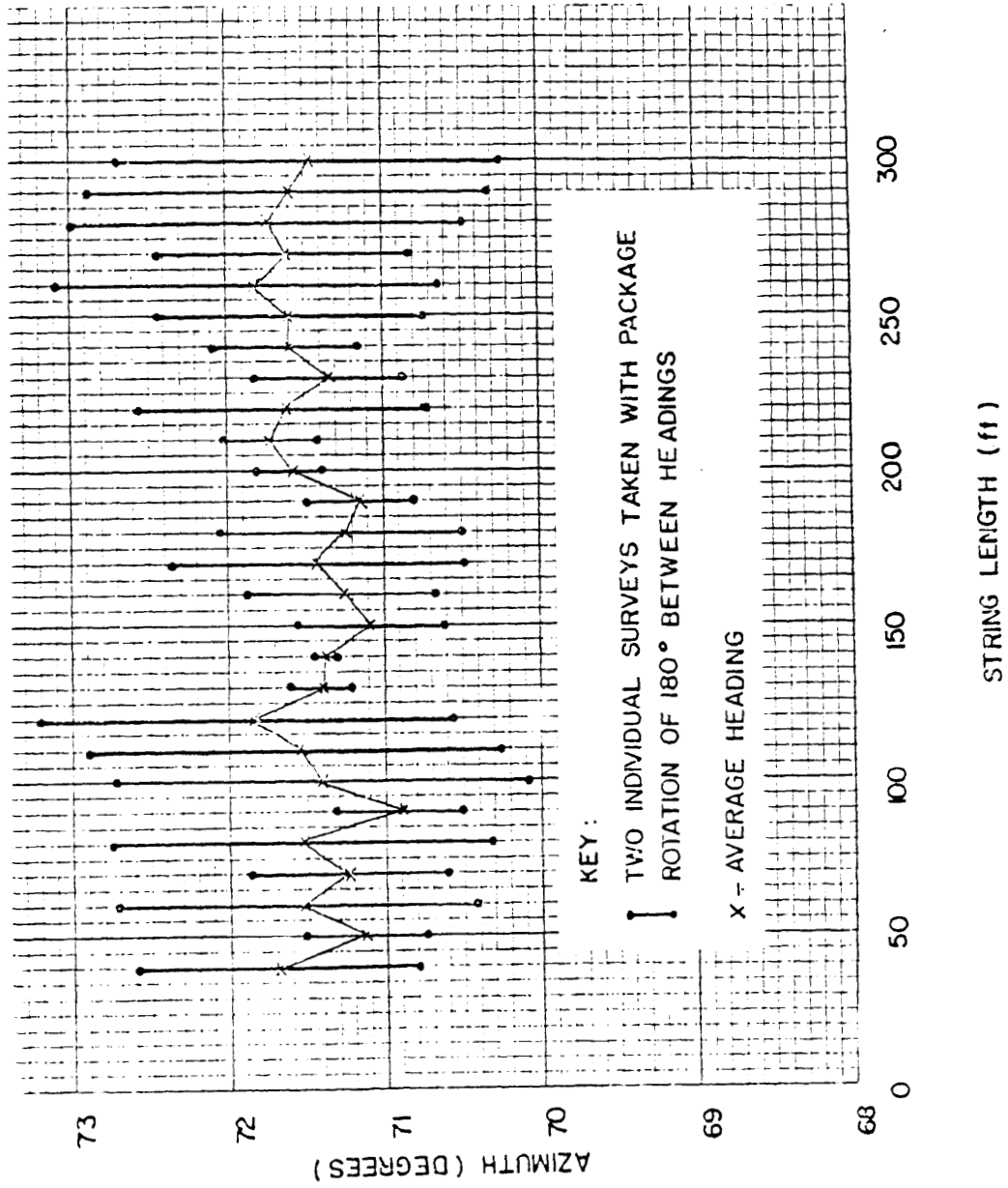


Figure 17

SPECIAL TESTING

During drill operation, significant non-linear variations in azimuth corresponding to angular package rotation were experienced as shown graphically in Figure 18a. The magnitude of these variations prompted a series of tests, relating magnetometer outputs to angular rotation, to define the source of this non-linearity.

The first test involved rotating the assembled inner package through 360° of roll in 10° intervals and triggering the package at each interval. The package outputs were picked up by the receiver, logged and processed in the computer as survey data. The resulting plot of azimuth versus package rotation (Figure 18b) reveals a variation of over +1.5 degrees, indicating the existence of the problem without the outer canister in place. An analysis of the raw data indicated that the previously calculated magnetometer offset factors were no longer valid and a reduction in azimuth variation could be effected by offset correction.

The next step in the elimination process was to physically separate the sensor canister from the electronics canister, while retaining the electrical integrity. The resulting data had slightly less variation with rotation than data taken with the complete package, but the same character was retained, as shown in Figure 18c. The effect of the electronic canister does not appear to be a problem.

The next step was to disassemble the sensor canister, noting the resultant changes in magnetometer outputs associated with each component's removal. The component having the greatest effect was the accelerometer, followed by much smaller but significant changes associated with the magnetometer alignment rods and outer sensor canister itself. Data on the magnetometer alone shows some reduction in azimuth variation

AZIMUTH DIFFERENCE (DEGREES)
 (EACH CASE NORMALIZED TO ITS MEAN AZIMUTH)

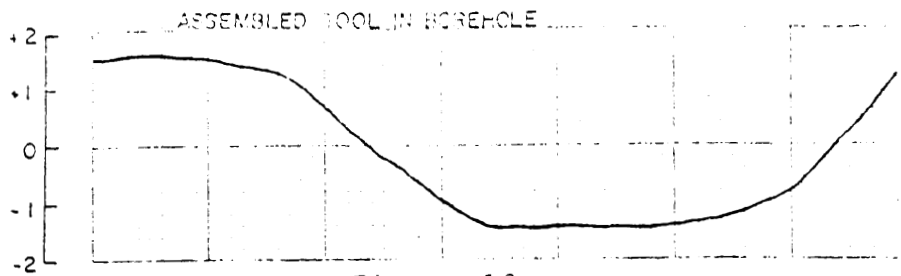


Figure 18a.

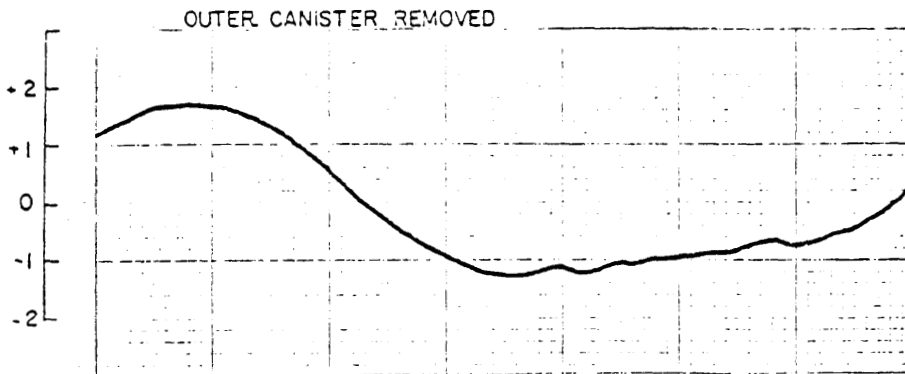


Figure 18b.

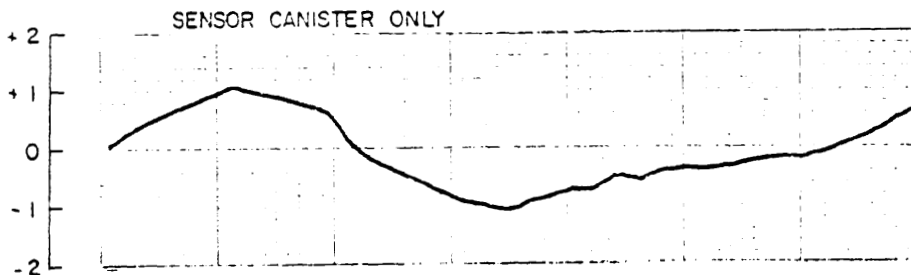


Figure 18c.

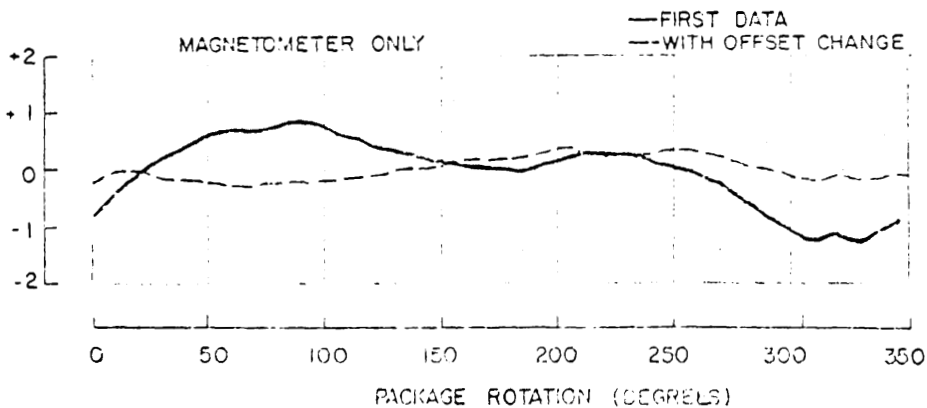


Figure 18d.

with rotation but more importantly the character of the variation was significantly different. This indicated that a change in the magnetic environment of the magnetometer had occurred.

The axis offsets were greatly changed so new offset factors, derived from current experiments, were inserted in the program. The resulting data contains only a $\pm .35^\circ$ variation in azimuth with rotation as shown in Figure 18d. It also possesses a character conducive to further reduction.

An attempt was then made to reduce the errors in previous configurations by appropriate changes in offset factors. A small improvement resulted in each case, but in no case was the error reduced less than $\pm 1^\circ$.

The above testing indicates that either all sources of magnetic abnormalities in the sensor canister must be removed by relocation of components and degaussing or the procedure of taking two measurements at each survey point (with an angular package rotation of 180° between measurements) must be continued.

There was no requirement to investigate the potential limits of accuracy of this type of tool. However, the question of limiting accuracy of a magnetic tool is often asked. Figure 19 is a plot of heading degrees versus the rotational angle of the drill string taken over a reasonably straight section of the hole. An envelope containing the majority of these points is shown as the solid line. The mid point of this envelope is shown as the dotted line. The mean of all points with respect to the dotted line is 7.5×10^{-3} degrees. The standard deviation, σ , is $.146^\circ$. The low value of the mean indicates that the dotted line represents a systematic variation which, with sufficient design or computational effort,

HEADING VS ROTATIONAL ANGLE

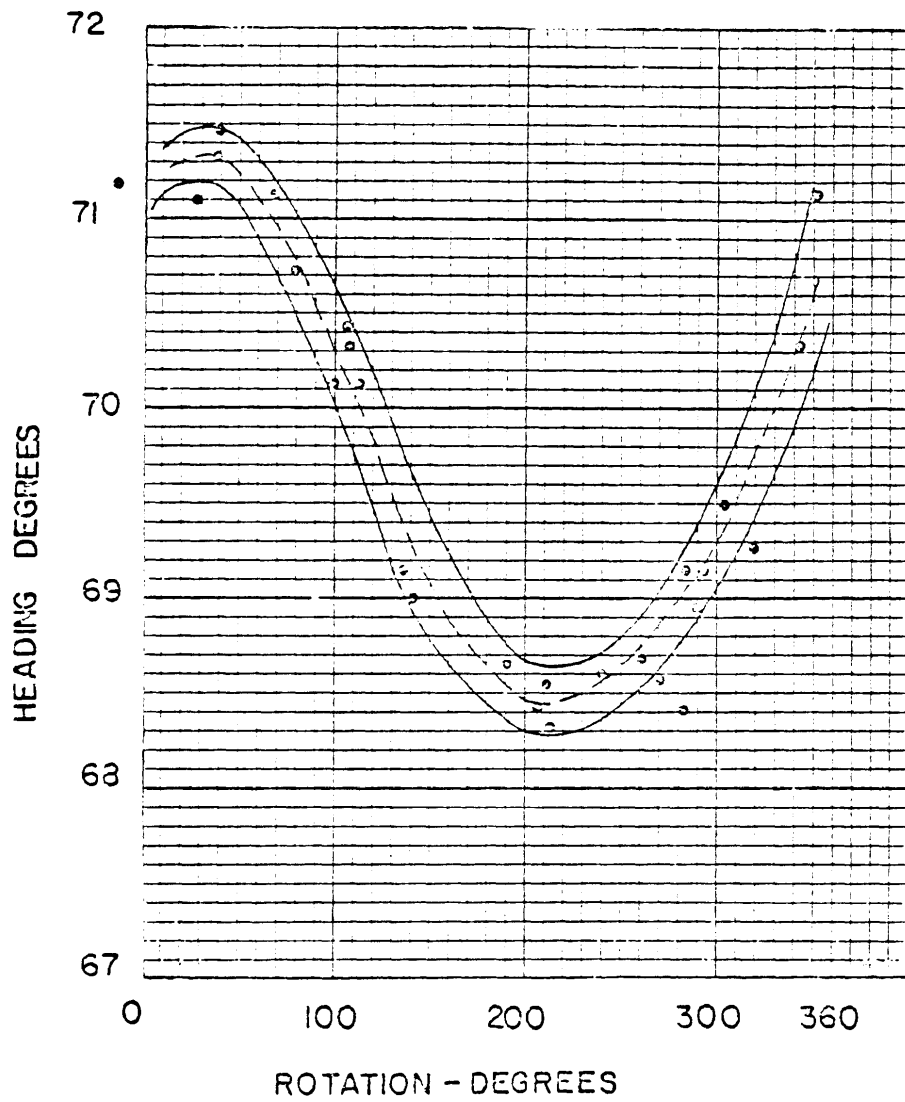


Figure 19

could be removed. The σ of $.146^\circ$ includes both actual changes in hole direction and statistical scatter of points. This indicates that a system such as this with an accuracy of better than $\pm .1$ degree is feasible.

ERROR ANALYSIS

CALCULATION OF LOCATION VECTOR

The RDS-500 computer was programmed to calculate the direction vectors for the down-hole package using the inputs from the package. In order to test these routines and to study the sensitivity of the calculations, simulated data was input to the programs.

Before discussing the results, the following terms must be defined:

- α = dip angle of the magnetic vector
- θ = dip of package with respect to the horizontal
- ϑ = angle of package with respect to magnetic North
- ψ = angle of rotation of a tick on the package with respect to vertical.

Using this terminology and the equations described in the proposal, we calculated θ , ϑ , and ψ given α and the direction cosines from the magnetometers and the accelerometer reading.

As was discussed in the proposal, when ϑ was near 0° or 180° (i.e. north or south), the calculations become more difficult. To show this, Figure 20 shows the standard deviation of the error from 100 runs of each direction when noise is added to the magnetometer channels. The amount of noise is comparable to a Gaussian white noise with a standard deviation of $1/2$ degree. The error in ϑ is small (below 1°) for directions between 20° and 160° . However, the error goes up near the north or south directions. This is because ϑ is calculated as an arc cosine function. This has more error near these values and also it is impossible to tell when the reading corresponds to negative angles.

The ambiguity of negative angles of ϑ is impossible to resolve without an additional sensor on board. No combination of

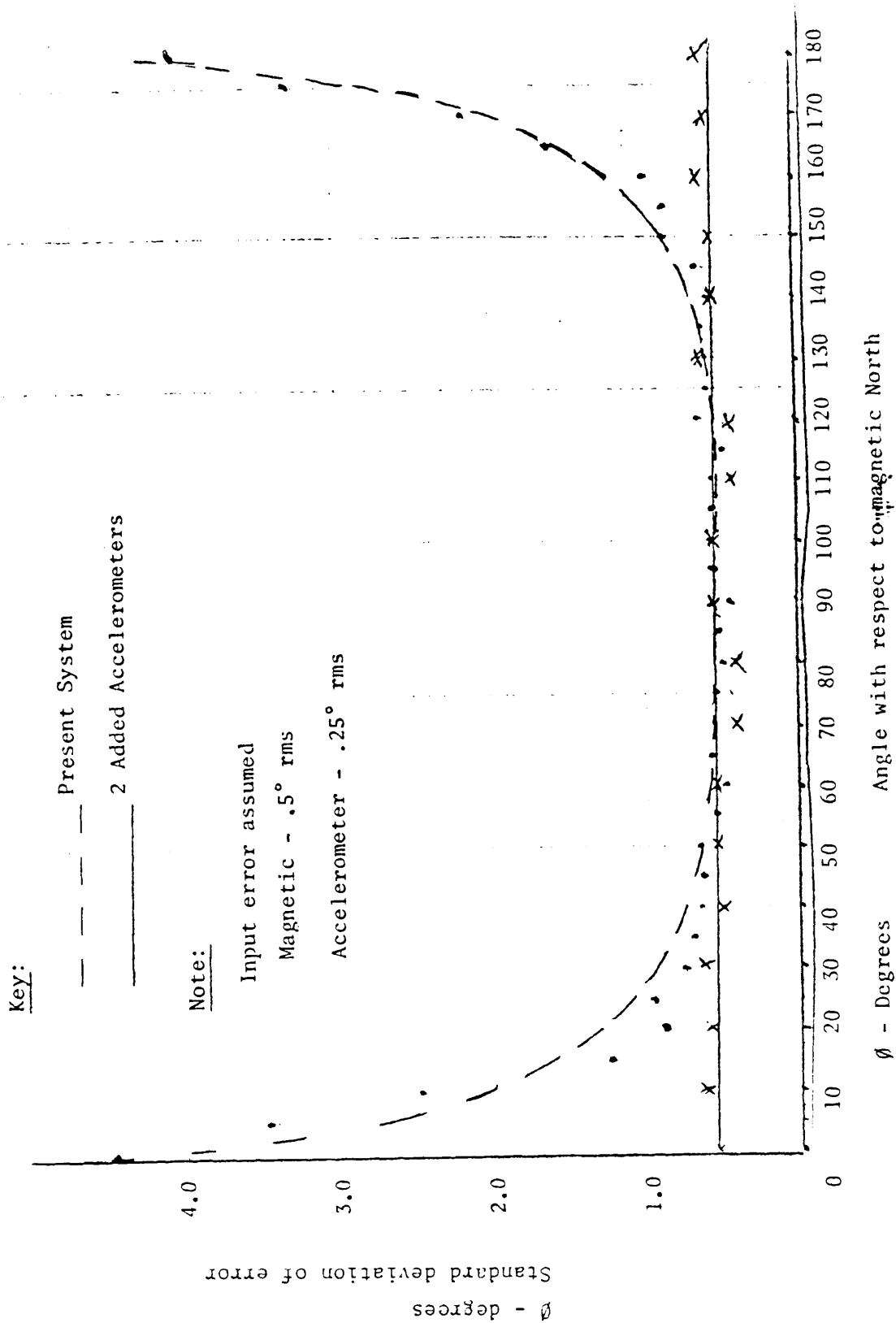


Figure 20. RMS Heading Error Vs. Heading Angle

mathematical tricks or package rotations can resolve this ambiguity.

As discussed in the proposal, two additional ambiguities exist. When the package is aligned with the magnetic vector, it is impossible to resolve the angle ψ . The final ambiguity exists when $\theta = 90^\circ$ (i.e. drilling in a vertical direction).^{*} Figure 21 shows this result. This figure is a plot of the error in θ as a function of θ for $\psi = 90^\circ$.

The ambiguity of not knowing whether the package is pointing west or east of north can be relieved by telling the system the initial direction as was done previously. However, if the direction is close to the North direction small measurement errors will cause larger direction errors.

The system was next programmed for the equations using two added accelerometers. The comparative error curves are shown on Figure 1. This step would reduce all errors due to geometrical factors with the possible exception of the elevation angle. Although we have not investigated it in detail, it is believe that even these errors could be eliminated using alternate algorithms. The added accelerometers also eliminate the ambiguities which exist in the present system.

^{*}It should be recorded however that the system was never intended for vertical work. The original specification in fact limited the angles to horizontal, plus or minus 45° . Thus, the ambiguity associated with drilling along the magnetic vector was prohibited.

$\alpha = 45^\circ$
 $\psi = 0$
 $\theta = 90^\circ$

88°

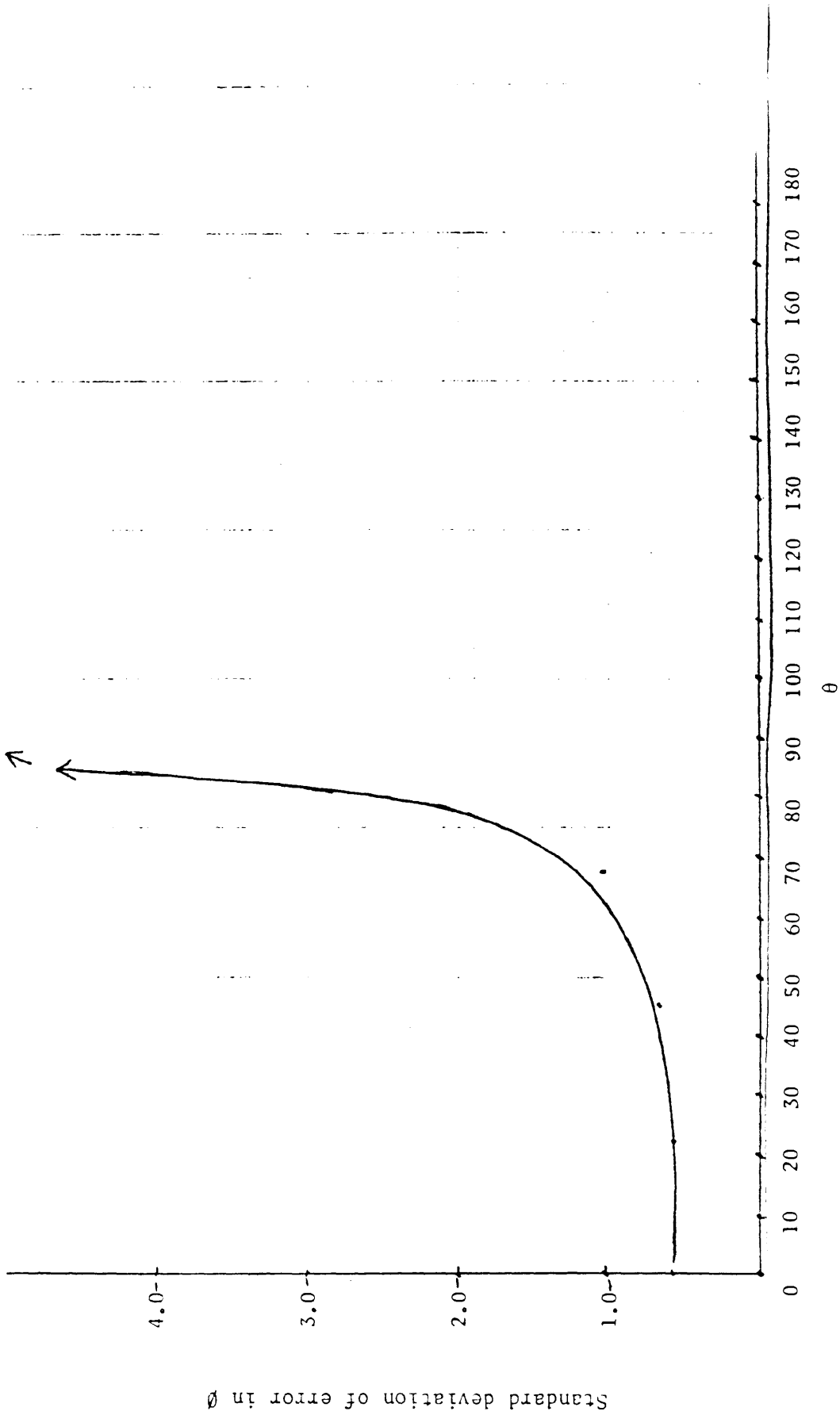


Figure 21. RMS Elevation Error Vs. Elevation Angle

APPENDIX B
CABLELESS SURVEY SYSTEM DOWNHOLE TOOL SPECIFICATIONS

CABLELESS SURVEY SYSTEM DOWNHOLE
TOOL OUTPUT SPECIFICATION

Carrier Frequency: 4.0527KHz \pm .005% Crystal Controlled

Transmitter Output Power: 1 watt nominal to input of trans-
mit Toriod) varies with coupling
conditions)

Modulation: Manchester Code \pm 60° Phase Modulation

Data Rate: 31.66Hz = Carrier divided by 128

Transmitter Sequence: 16 Seconds 0° Phase Shift Carrier
4 Seconds All 1's data
32 Bits Preamble
30 Bits Random Data (Not Used)
130 Bits Ten 12 Bit Data Channel
Parity

- Upon triggering the downhole tool transmits 16 seconds of 0° phase shift carrier (no modulation) which is used by the receiver to establish carrier phase lock and auto gain range.
- The downhole tools follows the carrier with 4 seconds of all 1's data which is used by the receiver to establish the data clock phase lock.
- The downhole tool follows the all 1's with a 32 bit preamble which the receiver uses to acknowledge that the upcoming data is real and prepares to alert the microprocessor.

The preamble code is:

10110000110111001011000011011100

If the exact code is not recognized, the receiver will ignore the remainder of the transmission.

- The next 30 bits of data transmitter are sent to the microprocessor but are thrown away as meaningless.

Transducers:

1) "Z" Axis Accelerometer:

Manufacturer: Sunstrand Data Control

Model: QA 116-15

Range (Full Scale)	±15/g
Sensitivity (Nominal)	250 mV/g
Output Resistance (Nominal)	250 ohms
Frequency Response (Nominal, ±5%)	DC to 500Hz
Natural Response (Nominal)	100Hz
Noise (Nominal): 0 to 10Hz	100 µV rms
0 to 500 Hz	300 µV rms
500 to 10Hz	600 µV rms
Broadband	1 mV rms
Excitation Voltage	±15 VDC ±10%
Excitation Current	17 mA quiescent, 35 mA full scale
Sensitivity Shift with Excitation Voltage	0.005%/V
Zero Shift with Excitation Voltage	50 µg/V
Resolution (DC)	0.000001 g
Threshold (DC)	0.000001 g
Linearity (DC)	0.03% of reading
Hysteresis (Less Than)	0.001% of full scale
Repeatability	0.003% of full scale
Zero Unbalance (Less Than)	±0.02 g
Damping Ratio (Approx) (3)	0.6
Thermal Zero Shift (Max)	0.0002 f/°F
Thermal Sensitivity Shift (Max)	0.01%/°F
Transverse Sensitivity	0.002 g/g

2) X and Y Axis Accelerometer

Manufacturer: Terra Technology
Model: MP-200A

Range: ± 1 g (minimum)
Scale Factor: 8.5 VDC/g $\pm 0.5\%$
Null Offset: < 0.020 volts
Temperature Coefficient: 0.01% of FS/ $^{\circ}$ F (Max)
Linearity: $\pm 0.02\%$ of Full Scale
Hysteresis and Resolution: 0.0001% of Full Scale
Turn-on to turn-on Repeatability: < 2 mv
(no tapping allowed)
Axis Alignment (WRT Case): $\pm 0.50^{\circ}$
Biaxial Orthogonality: $\pm 0.25^{\circ}$
Output Impedance: $< 15,000$ ohms
"A" Axis to be aligned to 8-32 Hole within 0.5°
Excitation Voltage: ± 10 to ± 15 V
Excitation Current: ± 24

3) Tri Axis Magnetometer

Manufacturer: EMCO
The Electro Mechanics Company
Model: 6713

Range: ± 0.7 Gauss
Scale Factor: .14 Gauss/volt (± 5 V)
Resolutions: $\pm 0.5^{\circ}$
Excitation Voltage: ± 13 to ± 18 VDC
Excitation Current: 60ma max
Voltage Ripple: $\pm 5\%$

Batteries:

Manufacturer: Gould Inc.
Model: 2.2SC (1/2D) NiCad
Quantity: 24

APPENDIX C

CABLELESS SURVEY SYSTEM TEST PLAN
AND TEST RESULTS

This Appendix C contains the test plan submitted to the USBM in September 1978. Immediately following the plan is the results of the system test and description of any deviations which were noted.

TEST PLAN FOR CABLELESS SURVEY SYSTEM

1. DESIGN REQUIREMENTS

A. Check to verify that the following are displayed:

<u>YES</u>	<u>NO</u>	
<u> </u>	<u> ✓ </u>	● Bearing in degrees and minutes
<u> </u>	<u> ✓ </u>	● Inclination in degrees and minutes
<u> ✓ </u>	<u> </u>	● Rotation Angle in degrees
<u> ✓ </u>	<u> </u>	● Horizontal deviation in feet
<u> ✓ </u>	<u> </u>	● Vertical deviation in feet
<u> ✓ </u>	<u> </u>	● Drill string depth

B. Verify that the following can be entered from the keyboard:

<u>YES</u>	<u>NO</u>	
<u> ✓ </u>	<u> </u>	● Magnetic dip angle
<u> ✓ </u>	<u> </u>	● Initial bearing
<u> ✓ </u>	<u> </u>	● Number of drill rods

C. Verify that hard copy can be produced from data received from the downhole unit.

<u>YES</u>	<u>NO</u>
<u> ✓ </u>	<u> </u>

D. Verify that self-checking can be performed on the:

<u>YES</u>	<u>NO</u>	
<u> ✓ </u>	<u> </u>	● Receiver
<u> ✓ </u>	<u> </u>	● Computational circuitry

E. Verify that data error detection and warning capability is functioning

YES NO

✓ —

F. Verify the following physical requirements:

YES NO

✓ —

● Weight, approx. 40 lbs.

● Size

Width 13-3/4 inches

Height 14-1/4 inches

Depth 11/7/16 inches

✓ —

● Unit's own carrying case with

Protective cover

Handle

— ✓

● Does handle serve as means to position and display at various viewing angles?

✓ —

● Is transit case supplied?

G. Is the unit intrinsically safe as defined in MESA Schedule 2G?

YES NO

✓ —

● Does the system operate from an external 12-volt automobile battery?

H. Is the electronic construction of modular design to allow rapid repair?

YES NO

✓ —

2. RECEIVER TESTS

Equipment necessary for this test will include a down-hole transmitter link emulator. This emulator will generate lock and transmit signals in strict accordance with those transmitted by the down-hole package at a carrier frequency of 4.0525 KH \pm .02%. The data field will be missing, however. It will also contain a white noise generator and a means to sum the two outputs. The signal should have a range of -30 μ v to 3v (100 dB) in 10 dB steps and the output noise levels should be adjustable to -3 dB below the signal. If a signal is properly received and decoded, the computer will detect the preamble and generate a "data error" signal because of the absence of the data field.

Procedure

1. With a full battery charge, turn the unit on and verify proper operation with Self-Test function.
2. Connect the emulator to the receiver input and begin the tests with a signal level of 50 μ v and a noise level of -3 dB, at a carrier center frequency of 4052.5 Hz. Send the preamble five times and note presence or absence of data error indication.
3. Repeat Step 2 nine more times, each time increasing signal and noise levels +10 dB.
4. Repeat Steps 2 and 3 for 4052 Hz and 4053.5 carrier center frequencies.
5. Measure receiver battery voltage and note elapsed test time.

NOTE: If at any time there is a low battery voltage indication in the computer section, stop the test and recharge those batteries.

Record

1. Any conditions under which an error is not detected.
If any preambles are sent (under allowable conditions) that do not cause data error indications, the receiver problem must be corrected and the tests run again from Step 1.

2. Results of Step 5.

3. BATTERY LIFE TESTS

The purpose of this test is to determine whether the unit will operate for six hours continuously, given a reasonable set of operating conditions.

Procedure

1. Charge the batteries normally, and measure the resultant battery voltage.
2. Apply the proper preamble from the emulator to the receiver every 15 minutes and check for data error indication. Every hour, operate the self test function and then measure battery voltage.
3. After six continuous hours, continue the test, measuring battery voltage every 15 minutes until that voltage indicates a cell voltage of 1.1v, or until a malfunction occurs.

Record

1. Results of Step 3 versus time of day.
2. Results of Step 4 versus time of day, and condition of battery voltage indicators.

Preface

"The unit" will refer to the processing and display system.

4. ENVIRONMENTAL TESTS

4.1 IMMERSION

The purpose of this test is to prove compliance with Mil-Std-819C Method 512, Procedure 1.

Procedure

1. Obtain a clean vessel with a cross section large enough to accept the unit and a total height of 48", and fill with water at $18^{\circ} \pm 5^{\circ}\text{C}$ to within 10" of the top.
2. Remove all internal components from the unit that are not secured with external fasteners.
3. Heat the unit, cover open, in a temperature chamber, for two hours at $45^{\circ} \pm 3^{\circ}\text{C}$.
4. Open and close the cover three times, then secure it with the built in latches.
5. Submerge the unit, as modified in Step 2, to the bottom of the vessel, using a method that will restrain the buoyancy of about 100 lbs. without damage to any part of the unit.
6. After 120 ± 5 minutes, remove the unit from the water and wipe the exterior surfaces dry.
7. Open the unit and inspect the interior and contents for evidence of leakage.

Record

1. Location and approximate amount of interior moisture observed in Step 7.

4.2 SHOCK TESTS

The purpose of this test is to prove compliance with Mil-Std-810C, Method 516.1, Procedure II, Transit Drop Test.

Procedure

1. Provide a test bed of 2" plywood, with greater cross section than the unit's transit case, on a concrete base.
2. Place the unit in its transit case and secure properly all closures.
3. From a height of 48" above the plywood surface, drop the case on each face, edge, and corner for a total of 26 drops.
4. Run the unit through all initial tests (Steps 1 and 4 of Receiver Testing).

Record

1. Results of Step 4.
2. Any observable physical changes in the transit case, foam packing, or the unit itself.

4.3 OPERATING TEMPERATURE TESTS

The purpose of this test is to verify operation of the unit over the specified range of 0°C to 50°C.

Procedure

1. The unit will be turned on and the specified warm up time allowed to elapse. Test conditions will be entered into the processor on the keyboard.

2. The unit will be placed in a chamber with a viewing port in the front, of sufficient size to view the display, and with a means to allow signal lines from the normal receiver input to be led out of the chamber.
3. Connect the emulator to the receiver input with an input level of 500 μ v and a noise level -6 dB and a carrier frequency of 4052.5 Hz.
4. Send preamble and record presence or absence of data error indication. NOTE: Presence of data error verifies proper decoding of preamble.
5. Repeat Steps 3 and 4 at carrier frequencies of 4053 Hz and 4053.5 Hz.
6. Temperature of the chamber will be lowered to 0°C and allowed to stabilize for one hour.
7. Repeat Steps 3-5.
8. The temperature of the chamber will be raised to +50°C and the unit allowed to stabilize for one hour.
9. Repeat Steps 3-5.

Record

1. Operating conditions and results of each Step 4 test.

4.4 TEMPERATURE SHOCK TEST

The purpose of this test is to prove compliance with Mil-Std-202E, Method 107D,A, as modified to protect certain components and conserve testing time. Specifically, the liquid crystal display and the batteries are not specified to withstand the high temperature extreme of 80°C. The display, the batteries, the DC/DC converters, the keyboard, and the printer will not withstand the low temperature extreme of -55°C. The batteries, converters, and display are not easily removed. The display has the narrowest range, namely -20°C to +70°C, so we are modifying this thermal shock test to be performed over that range.

Procedure

1. The unit, with cover closed, will be placed in a temperature chamber cooled to -20°C for four hours, with no more than five minutes elapsed if it is being cooled from the high temperature.
2. The unit is then heated to +70°C, with no more than five minutes in the transition from -20°C, where it will remain for four hours.
3. Steps 1 and 2 are each performed a total of five times in sequence.
4. At room temperature, turn the unit on, allow time to warm up, then perform the Receiver Test Section, Steps 1 and 5.

NOTE: If the unit weight is below 30 lbs., times at temperature extremes may be reduced to two hours each.

Record

1. Results of Step 5.
2. Any physical changes evident on post test inspection.

4.5 HUMIDITY TEST

The purpose of this test is to prove compliance of the unit with Mil-Std-810C, Method 507.1, Procedure I, as modified by ENSCO to conserve costs.

Procedure

1. Full charge the unit batteries, remove the protective cover, and connect a dummy connector to the receiver input. Install the connector caps for the power and computer connectors.
2. Place the unit in the temperature chamber and slowly raise the temperature and humidity over a period of two hours to 65°C and 92% r.h., respectively.
3. Maintain the condition of Step 2 for six hours.
4. Open the test chamber and allow it to stabilize at room temperature.
5. Operate the self-test and note proper response.

Record

1. Results of Step 5.
2. Any physical changes noted in the unit.

5. FIELD SURVEY TEST

This test will demonstrate the integrity of the system as a whole. Several compass points and package inclinations will be surveyed and compared with coincident transit readings. Transit accuracies will be kept to $\pm 0.01^\circ$.

Procedure

5.1 INITIAL MEASUREMENTS

1. Assemble the cableless survey tool with all batteries at full charge.
2. Run Self-Test.
3. Position and level the tool at due magnetic north (0°) and trigger the package.
4. Check the axis alignment offset constants and monitor housekeeping data from the down-hole package.
5. Initiate dip calculation on computer. NOTE: In the following steps, use the external control panel of the computer to read out sensor readings for each point desired.
6. Align the package with an elevation of -1° , and a heading of 0° , and take readings for the following package rotations: 0° , 45° , 90° , 135° , 180° , 225° , 270° , and 315° . Use a transit at each point for a reference reading.
7. Repeat Step 6 for an elevation of 0° .
8. Repeat Step 6 for an elevation of $+1^\circ$.
9. Repeat Steps 6, 7, and 8 at a heading of 90° .

5.2 SIMULATED DRILLING TRAJECTORY TEST

10. Align the package to 0° heading. Perform 10 random alignments within the range of 359° to 1° (heading) and -1° to 1° (elevation) to simulate the drilling operation. Each point will be entered into the processor as though it were 10' of drill rod from the previous point. Take transit readings of each point for reference.
11. Repeat Step 10, but within the heading range of 269° to 271° .
12. Calculate the simulated course from the transit readings. Then compare with the survey tool results.

Record

1. Results of Steps 2, 4, and 5.
2. Sensor readouts and corresponding transit reading for each of the 24 points in Steps 6, 7, 8, and 9.
3. Results of Steps 10 and 11.
4. Deviations from actual course derived in Step 12.

5.3 DRILLING TESTS

This test will insure that the cableless survey tool operates to design specifications in the actual drilling environment.

Procedure

Initial Measurements

1. Complete assembly of cableless survey tool, with all batteries fully charged, at the surface site of the chosen drilling location.

2. Initiate Self-Test.
3. Trigger the package transmission and determine the mechanical offset of the assembled package.
4. Determine local dip angle, using the computer.

Installation in the Mine

5. Set up the driller console (processing and display subsystem) in the mine. Be certain that connector caps are installed on power and computer connectors.
6. Enter initializing data.
7. Install receiver transducer.
8. Initiate Self-Test.

Initial Survey

9. Perform a Sperry-Sun Multi-Shot survey of the existing portion of the hole.
10. Survey the existing hole with the cableless survey tool. At each 10-foot measurement, stop the drill and trigger a transmission. Then rotate the package $180^\circ \pm 10^\circ$ and trigger another transmission.
11. Compare the results of Steps 9 and 10.

Drill and Survey

12. Continue drilling and survey every 10', as in Step 10, to a depth of 1500'.
13. Remove the tool and survey the new hole drilled in Step 12 every 20 feet, using the Sperry-Sun Multi-Shot.

14. Compare the results of Steps 12 and 13.

NOTE: Recharge the batteries and service the printer at the end of each day's operation or sooner if required. Compare daily results with printer output.

Record

1. Results of Step 2.
2. Results of Steps 3 and 4.
3. Results of Step 8.
4. Enter log obtained in Step 9, including house-keeping data from the down-hole package.
5. Parameters of bearing, inclination, angle, horizontal and vertical deviation, drill string depth, and true depth for each point in Step 10.
6. Results of Step 12, as above.
7. Enter log obtained in Step 13.

DEVIATIONS FROM TEST PLAN

1. DESIGN REQUIREMENTS

- 1.A Bearing and inclination angles are displayed as decimal degrees - example: Bearing + 69.28° rather than degrees and minutes.
- 1.B No Deviations
- 1.C No Deviations
- 1.D No Deviations
- 1.E No Deviations
- 1.F All requirements are met except that handle cannot be used to position unit at various display angles.
- 1.G The system is designed to be intrinsically safe, although as of this date, the uphole processor has not completed certification by MSHA. The downhole tool's explosion proof housing was retained unaltered and continues to remain certified explosion proof.
- 1.H No Deviations

2. RECEIVER TEST

Under this contract no downhole emulator was constructed. Internal self test in the receiver/processor were included within the uphole unit. This self test does include a complete simulation of carrier lock, preamble recognition and data verification.

The receiver was tested using the downhole breadboard unit. Signal to noise ratios from 0dB to +6dB was inserted in the input of the receiver with a signal level of 3 μ v and 30 μ v. At 30 μ v no errors occurred above a signal to noise ratio of +2dB. At a signal level of 3 μ v phase shift which occurred during the auto gain ranging did not always allow adequate

time for the carrier phase lock loop to stabilize thereby prohibiting the preamble from being detected. This problem was corrected by employing wider bandwidth amplifiers in the auto gain ranging section of the receiver. After this correct transmission was received without error with a signal to noise ratio of +3dB.

At 30 μ v signal level some data was received without error with a signal to noise ratio of 0dB. However, since less than 90% of the transmissions were correct, the false alarm or error detection rate was deemed to high. It should be noted that in more than 90% of the cases when the preamble is recognized all data is transferred without error. Conversely, since the receiver does not indicate a data transmission unless the preamble is recognized, very few bad transmissions are even detected.

3. BATTERY LIFE TEST

The battery life test was performed for six continuous hours, at which time the receiver battery was automatically disconnected due to low voltage (as designed). Four data errors were encountered during that time, but this was due to inadvertently not terminating the receiver input.

4. ENVIRONMENTAL TESTS

4.1 Immersion

No interior moisture was evident.

4.2 Shock Tests

Deleted by Contract Modification.

4.3 Operating Temperature Tests

At 0°C, there was no data errors using the self test, the LCD display was slow but functional, and the printer performed properly. At 50°C, there was no data errors using the self test and all other devices functioned normally.

4.4 Temperature Shock Test

As noted before a downhole survey tool emulator was not produced. Therefore, the self-test function was used. After the cycling and at room temperature, all systems functioned properly with no errors. No physical changes were evident.

4.5 Humidity Test

The proper response was obtained from the self test.

5. FIELD SURVEY TEST

5.1 Initial Measurements

See Figure - Magnetometer output for Y axis and Z axis for rotation about X axis.

See Figure - Accelerometer output for Y axis and Z axis for rotation about X axis.

See Figure - Magnetometer output for Y axis and X axis for rotation about Z axis.

5.2 Simulated Drilling Trajectory Test

The simulated trajectory test was done by placing a pattern of nine holes in a board as shown below:

●2	●3	●4
●9	●1	●5
●8	●7	●6

The coordinate distance between each hole was such that movement between any two adjacent holes vertically or horizontally repositioned the tool by 1° in bearing for horizontal and 1° in inclinations vertically. The simulated survey was performed by entering the initial conditions for hole #1 at an initial

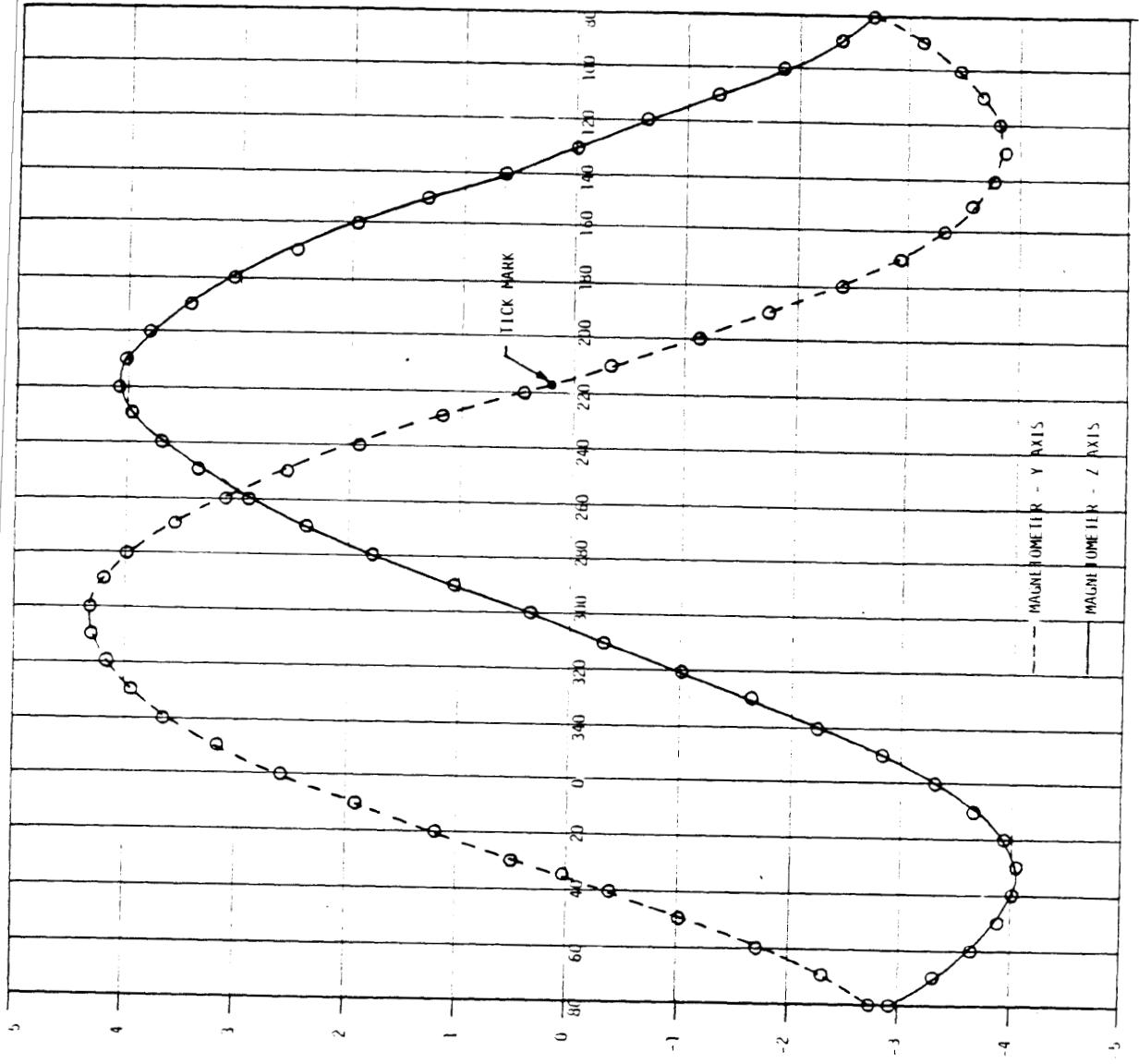


Figure 23. Magnetometer Output for Y Axis and Z Axis

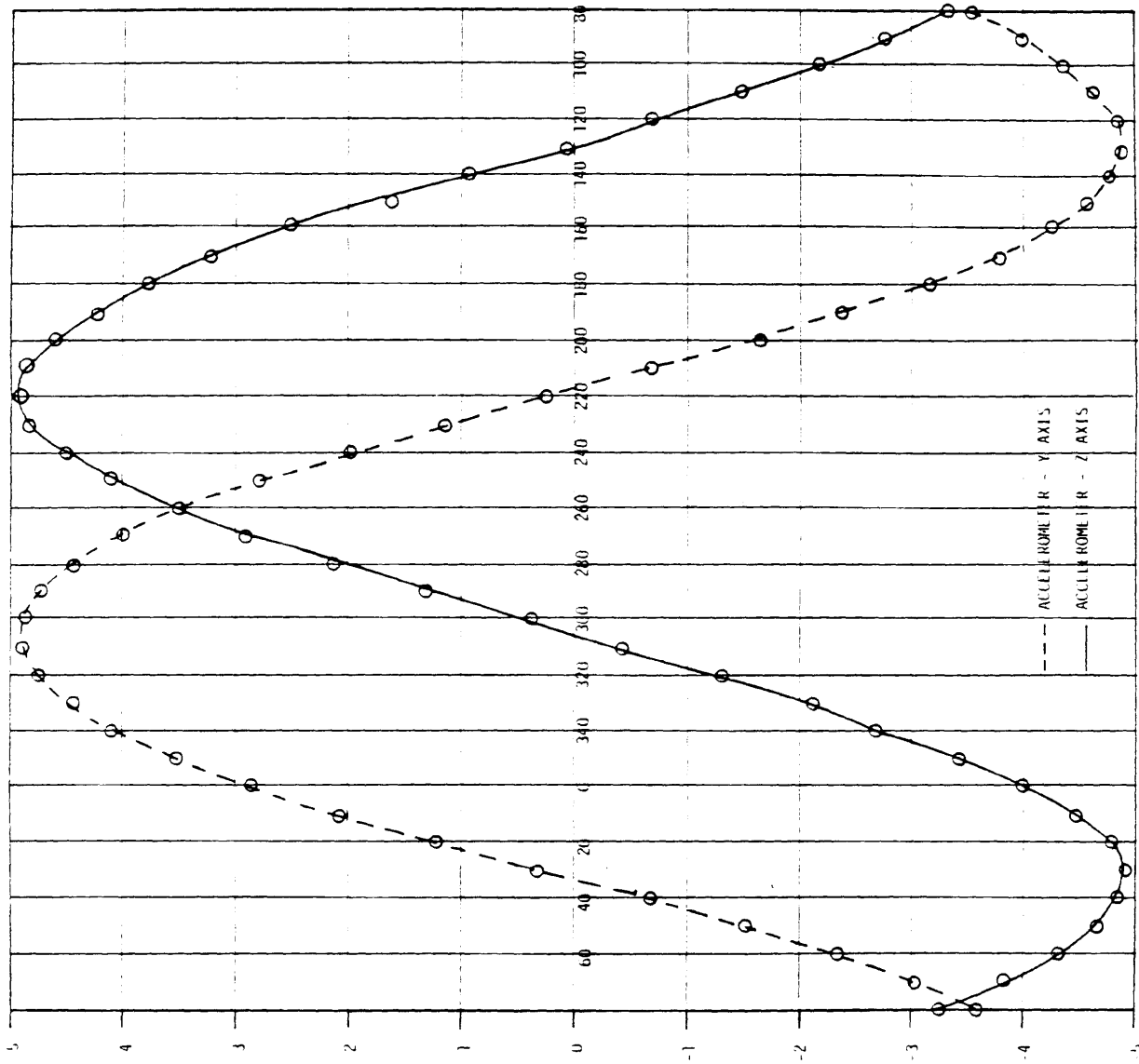


Figure 24. Accelerometer Output for Y Axis and Z Axis for Rotation about X Axis

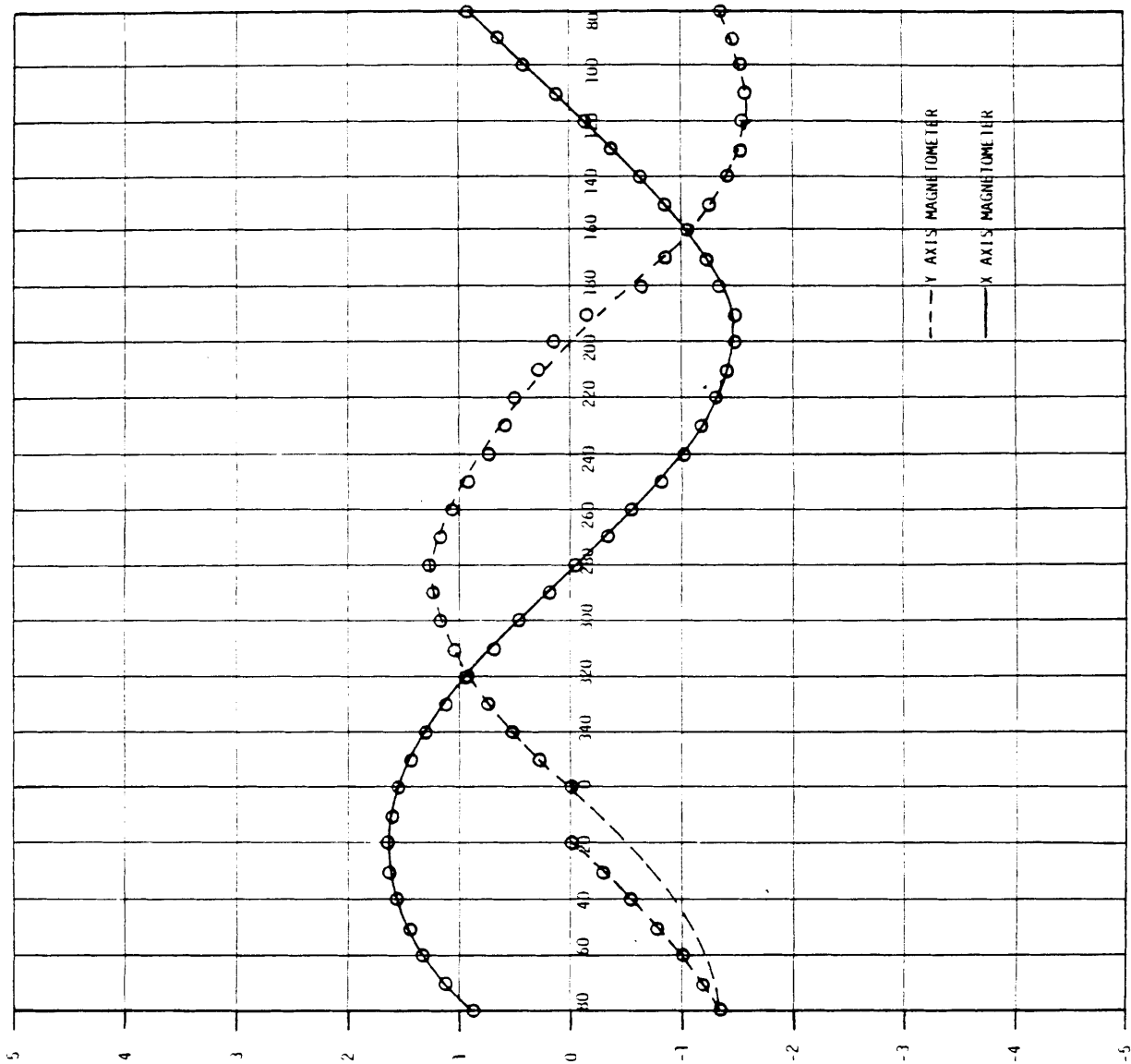


Figure 25. Magnetometer Output for Y Axis and X Axis for Rotation about X Axis

string length of 20 feet. Then a survey of the first hole position was done and an assumed 10 foot drill rod added. The tool was then positioned sequentially in each hole and a survey done adding 10 foot rod sections for each hole until hole #1 was repeated. This resulted in a total simulated survey of 120 feet of string length. Figure 26A shows a comparison of calculated bearings versus tool measurements. Figure 26B gives the same comparison for inclination. Figure 26c compares the theoretical survey path to the computer results provided by the cableless survey system.

5.3 Drilling Tests

Drilling tests were performed at the Federal #1 mine in Granttown West Virginia. The following deviations from this test plan are noted.

- The hole depth was terminated at 330 feet due to drilling problems with the drilling equipment and the contact of a seized drill string located in an adjacent hole.
- No readings were taken with the Sperry Sun Multishot system between 75 and 165 feet.

Figure 27 shows the comparison of vertical deviation as measured by the two systems.

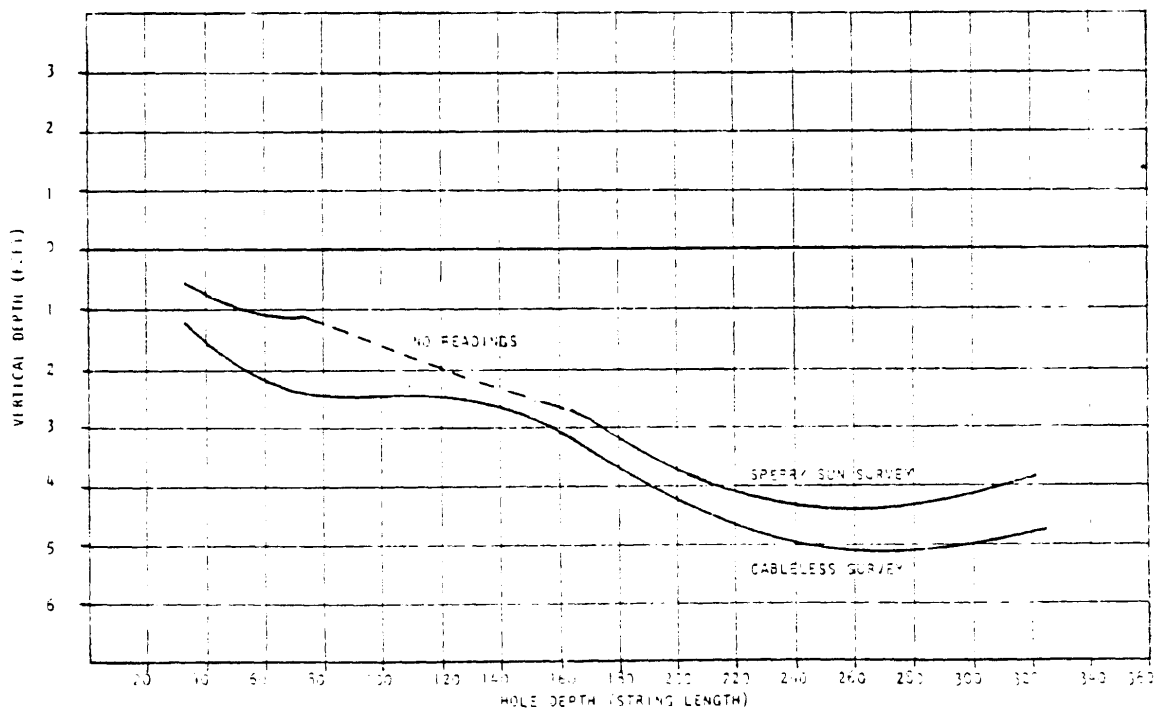


Figure 27 . Vertical Survey of "Horizontal" Drill Hole Using Sperry Sun Survey System and Cableless Electronic Survey System

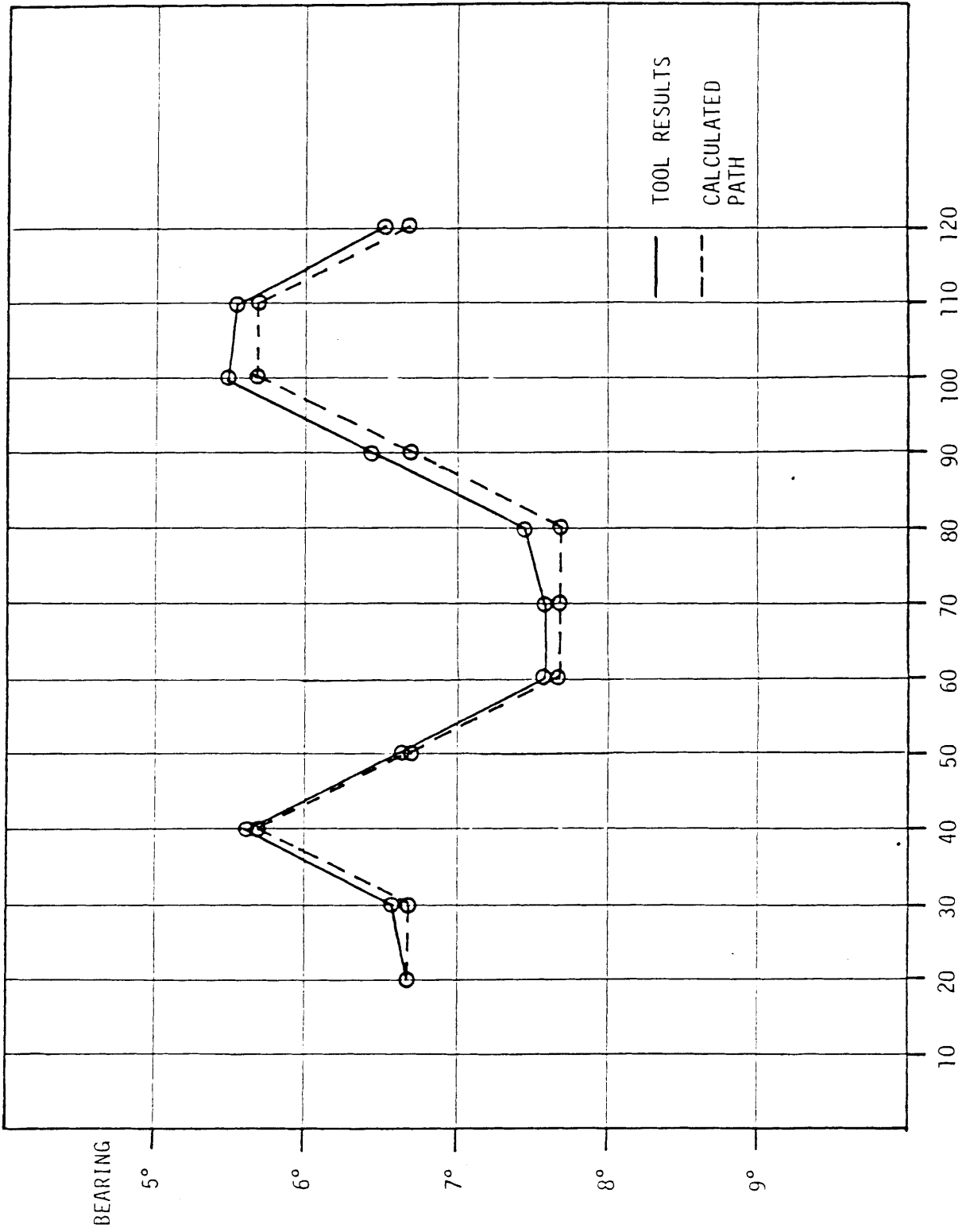


Figure 26a Comparison of Calculated Survey Path vs. Measured Bearings for Simulated Trajectory Test

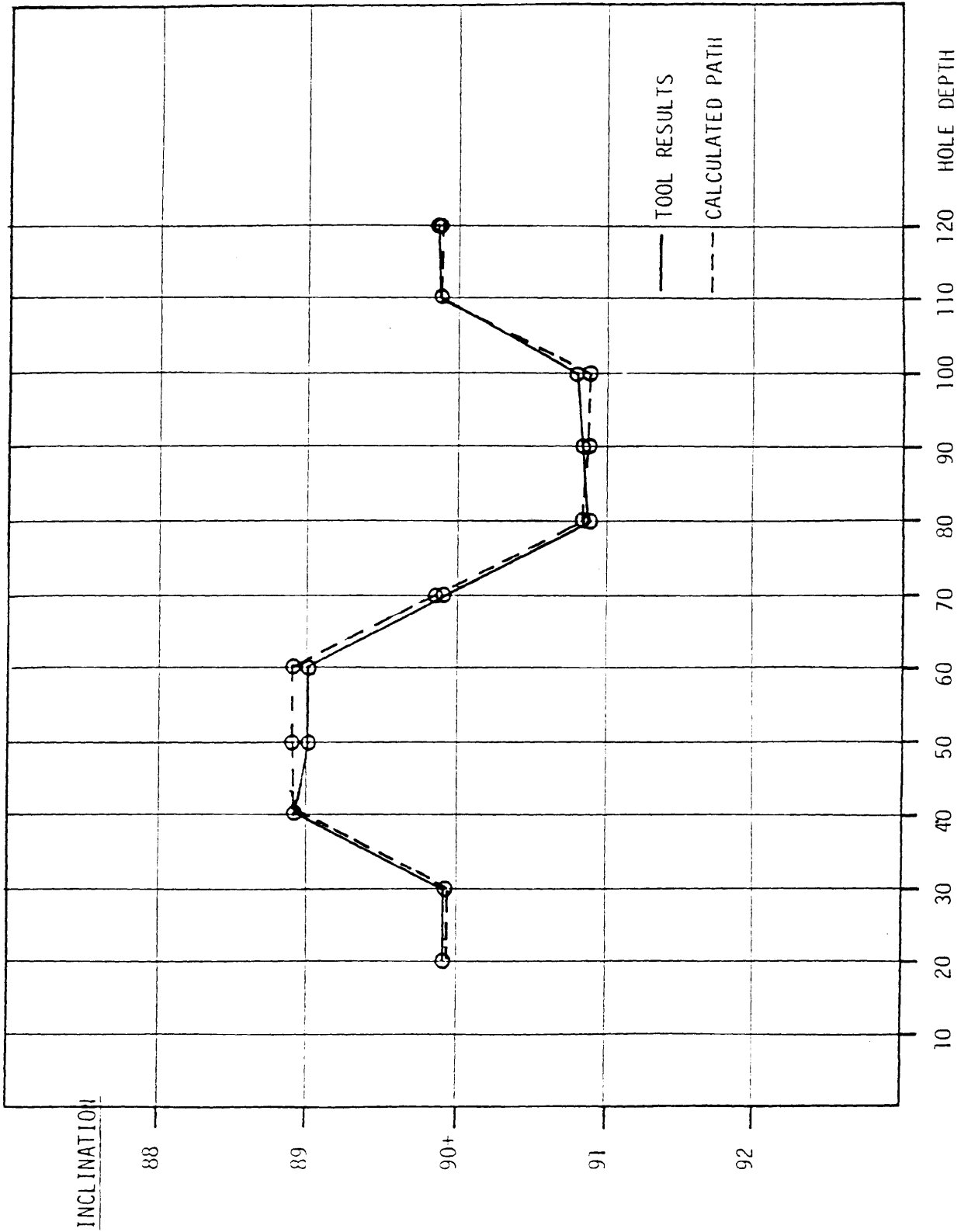


Figure 26b. Comparison of Calculated Survey Path vs. Measured Inclination for Simulated Trajectory Test

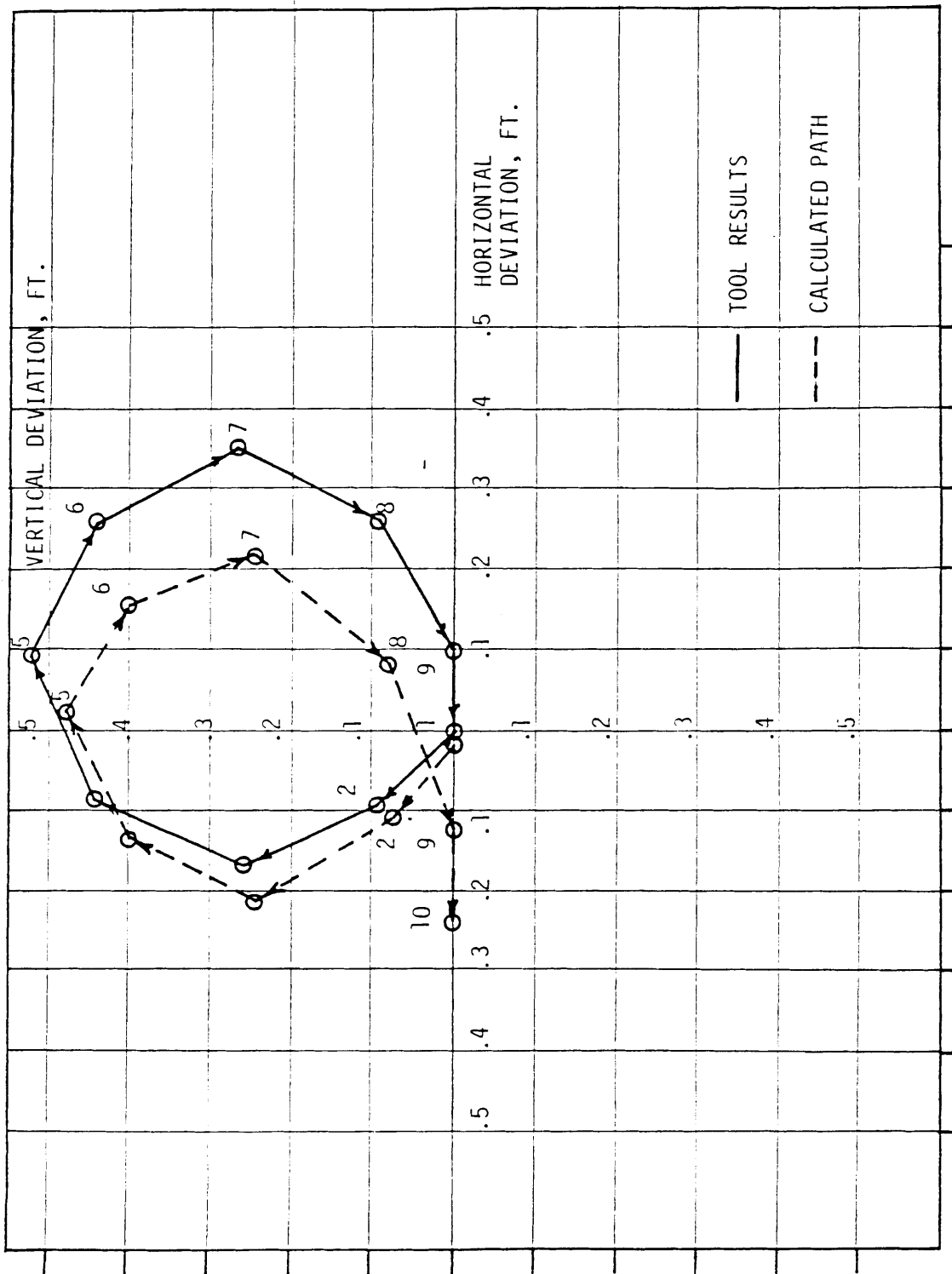


Figure 26c. Comparison of Calculated Survey Path vs. Measured Survey Path for Simulated Trajectory Test.

APPENDIX D

SYSTEM SCHEMATIC DIAGRAMS AND SOFTWARE LISTINGS

CONNECTOR DESIGNATION AND PIN
ASSIGNMENTS FOR DOWNHOLE PACKAGE

Sensor Canister/Electronics: J1/P1

Connector: Bendix PT02A-14-18S/P

<u>Pin</u>	<u>Signal</u>
A	Wiper Pressure Switch
B	X Axis Accelerometer
C	Y Axis Accelerometer
D	+12 volts, Z Axis Accelerometer
E	Power Return, Z Axis Accelerometer
F	NC
H	Signal Return, Z Axis Accelerometer
J	+12 volts, X,Y Axis Accelerometer and X,Y,Z, Axis Magnetometer
K	-12 volts, X,Y Axis Accelerometer and X,Y,Z, Axis Magnetometer
L	Power and Signal Return, X,Y Axis Accelerometer and X,Y,Z, Axis Magnetometer
M	+12 volts, Pressure Switch
N	Signal Return, Pressure Switch
P	-12 volts, Z Axis Accelerometer
R	Signal Output Y Axis Magnetometer
S	Signal Output X Axis Accelerometer
T	Signal Output X Axis Magnetometer
U	Signal Output Z Axis Magnetometer

Electronics/Battery Pack: P2/J2

Connector: Bendix PT06-10-6- S/P

<u>Pin</u>	<u>Signal</u>
A	Transmit Toriod
B	Return, Transmit Torriod and Case Ground
C	- Battery Voltage
D	± Battery Return
E	+ Battery Voltage
F	NC

Z-Axis Accelerometer: J3

Connector: Sunstrand Data Control CA-116-15-30

<u>Pin</u>	<u>Signal</u>
1	+12 volts
2	Signal Return
3	Signal Output
4	-12 volts
5	Power Return
6	Self Test

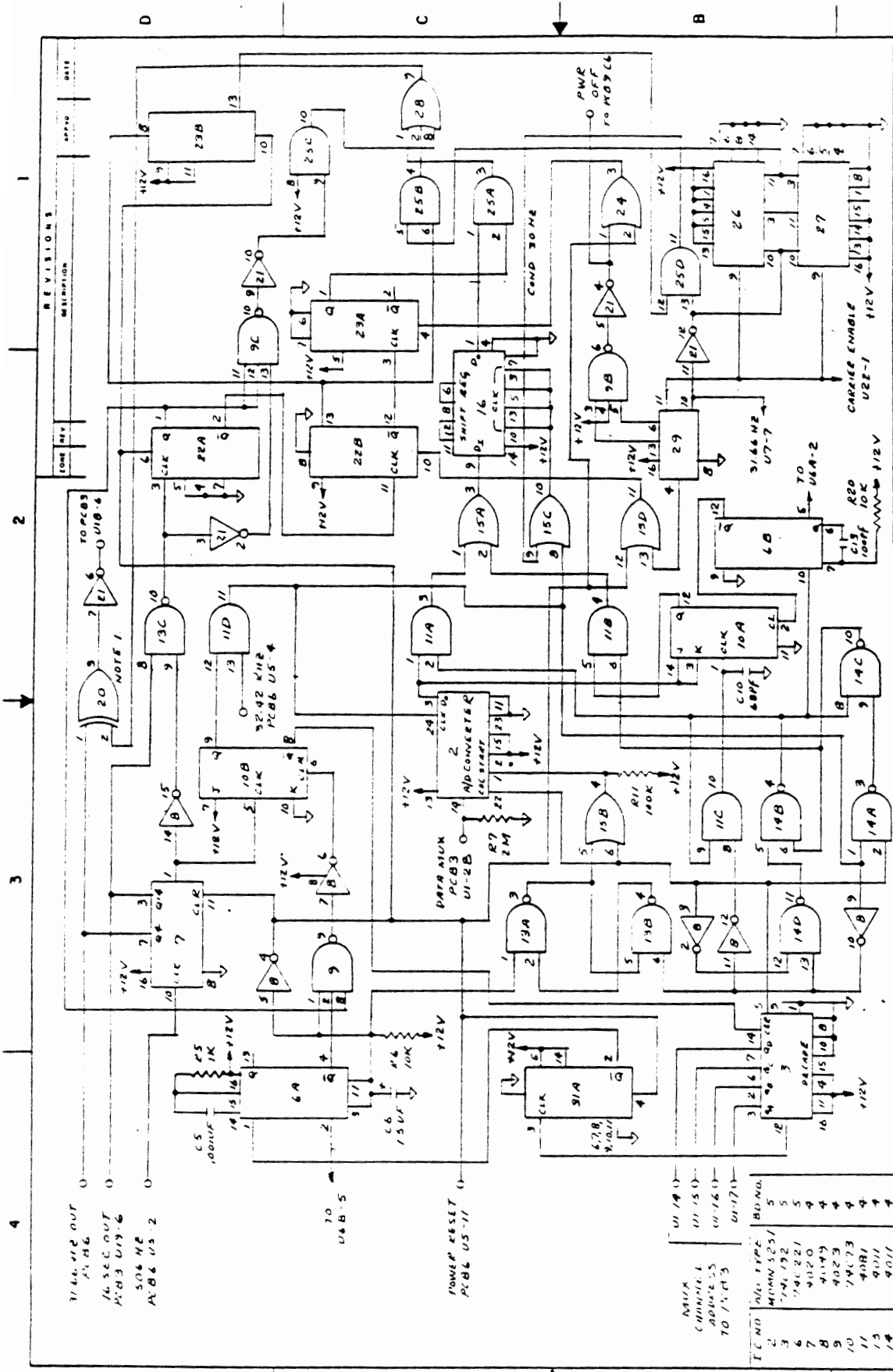
X,Y Axis Accelerometer: No Connector

<u>Pin</u>	<u>Signal</u>
1	+12 volts
2	-12 volts
3	Power and Signal Return
4	X Axis Output
5	Y Axis Output

Magnetometer J4

Connector: PT02-C-10-65

<u>Pin</u>	<u>Signal</u>
A	+12 volt
B	Power and Signal Return
C	-12 volt
D	X Axis Output
E	Y Axis Output
F	Z Axis Output



REV	DATE	BY	CHKD	APP'D	DESCRIPTION
1					
2					
3					
4					

IC NO	IC TYPE	QUANTITY	REV
1	74181	1	1
2	74180	1	1
3	7474	1	1
4	7475	1	1
5	7400	1	1
6	7401	1	1
7	7402	1	1
8	7404	1	1
9	7408	1	1
10	7432	1	1
11	7430	1	1
12	7431	1	1
13	7404	1	1
14	7404	1	1
15	7404	1	1
16	7404	1	1
17	7404	1	1
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27	7404	1	1
28	7404	1	1
29	7404	1	1
30	7404	1	1
31	7404	1	1

REVISIONS	DATE	DESCRIPTION
1		
2		
3		
4		

CONTRACT NO.	DATE	SIGNATURE	CHKD	APP'D
NO177069	1/15/69	[Signature]	[Signature]	[Signature]

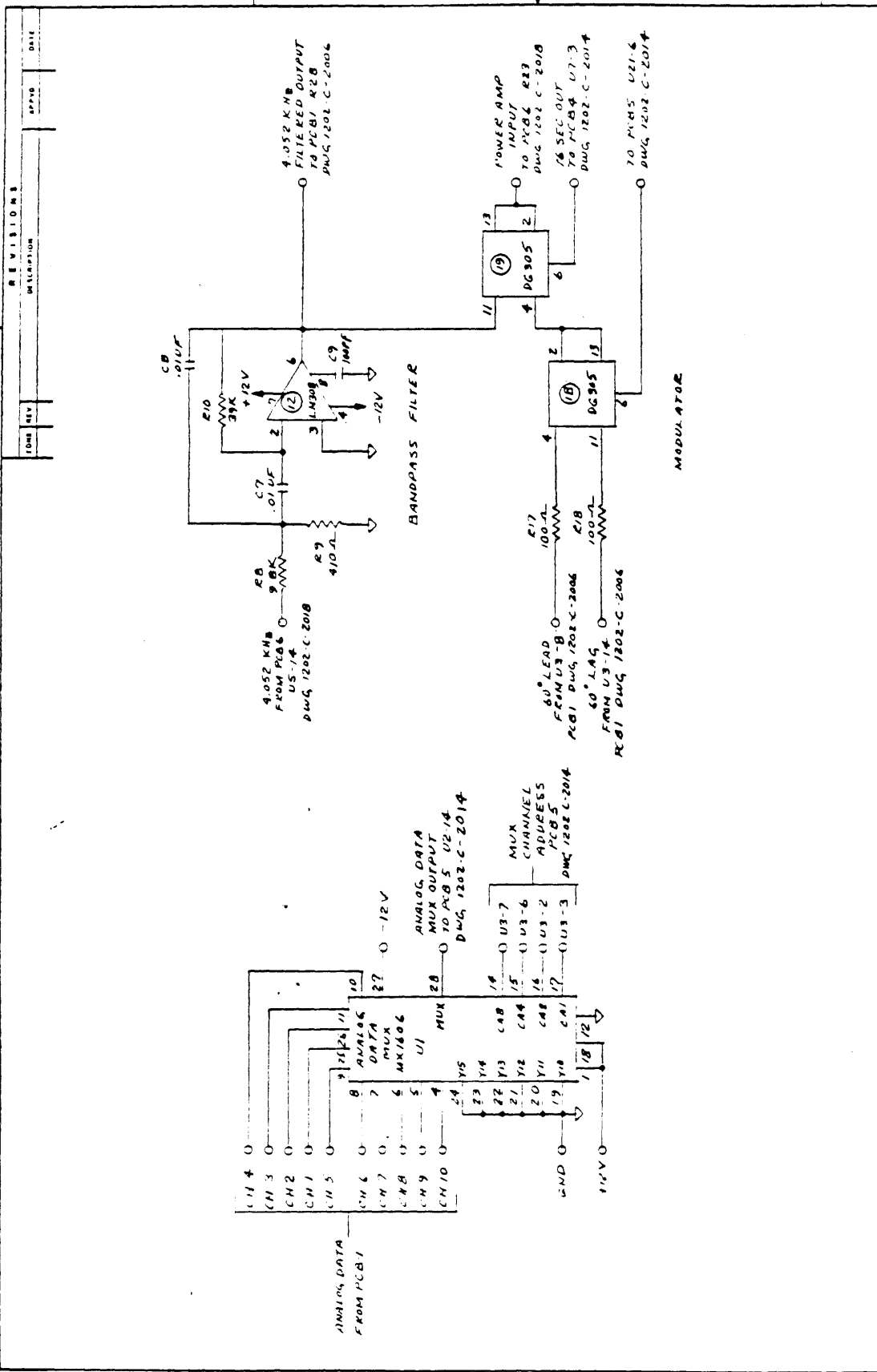
ENSCO, INC.	SPRINGFIELD, VIRGINIA
SCHEMATIC DIAGRAM	
DOWNHOLE MACHINERY	
PCB 2, A & S	
SIZE	CORE IDENT NO
C 06359	U2B-1
SCALE	1202-C-2014
SHEET	1

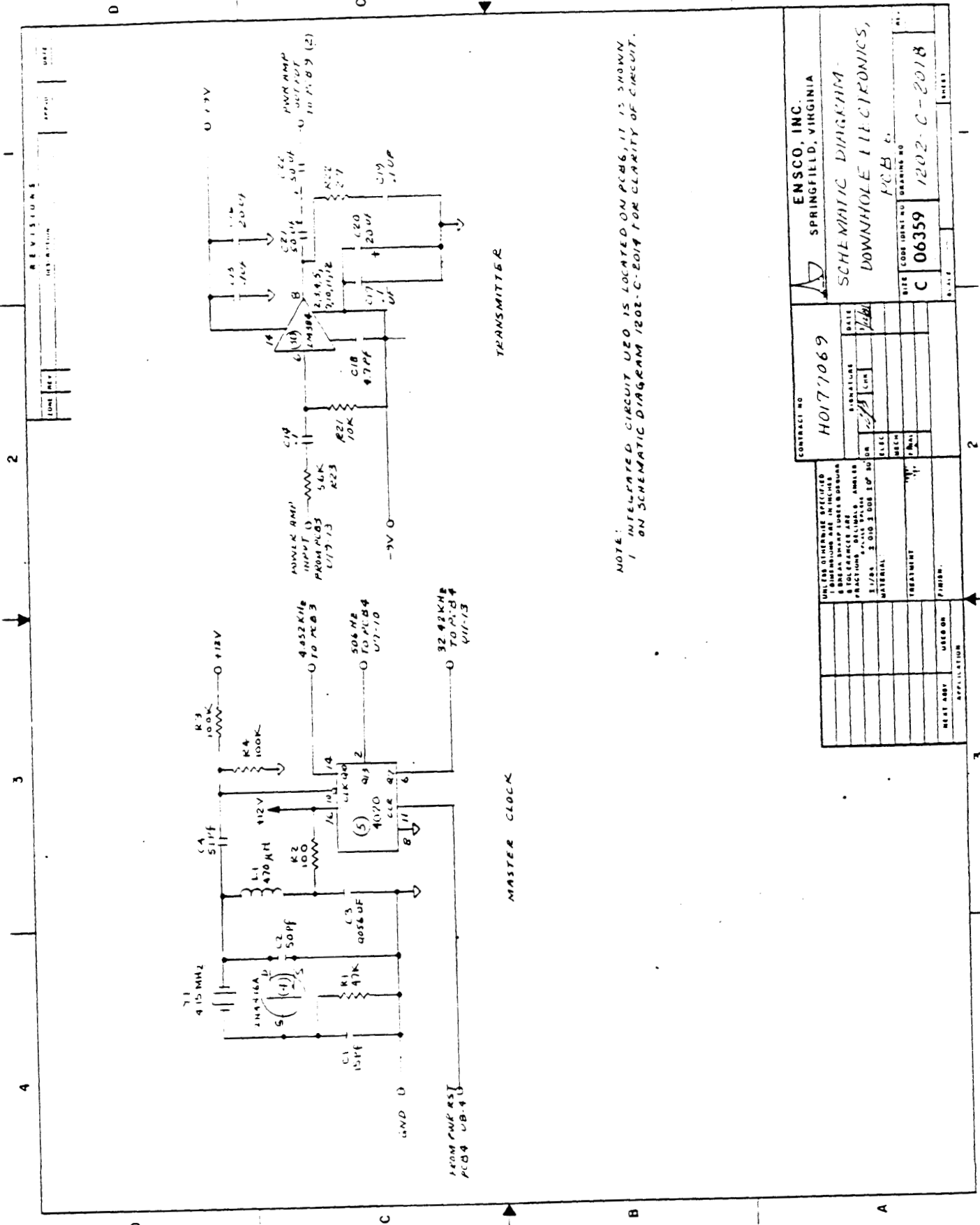
UNLESS OTHERWISE SPECIFIED
 5 TOLERANCES ARE
 FRACTIONS, DECIMALS, ANGLES
 3/16" 3 DIG 1 008 10 10 10
 MATERIAL

TREATMENT: _____
 FINISH: _____

REEL ABB: _____ USED IN: _____
 APPLICATION: _____

NOTES:
 1 U20 (40-10) IS LOCATED PCB 6,
 IS SHOWN ON THIS SCHEMATIC
 FOR CIRCUIT CONTINUITY.

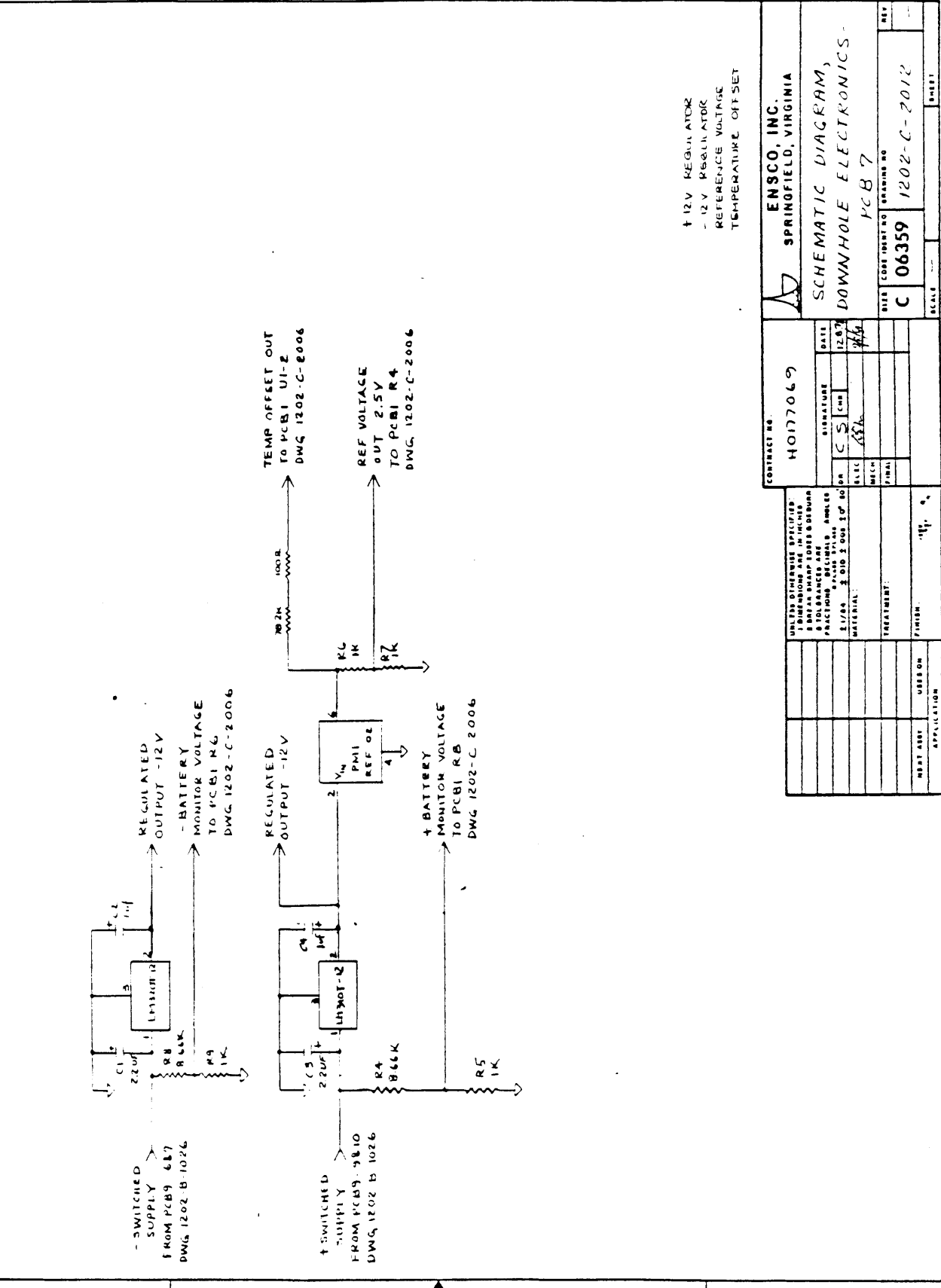




NOTE:
 1 INTEGRATED CIRCUIT U20 IS LOCATED ON PCB 6, 11 IS SHOWN
 ON SCHEMATIC DIAGRAM 1202-C-2018 FOR CLARITY OF CIRCUIT.

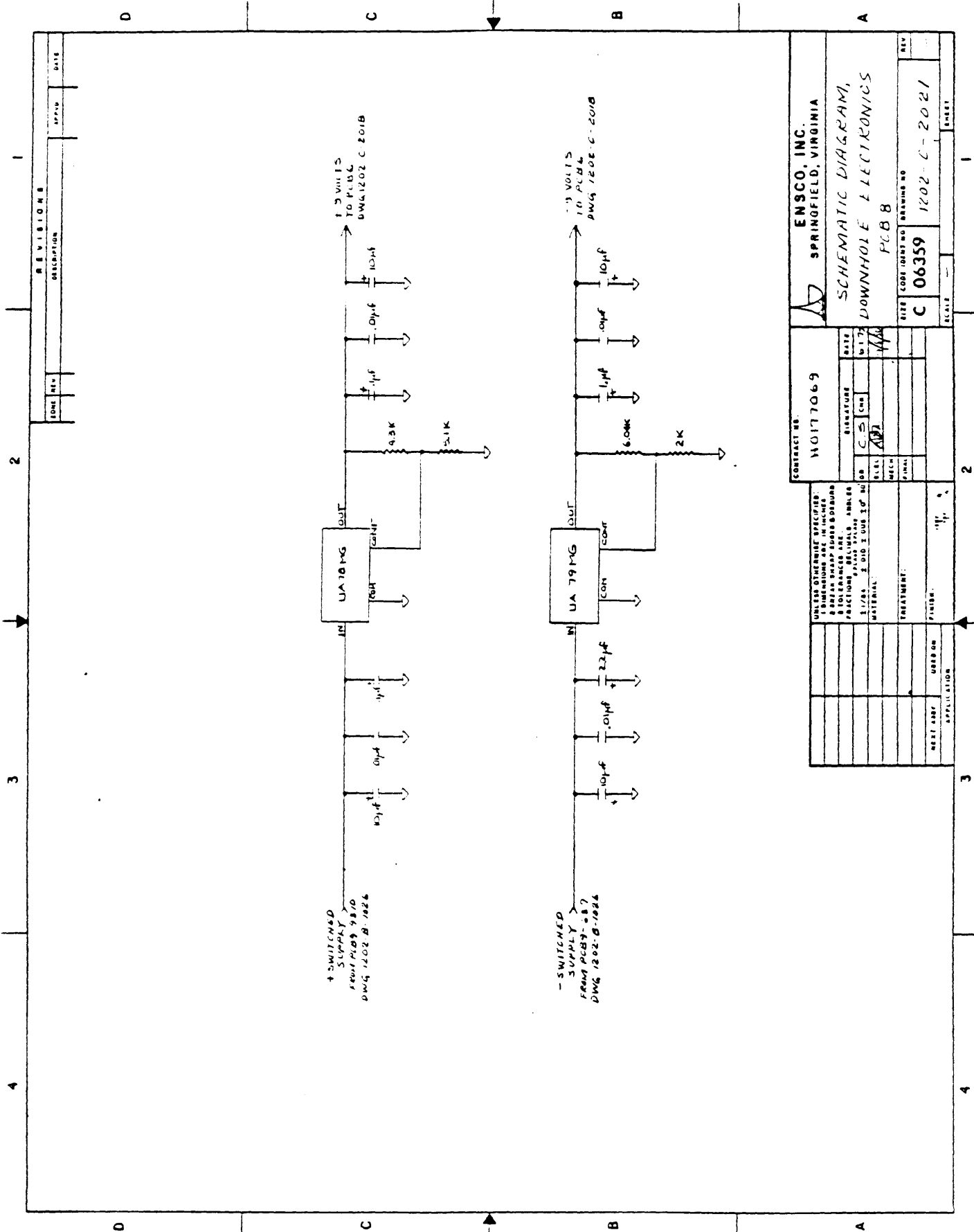
REVISIONS DATE		ENSCO, INC. SPRINGFIELD, VIRGINIA	
CONTRACT NO. H0171069		SCHEMATIC DIAGRAM DOWNHOLE ELECTRONICS,	
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES DIMENSIONS IN PARENTHESES ARE FRACTIONS DECIMALS, ANGLES IN DEGREES, SURFACE FINISH UNLESS OTHERWISE SPECIFIED		SIZE CODE DRWT NO C 06359	
SIGNATURE DATE		PCB NO. 1202-C-2018	
MATERIAL		DRAWING NO	
TREATMENT		SHEET	
FINISH		1	
NEXT APPY APPLICATION		2	
USED ON		3	
4		4	

REV	DESCRIPTION	DATE
1		



+12V REGULATOR
 -12V REGULATOR
 REFERENCE VOLTAGE
 TEMPERATURE OFFSET

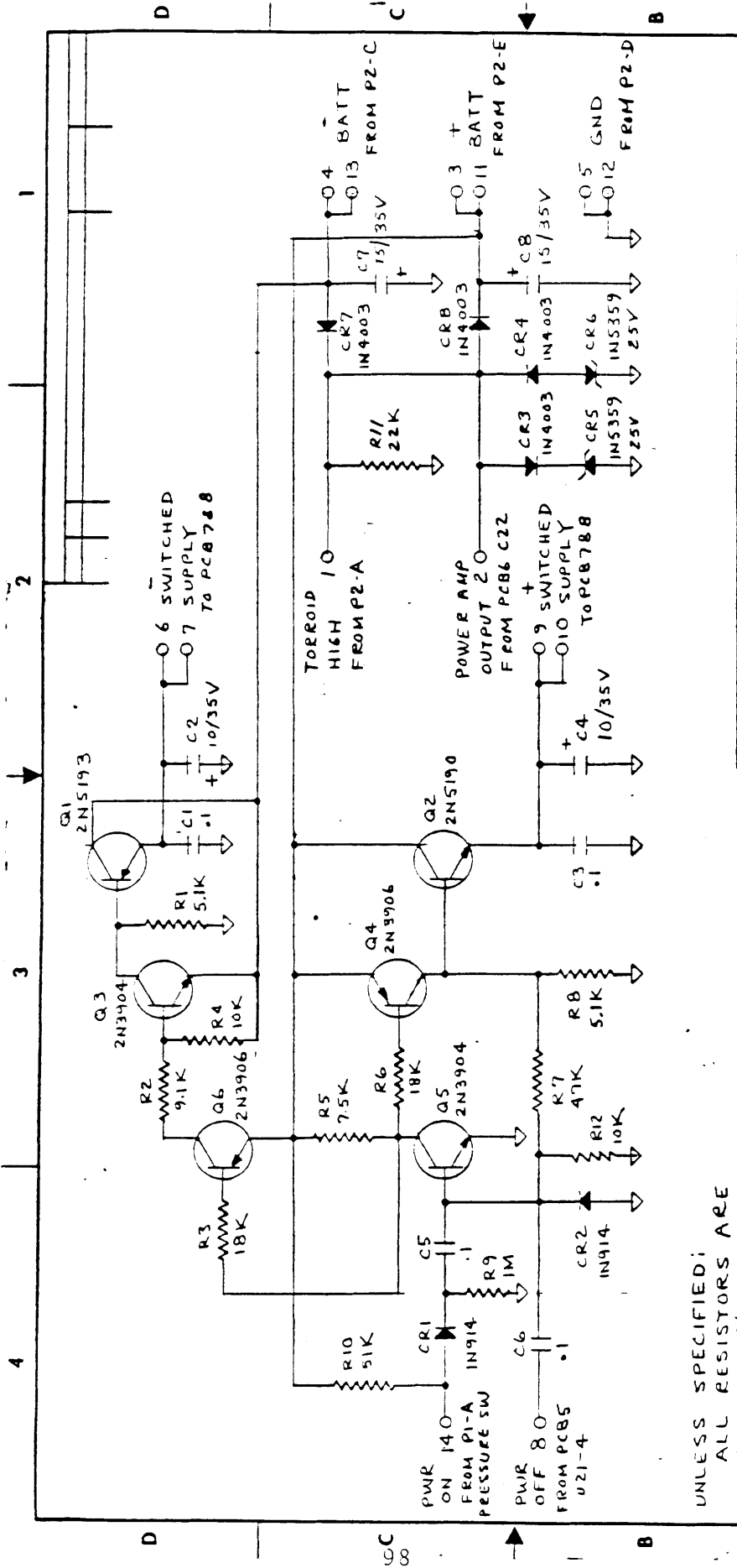
ENSCO, INC. SPRINGFIELD, VIRGINIA		CONTRACT NO. HO177069	
SCHMATIC DIAGRAM, DOWNHOLE ELECTRONICS - PCB 7			
DATE 12/87	SIGNATURE C S	SCALE ---	SHEET ---
REV ---	CONFIDENTIAL ---	ORDERING NO. 1202-C-2012	REV ---



REVISIONS		DATE
1	DESCRIPTION	
2		
3		
4		

CONTRACT NO. N0177069		ENSCO, INC. SPRINGFIELD, VIRGINIA	
DATE: 11/28/87		SCHEMATIC DIAGRAM, DOWNHOLE ELECTRONICS PCB B	
DR: CS	CHK: [Signature]	SIZE: C	CODE (PRINTING DRAWING NO): 06359
DESIGN: [Signature]	DATE: 11/28/87	SCALE: 1	1202-C-2021
MATERIAL:	TREATMENT:	REV: 1	SHEET: 1

UNLESS OTHERWISE SPECIFIED, DIMENSIONS ARE IN INCHES	DATE: 11/28/87
80/20 ANGLE SHARP EDGES & CORNERS	DR: CS
8 TOLERANCES ARE:	CHK: [Signature]
FRACTIONS: 1/16, 1/8, 1/4, 3/8, 1/2	DESIGN: [Signature]
DECIMALS: 0.0005, 0.001, 0.002, 0.005, 0.01, 0.02, 0.05, 0.1	DATE: 11/28/87
1/200 ± 0.0015" MAX	SCALE: 1
MATERIAL:	SIZE: C
TREATMENT:	CODE (PRINTING DRAWING NO): 06359
NEST AND USED ON:	1202-C-2021
APPLICATOR:	SHEET: 1



UNLESS SPECIFIED:
 ALL RESISTORS ARE
 1/4 W 5% CARBON

ENSCO, INC. SPRINGFIELD, VIRGINIA		CONTRACT NO. H0177069	
SCHEMATIC DIAGRAM, DOWNHOLE ELECTRONICS - POWER TRIGGER PCB9		DATE 7/20/80	
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DRAWING NO. 1202-B-1026		SCALE:	
SHEET 4		REVISION A	

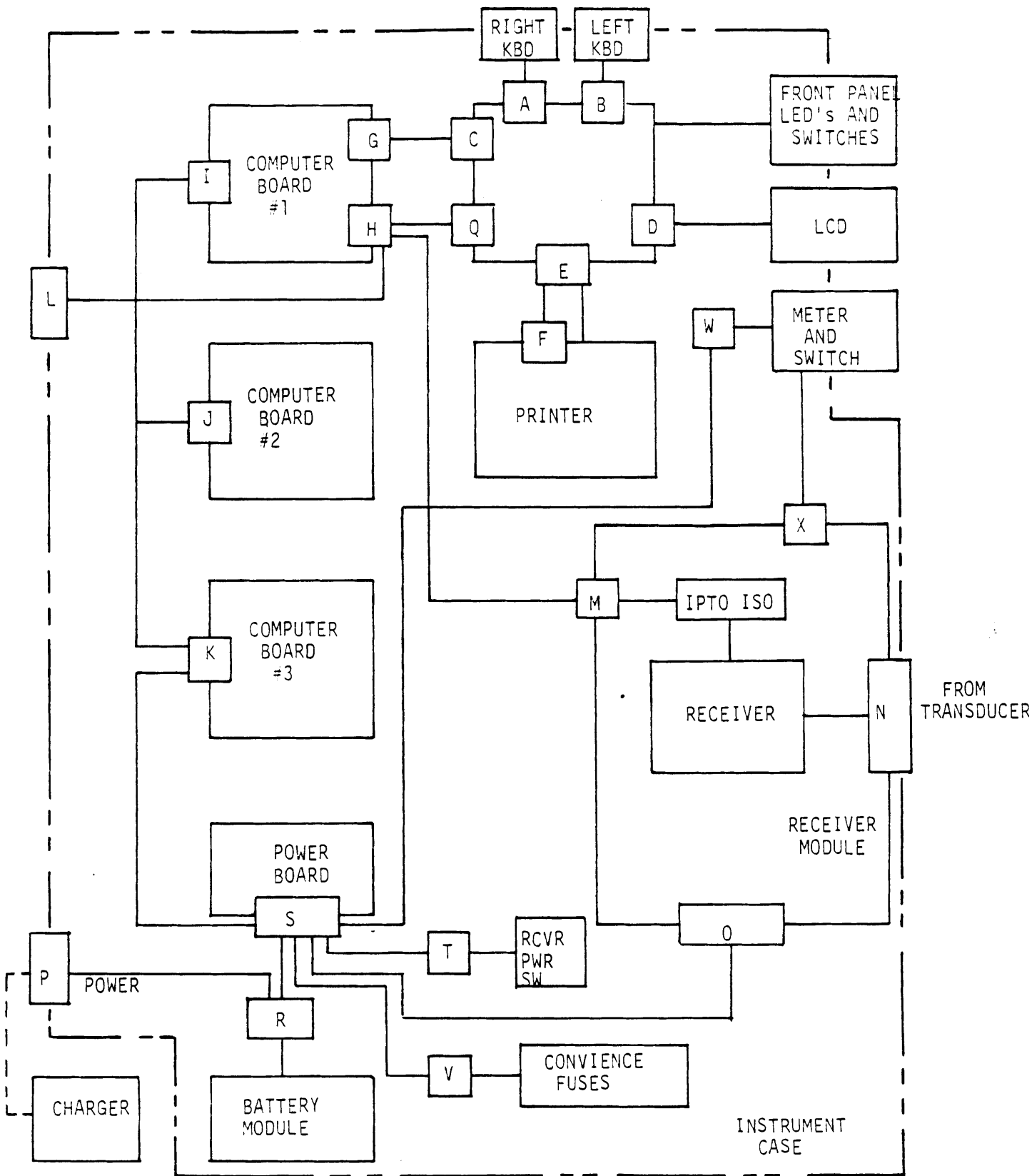


ENSCO INC
SPRINGFIELD, VIRGINIA

PROJECT NO 7017069

DATE 06/15/59

NO.	DESCRIPTION	QTY	UNIT	PRICE	TOTAL
1	REAR PANEL	1	EA	100.00	100.00
2	PRINTER	1	EA	200.00	200.00
3	RECEIVER CHASSIS	1	EA	150.00	150.00
4	RECEIVER TRANSDUCER CONNECTOR	1	EA	50.00	50.00
5	ASSIGNMENT CASE	1	EA	75.00	75.00
6	INTERCOM HANDS ON	1	EA	25.00	25.00
7	CONTROL ROOM	1	EA	100.00	100.00
8	REAR PANEL	1	EA	100.00	100.00
9	RECEIVER CHASSIS	1	EA	150.00	150.00
10	RECEIVER TRANSDUCER CONNECTOR	1	EA	50.00	50.00
11	ASSIGNMENT CASE	1	EA	75.00	75.00
12	INTERCOM HANDS ON	1	EA	25.00	25.00
13	CONTROL ROOM	1	EA	100.00	100.00
14	REAR PANEL	1	EA	100.00	100.00
15	RECEIVER CHASSIS	1	EA	150.00	150.00
16	RECEIVER TRANSDUCER CONNECTOR	1	EA	50.00	50.00
17	ASSIGNMENT CASE	1	EA	75.00	75.00
18	INTERCOM HANDS ON	1	EA	25.00	25.00
19	CONTROL ROOM	1	EA	100.00	100.00
20	REAR PANEL	1	EA	100.00	100.00
21	RECEIVER CHASSIS	1	EA	150.00	150.00
22	RECEIVER TRANSDUCER CONNECTOR	1	EA	50.00	50.00
23	ASSIGNMENT CASE	1	EA	75.00	75.00
24	INTERCOM HANDS ON	1	EA	25.00	25.00
25	CONTROL ROOM	1	EA	100.00	100.00



Processing and Display Subsystem Interconnection Diagram

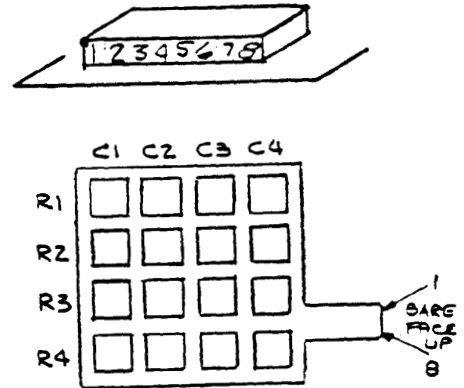
CONNECTOR DESIGNATIONS AND PIN ASSIGNMENTS
FOR UPHOLE RECEIVER/PROCESSOR PACKAGE

Right Keyboard to Front Panel PCB: JA

Left Keyboard to Front Panel PCB: JB

Connector: Burndy 8 Pin

<u>Pin</u>	<u>Signal</u>
1	R1
2	C2
3	C3
4	C4
5	R2
6	R3
7	R4
8	C1



Front Panel to Computer Board #1: JC/PC

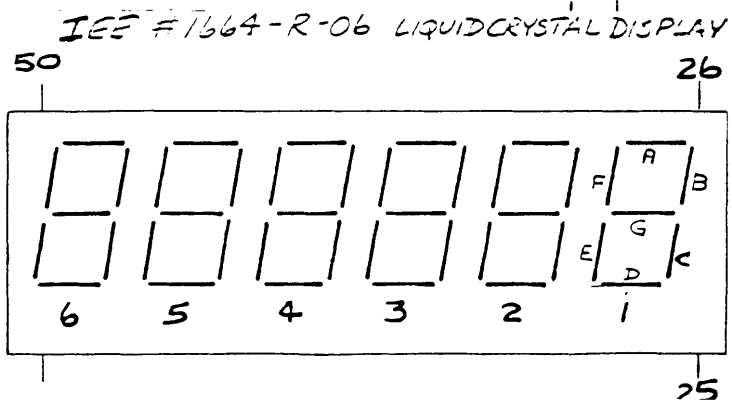
Connector: Augat 110-26001-102

<u>Pin</u>	<u>Signal</u>
1	DX0
2	DX1
3	DX2
4	DX3
5	DX4
6	DX5
7	DX6
8	DX7
9	DX8
10	DX9
11	DX10
12	DX11
13	GND
14	+5V _m (Switched)
15	SYS RESET

<u>Pin</u>	<u>Signal</u>
16	KACK-
17	KREQ2+
18	KREQ1+
19	+5V _m (Switched)
20	+5V _m (Switched)
21	+5V _m (Source)
22	AF1
23	AF2
24	AW2
25	+5V _m (Source)
26	+5V _m (Source)

Front Panel PCB to LCD: JD
Connector: Augat 325AG1F

<u>Pin</u>	<u>Signal</u>
1	BP
2	E6
3	D6
4	C6
5	DP5-6
6	E5
7	D5
8	C5
9	DP4-5
10	E4
11	D4
12	C4
13	DP3-4
14	E3
15	D3



<u>Pin</u>	<u>Signal</u>
16	C3
17	DP2-3
18	E2
19	D2
20	C2
21	DP1-2
22	E1
23	D1
24	C1
25	B1
26	A1
27	F1
28	G1
29	B2
30	A2
31	F2
32	G2
33	L
34	B3
35	A3
36	F3
37	G3
38	B4
39	A4
40	F4
41	G4
42	L
43	B5
44	A5
45	F5
46	G5
47	B6
48	A6
49	F6
50	G6

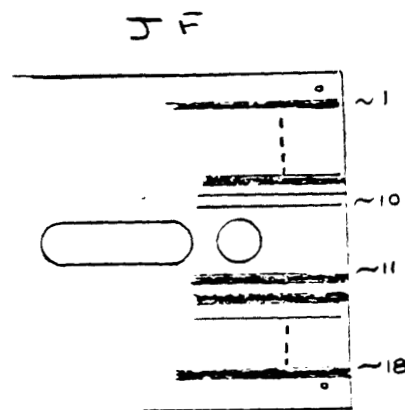
Front Panel Electronics to Printer: JE/PE
Connector: Augat 110-26001-102

<u>Pin</u>	<u>Signal</u>
1	DIG 11
2	DIG 9
3	DOT 5
4	DIG 7
5	DOT 4
6	DIG 5
7	DIG 3
8	DIG 1
9	NC
10	NC
11	NC
12	NC
13	NC
14	DIG 12
15	DIG 10
16	DIG 8
17	DOT 3
18	DIG 6
19	DOT 2
20	DIG 4
21	DIG 2
22	DOT 1
23	Motor Yellow
24	Motor Red
25	Motor Orange
26	Motor Brown

Front Panel Cable to Printer Element: JF

Connector: Part of Texas Instruments Printer EPN9112

<u>Pin</u>	<u>Signal</u>
1	NC
2	DIG 12
3	DIG 11
4	DIG 10
5	DIG 9
6	DIG 8
7	DOT 5
8	DOT 3
9	DIG 7
10	DIG 6
11	DOT 4
12	DOT 2
13	DIG 5
14	DIG 4
15	DIG 3
16	DIG 2
17	DIG 1
18	DOT 1



Computer Board #1 to Front Panel: JG/PG

Connector: Augat 110-26001-601

<u>Pin</u>	<u>Signal</u>
(Same as JC/PC)	

Computer Board #1 (JH) to Front Panel (JQ), Receiver (JM),
Ext. Computer (JL)

Connector: Augat 110-26001-601

<u>Pin</u>	<u>Signal</u>	<u>Destination</u>
1	AF4	JQ
2	AF3	JQ
3	BS4	JQ
4	BW2	JQ
5	RCVR CLK	JM
6	RCVR DATA	JM
7	UART CLK	JL
8	720 DATA	JL
9	GND	JL
10	300 BAUD	JL
11	+5V from TTY	JL
12	5V UART	JL
13	NC	-
14	NC	-
15	Printer +5V _B	JQ
16	Printer Pwr Control	JQ
17	Printer +12V _B	JQ
18	+5V _m to RCVR OPTO ISO	JM
19	GND to RCVR OPTO ISO	JM
20	SELF Test Output	JM
21	+12V from TTY Interface	JL
22	UART DATA	JL
23	-12V FROM TTY Interface	JL
24	CR Wait from TTY	JL
25	Printer +12V _B	JQ
26	NC	-

Computer Board 1,2,3, JI, JJ, JK (all connectors bussed pin for pin)
 Connector: Viking 3VH 36/IJND

<u>Pin</u>	<u>Signal</u>
1	NC
2	BF3
3	+5V _C Unswitched
4	+12V _A
5	+5V _M
6	XTB
7	XTA
8	V _M Lo
9	INT GNT
10	SKP INT
11	DEVSEL
12	GND
13	Sys Res & Pwr Up
14	Sys Res
15	Y
16	AS2
17	C2
18	MEMSW
19	MEMSW
20	C1
21	+12V _B
22	GND
23	NC
24	+5V _A
25	APU OFF
26	2.4315MHz
27	XTC
28	24.315KHz
29	READD
30	MEMSEL
31	AS2

<u>Pin</u>	<u>Signal</u>
32	NC
33	NC
34	Wait
35	AR1
36	+5V _B
37	NC
38	LXMAR
39	S-T DATA
40	NC
41	NC
42	DX8
43	DX7
44	DX9
45	DX0
46	GND
47	DX10
48	DX1
49	NC
50	DX11
51	DX6
52	GND
53	AW1
54	DX2
55	4MHZ
56	DX3
57	Power A CTL
58	GND
59	DX4
60	NC
61	NC
62	DX5
63	NC
64	GND
65	PWR B Control

<u>Pin</u>	<u>Signal</u>
66	BF4
67	NC
68	NC
69	NC
70	+5V _M
71	NC
72	+5V _M

External Computer Connector: JL
Connector: ITT KPT07E16-26S

<u>Pin</u>	<u>Signal</u>
A	CR Wait
W	Spare
X	UART DATA
Y	-12V
Z	+12V
a	GND
c	+5V (from TTY)
B	UART CLK
C	300 BAND

Receiver to Computer JM
Connector: Winchester MRE-9P/PR

<u>Pin</u>	<u>Signal</u>
A	Receiver Data Out
B	Receiver Clock Out
C	Computer GND
D	+5V _M
E	Self Test Input

External Receiver Input Connector JN
Connector: KPT07E 16-8S

<u>Pin</u>	<u>Signal</u>
C	Input 1
D	Shield
E	Input 2

Receiver Power Input: JO
Connector: Winchester MRE 95J

<u>Pin</u>	<u>Signal</u>
A	+8 Volts
B	- 8 Volts
C	GND
D	Low Voltage Alarm
E	+5V

External Power and Charging Connector: JP
Connector: ITT KPT07E12-8S

<u>Pin</u>	<u>Signal</u>
A	Ext. Pwr
B	RCVR Batt Chg
C	RCVR GND
D	Processor Batt Chg
E	Processor GND
F	Spare
G	RCVR Batt Sense
H	Proc Batt Sense

Front Panel to Computer Board #3: JQ
Connector: Augat 110-26001-601

<u>Pin</u>	<u>Signal</u>
1	AF4
2	AF3
3	B54
4	BW2
	110

<u>Pin</u>	<u>Signal</u>
15	+5V _B Printer
16	Printer Power Control
17	+12V _B Printer
25	+12V _B Printer

Battery Module Connector: JR
Connector: Winchester MRE 95

<u>Pin</u>	<u>Signal</u>
A	Ext Pwr
B	RCVR Batt Chg
C	RCVR GND
D	Processor Batt Chg
E	Processor GND
F	RCVR Source
H	RCVR Sense
J	Processor Source
K	Processor Sense

Power Supply Board: JS
Connector: Elco 6007-22-44B

<u>Pin</u>	<u>Signal</u>
1	NC
2	-8V to RCVR
3	+8V to RCVR
4	+5V to RCVR
5	RCVR GND
6	RCVR LOW Voltage Alarm
7	NC
8	RCVR Batt Sense
9	RCVR Pwr +5V (Unswitched)
10	RCVR Batt Source
11	Proc GND

<u>Pin</u>	<u>Signal</u>
12	Proc Batt Low Alarm
13	Proc Battery Sense
14	+5V _C to RAM & Proc. Switch (Unswitched)
15	Proc Batt Source
16	+12V _B to Printer
17	Printer Pwr Control B
18	+5V _M to Proc
19	AM9511 Pwr Control A
20	+5V _B to Printer
21	+5V _A to AM9511
22	+12V _A to AM9511

Power Supply Board to Power Switch JT

Connector: Waldom 03-06-1041

<u>Pin</u>	<u>Signal</u>
1	+5V _R Unswitched
2	GND
3	+5V _R Switched

Battery Modules to Conscience Fuser: JV

Connector: Waldom 03-06-10Y1

<u>Pin</u>	<u>Signal</u>
1	RCVR Source
2	RCVR Source (Fused)
3	PROC Source
4	PROC Source (Fused)

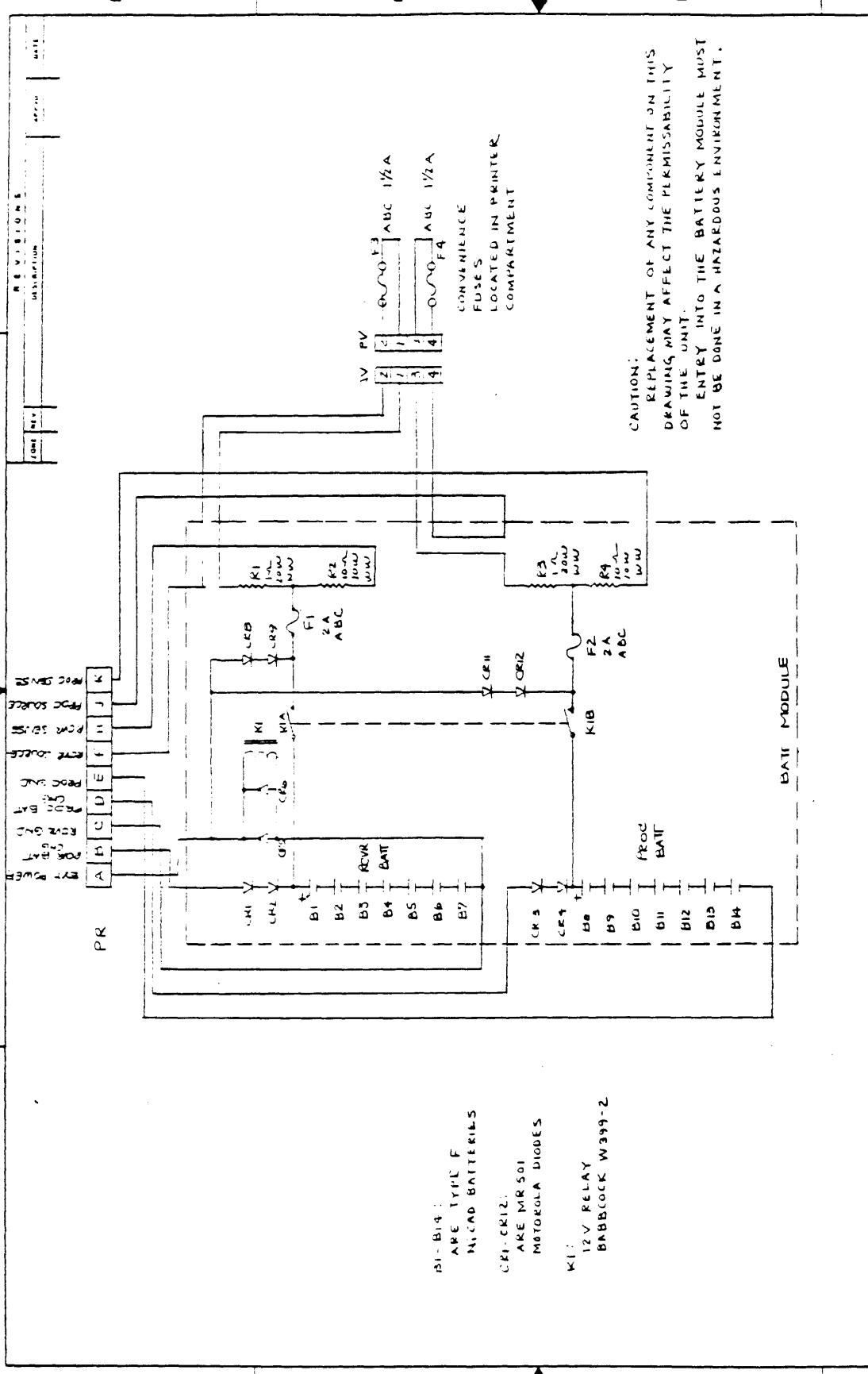
Front Panel Meter to Power Supply: JW

Connector: Waldom 03-06-1041

<u>Pin</u>	<u>Signal</u>
1	PROC GND
2	RCVR Source
3	PROC Source

Front Panel Meter to RCVR: JX
Connector: RCA Phono

<u>Pin</u>	<u>Signal</u>
Tip	RCVR VCXO Control Voltage
Ring	RCVR GND



B1 - B14 :
ARE TYPE F
NICAD BATTERIES

CR1 - CR12 :
ARE MR 501
MOTOROLA DIODES

K1 :
12V RELAY
BABBCOCK W399-2

CAUTION:
REPLACEMENT OF ANY COMPONENT ON THIS
DRAWING MAY AFFECT THE PERMISSIBILITY
OF THE UNIT.
ENTRY INTO THE BATTERY MODULE MUST
NOT BE DONE IN A HAZARDOUS ENVIRONMENT.

CONVENIENCE
FUSES
LOCATED IN PRINTER
COMPARTMENT

REV. NO.	DESCRIPTION	DATE

CONTRACT NO. HO171019

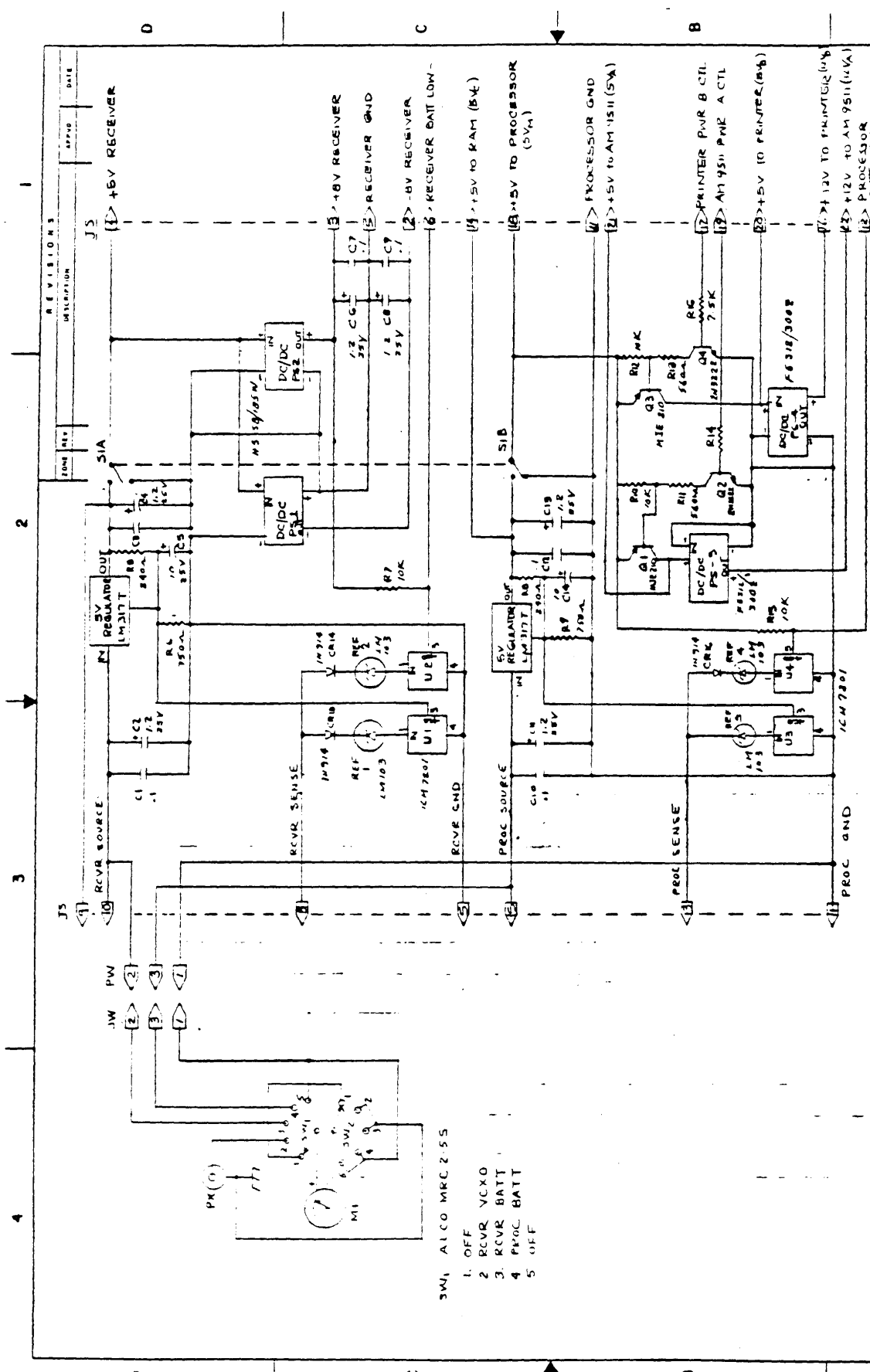
ENSCO, INC.
SPRINGFIELD, VIRGINIA

Schematic Diagram,
BATTERY MODULE

DATE: 4/17/64
BY: [Signature]

SIZE: C 06359 1202-C-3033

UNIT	QUANTITY	DESCRIPTION	REMARKS



SW1, ALICO MKC255

1. OFF
2. RCVR VCKO
3. RCVR BATT
4. PROC BATT
5. OFF

REV	DESCRIPTION	DATE
1	REVISIONS	

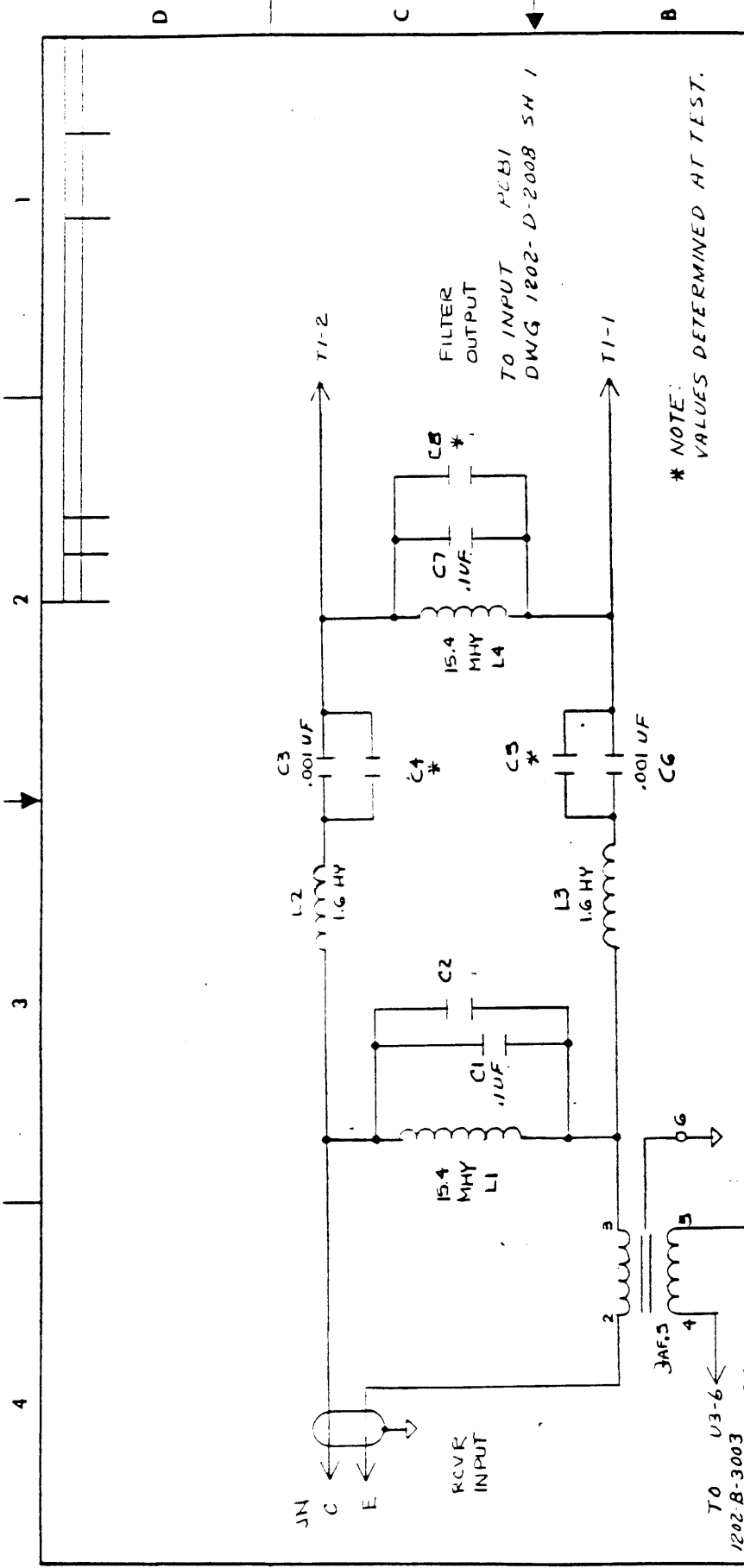
CONTRACT NO	HO177069
DATE	11/19
SIGNATURE	[Signature]
LEVEL	1
DESIGNER	[Name]
CHECKED	[Name]
DATE	11/19
SCALE	1:1
SHEET	1

ENSCO, INC.
SPRINGFIELD, VIRGINIA

SCHEMATIC DIAGRAM,
POWER SUPPLY -
RECEIVER/PROCESSOR

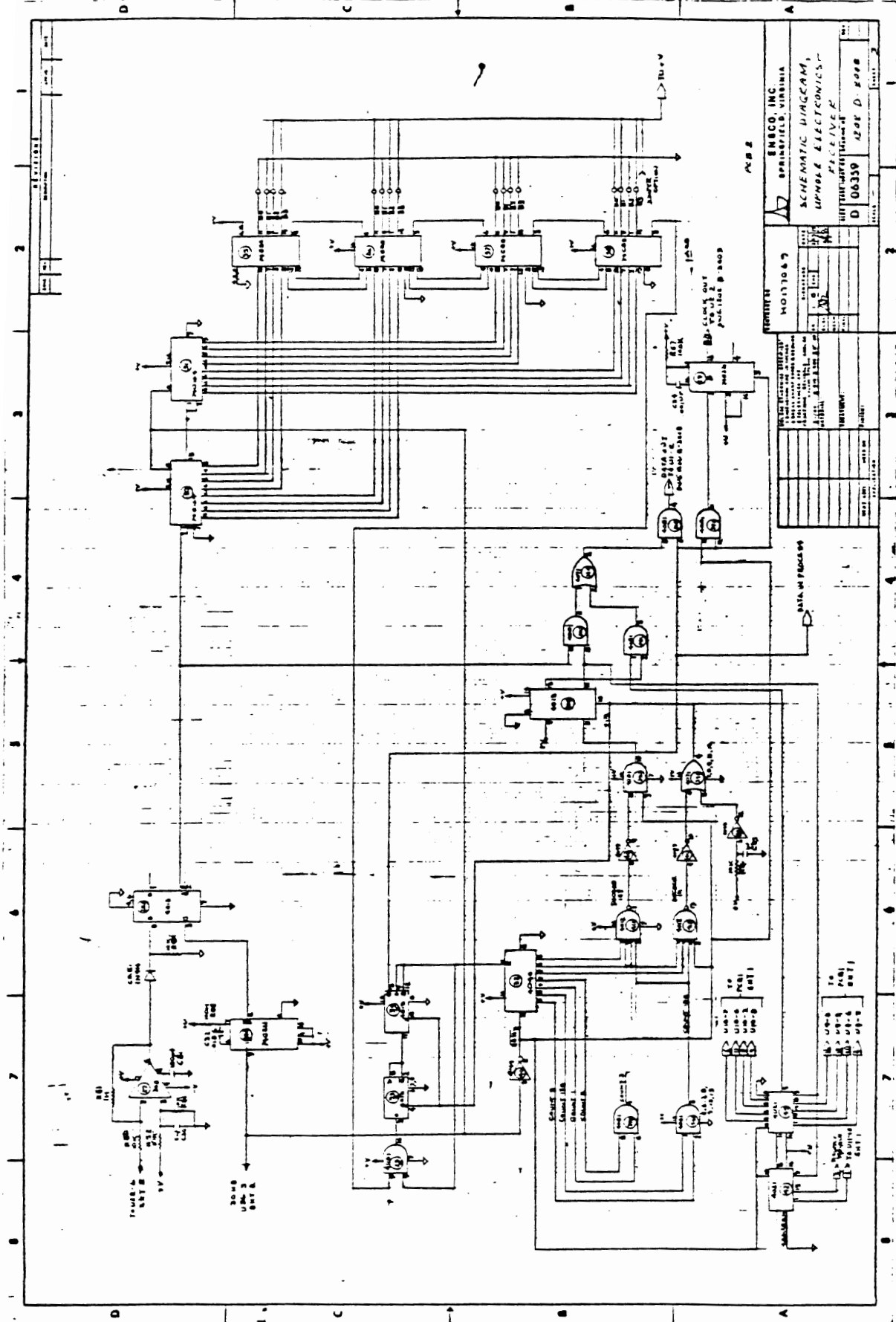
SIZE CODE IDENT NO DRWG NO
C 06359 1202 C-3020

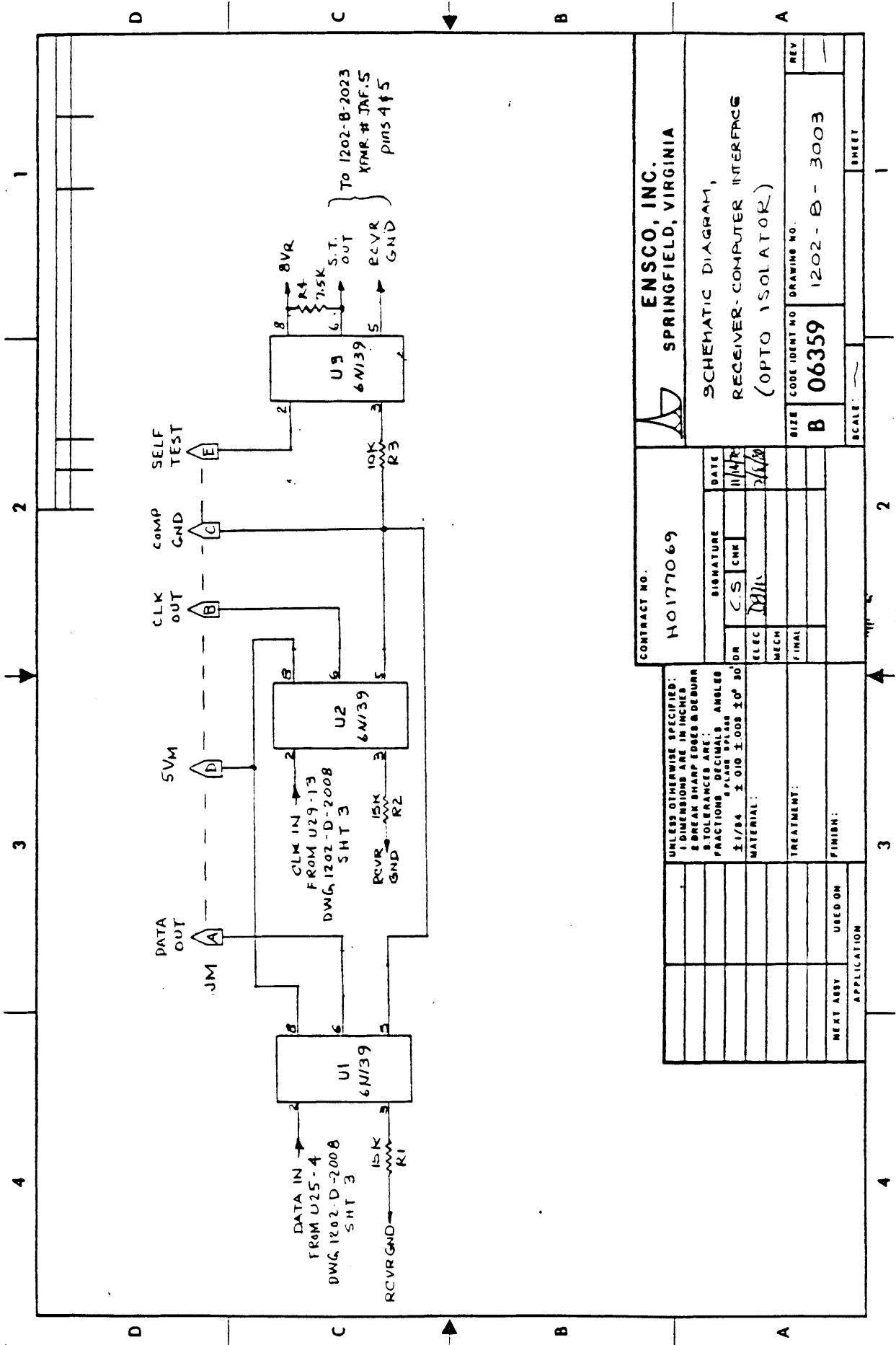
UNLESS OTHERWISE SPECIFIED
1 DIMENSIONS ARE IN INCHES
2 TOLERANCES ARE AS SHOWN
3 HOLE DIA TOLERANCE UNLESS
SPECIFIED OTHERWISE
4 UNLESS OTHERWISE SPECIFIED
5 UNLESS OTHERWISE SPECIFIED
6 UNLESS OTHERWISE SPECIFIED



* NOTE:
VALUES DETERMINED AT TEST.

ENSCO, INC. SPRINGFIELD, VIRGINIA		CONTRACT NO. HO177069	
Schematic Diagram, Uphole Electronics- Filter for Receiver			
SIZE B	CODE IDENT NO 06359	DRAWING NO. 1202-B-2023	
REV ---	SCALE: --- SHEET 1		
UNLESS OTHERWISE SPECIFIED: 1 DIMENSIONS ARE IN INCHES 2 BREAK SHARP EDGES & DEBUR 3 TOLERANCES ARE: FRACTIONS DECIMALS ANGLES $\pm 1/64$ $\pm .010$ $\pm .008$ $\pm 0^\circ 30'$		MATERIAL: TREATMENT: FINISH:	
SIGNATURE C.S. CHK DATE 2/23/74 2/16/74		ELEC MECH FINAL	
NEXT ASSY USED ON		APPLICATION	





ENSCO, INC.
 SPRINGFIELD, VIRGINIA

SCHEMATIC DIAGRAM,
 RECEIVER-COMPUTER INTERFACG
 (OPTO ISOLATOR)

CONTRACT NO. H0177069

DATE	11/17/78
SIGNATURE	<i>[Signature]</i>
DR	C.S. CHM
ELEC	
MECH	
FINAL	

UNLESS OTHERWISE SPECIFIED:
 1 DIMENSIONS ARE IN INCHES
 2 BREAK SHARP EDGES & DEBURR
 3 TOLERANCES ARE:
 FRACTIONS DECIMALS ANGLES
 ± 1/84 ± 0.01 ± 0.008 10° 30'

MATERIAL:

TREATMENT:

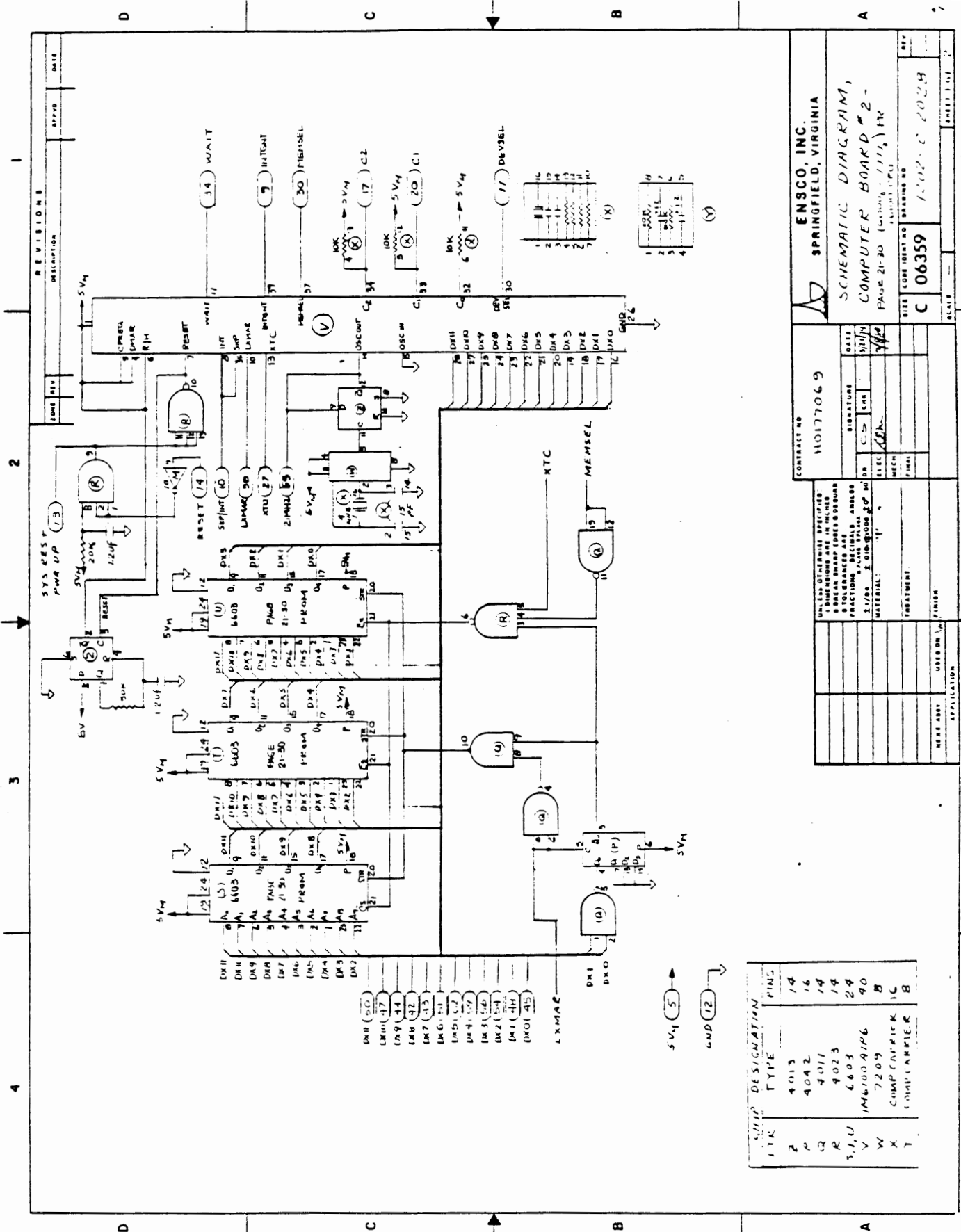
FINISH:

NEXT ASSY	USED ON
APPLICATION	

SIZE CODE IDENT NO DRAWING NO. REV

B 06359 1202-B-3003

SCALE: 1:1 SHEET 1



REVISIONS

NO.	DESCRIPTION	APPROV.	DATE

CONTRACT NO. HD177069

ENSCO, INC.
SPRINGFIELD, VIRGINIA

SCHEMATIC DIAGRAM,
COMPUTER BOARD #2 -
PAUSE 21-30 (REVISED 1/11/64) PK

DATE: 1/11/64
BY: JFB
CHECKED: JFB

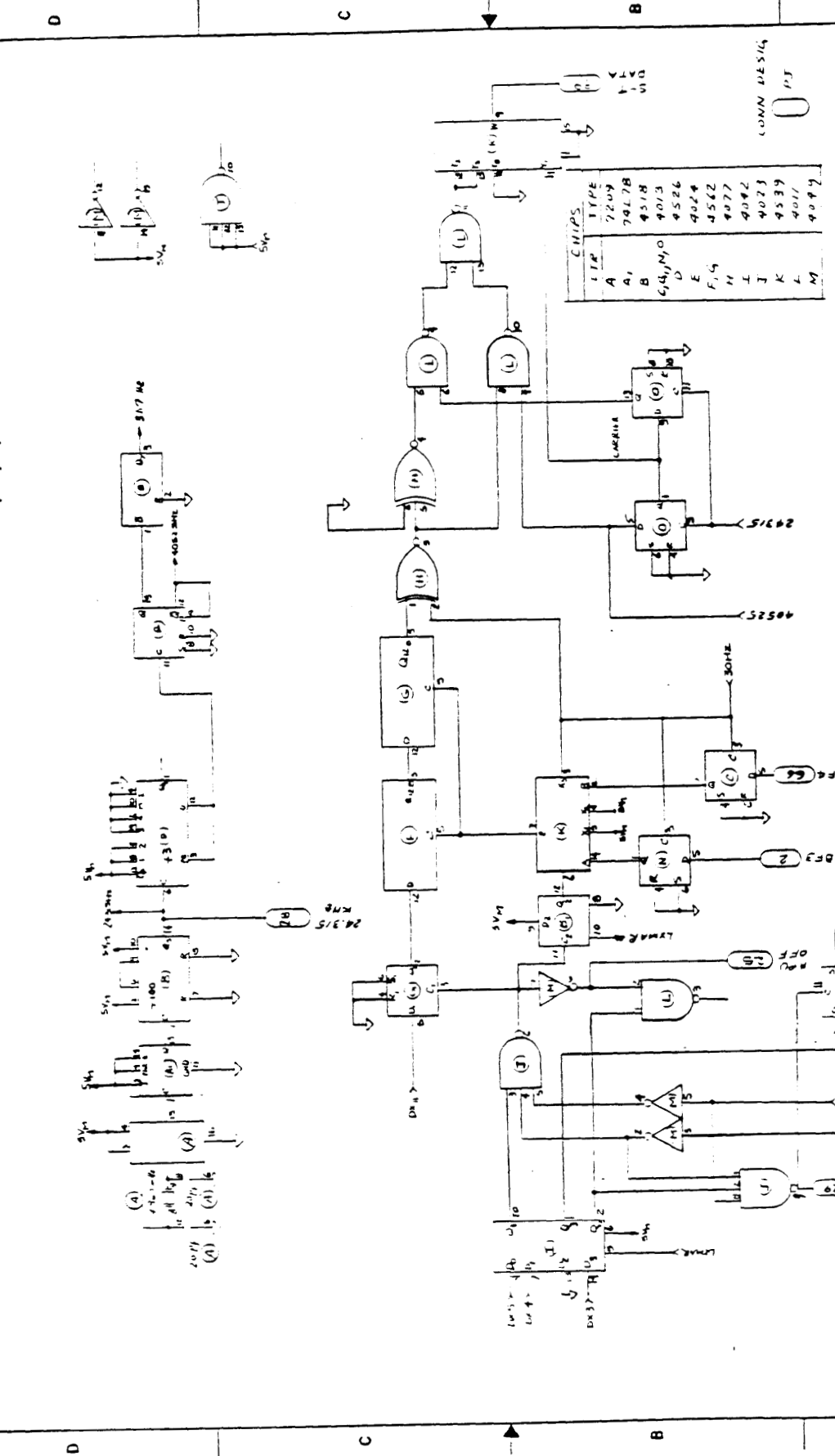
SIZE: 100 (100) NO. DRAWING NO. C 06359
SCALE: 1:1

UNLESS OTHERWISE SPECIFIED:
DIMENSIONS ARE IN INCHES
DIMENSIONS IN PARENTHESES ARE IN MILLIMETERS
FRACTIONS ARE TO BE DECIMALS
TOLERANCES ARE:
FRACTIONS: .010, .015, .020, .030, .040, .050, .060, .070, .080, .090, .100
DECIMALS: .005, .010, .015, .020, .030, .040, .050, .060, .070, .080, .090, .100
MATERIAL: .015" ALUMINUM
TREATMENT: ANODIZED

REV.	DATE	DESCRIPTION

ITK	DESIGNATION	PINC
2	4013	14
P	4042	16
Q	4011	14
R	4023	14
S, U	4003	24
V	7400	14
W	7209	8
X	COMPARATOR	16
Y	COMPARATOR	16

REV	DESCRIPTION	APPRO	DATE
1			
2			
3			
4			



LET	TYPE
A	7209
A1	74L7B
B	4318
C4, M, O	4013
D	4526
E	4024
F, S	4542
H	4077
I	4042
J	4023
K	4539
L	4011
M	4044

ENSCO, INC.
 SPRINGFIELD, VIRGINIA

CONTRACT NO. 110177069

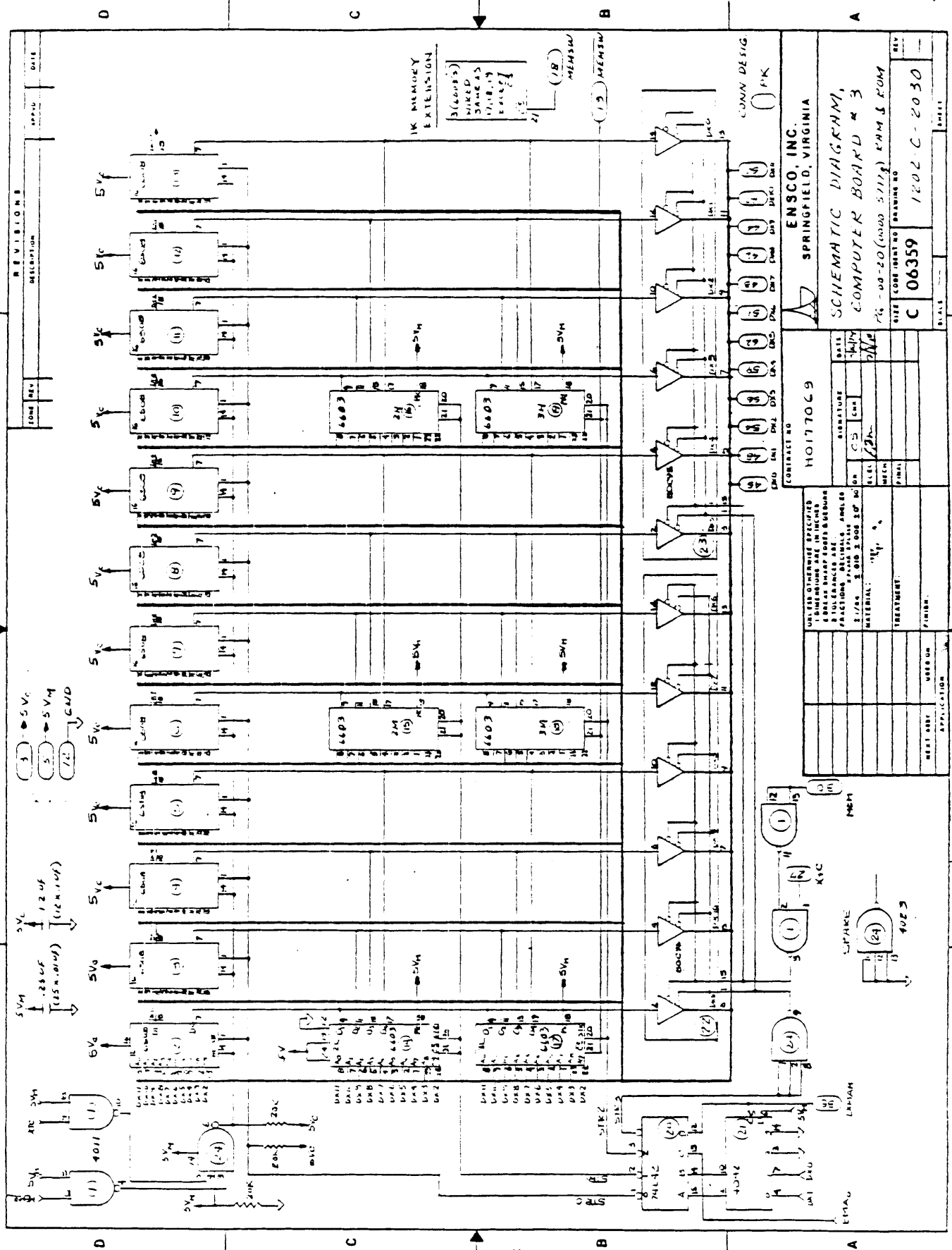
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES. TOLERANCES ARE: FRACTIONS, DECIMALS, ANGLES 1/16", 1/32", 1/64" 1/16", 1/32", 1/64"

DATE: 10/22/64
 SIGNATURE: [Signature]
 TITLE: [Title]

SIZE: C 06359
 SHEET NO: 1202-C-2028
 SHEET 2

SCHEMATIC DIAGRAM,
 COMPUTER BOARD #2
 SELF TEST

APP. CODES:
 6500 - READ & MEMSW
 8100 - MEMSW (CALLS UP MEMORY EXTENSION)
 6600 - CLOCK SR & MPU OFF



REV.	DESCRIPTION	DATE
1		
2		
3		
4		

ZONE	REV.
1	
2	
3	
4	

REV.	DESCRIPTION	DATE
1		
2		
3		
4		

1K MEMORY EXTENSION
 3 (4003's)
 WIRE
 SAME AS
 1718, 19
 21 (2)
 MEMSW

CONTRACT NO. HO177069
 ENSCO, INC.
 SPRINGFIELD, VIRGINIA

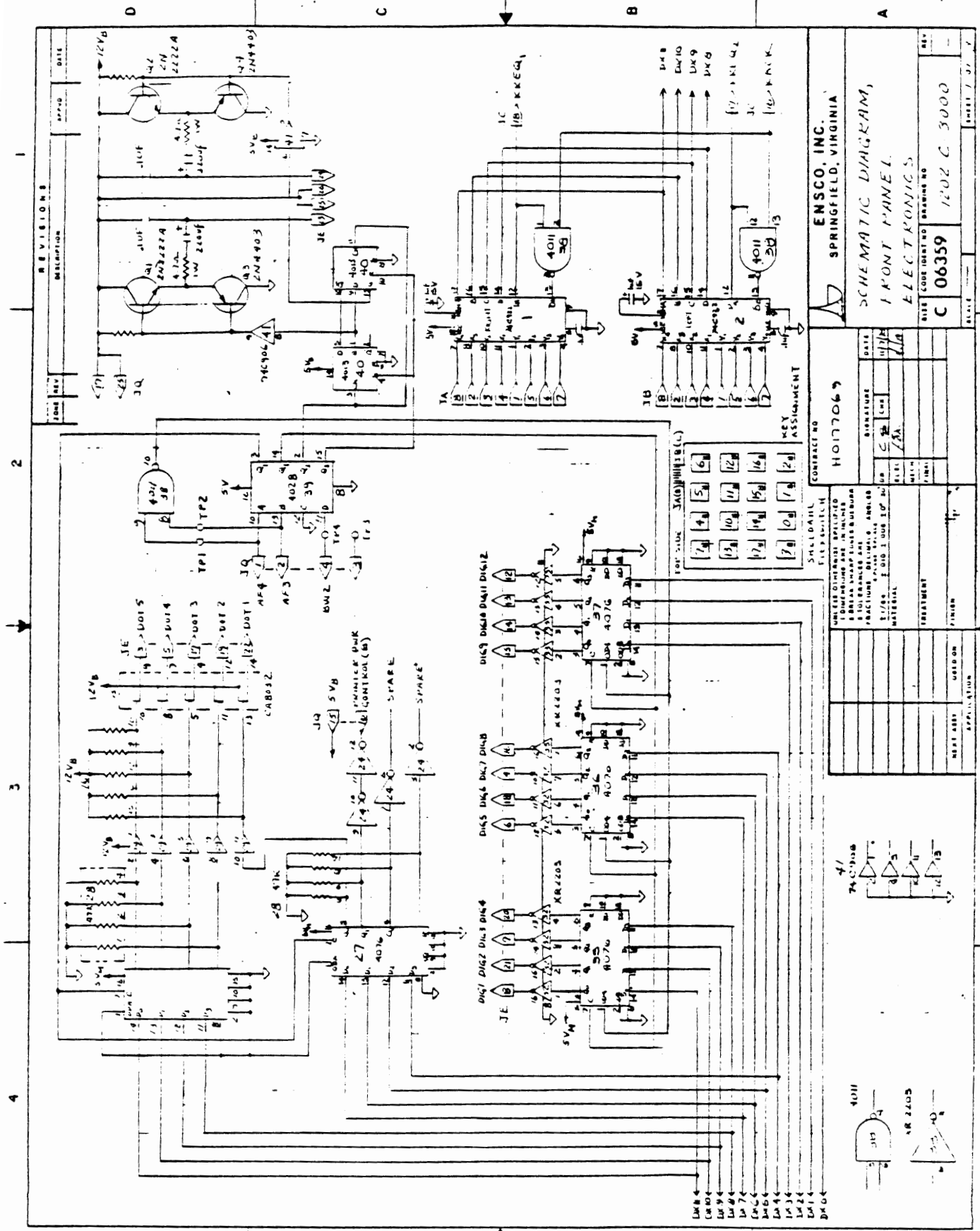
SCHMATIC DIAGRAM,
 COMPUTER BOARD # 3
 PG - 00-20 (0000 5112) KMM S ROM

SIZE CODE POINT NO DRAWING NO
C 06359 1802-C-2030

UNLESS OTHERWISE SPECIFIED
 DIMENSIONS ARE IN INCHES
 TOLERANCES ARE:
 FRACTIONS: BALLBORN, ANGLES
 2/1000 3/100 3/100 3/100 3/100
 MATERIAL: "NY" 9
 TREATMENT:

DATE: 1/24/64
 SIGNATURE: [Signature]
 DESIGNED BY: [Signature]
 CHECKED BY: [Signature]
 DRAWN BY: [Signature]
 FINISH:

APPLICATOR: [Signature]
 USED ON: [Signature]
 APPLICATION: [Signature]



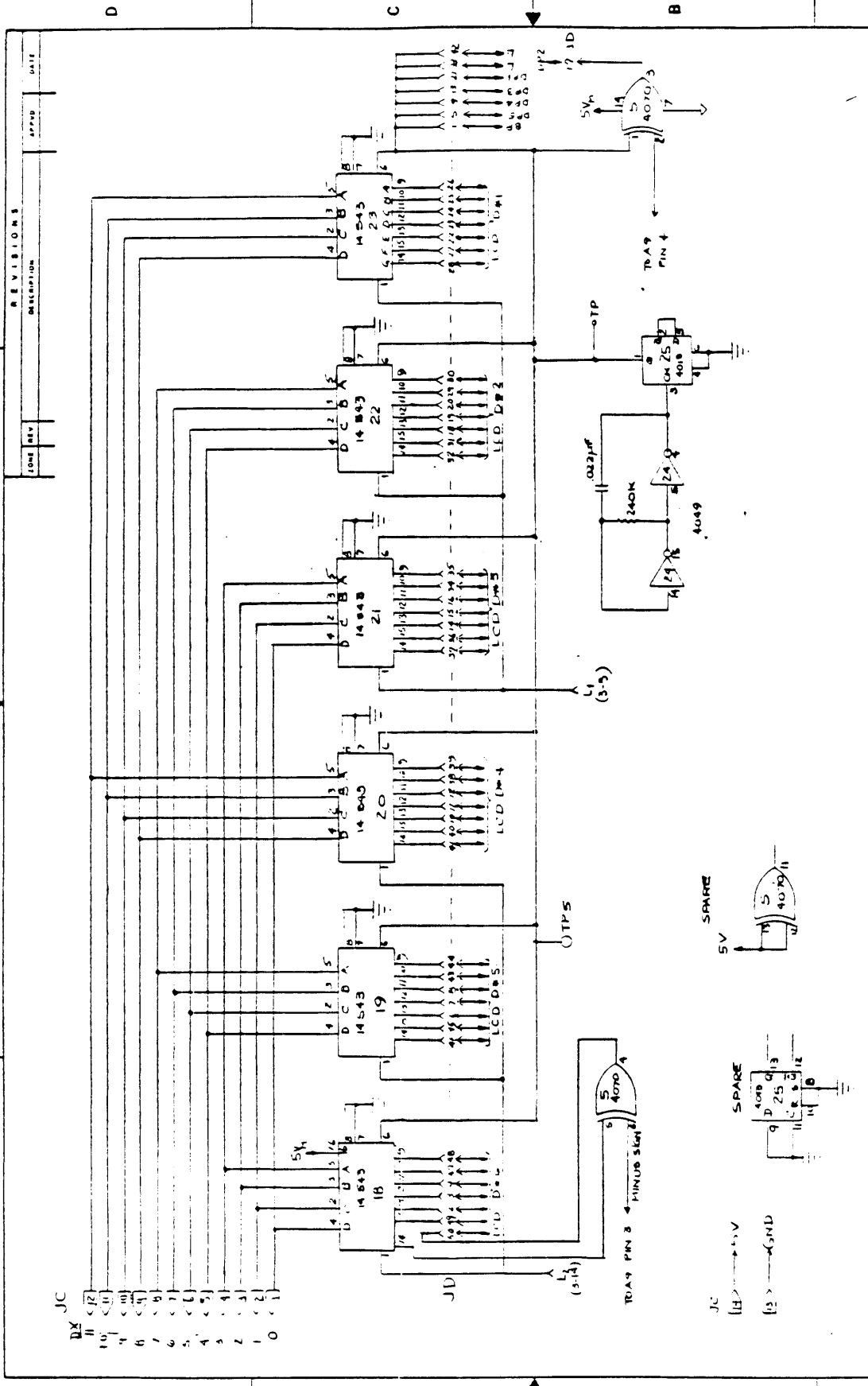
REV	DESCRIPTION	DATE
1		

ENSCO, INC.
 SPRINGFIELD, VIRGINIA
SCHEMATIC DIAGRAM,
FRONT PANEL,
ELECTRONICS

DATE	11/24
SIGNATURE	[Signature]
DESIGNER	[Signature]
DRW	[Signature]
CHECKED	[Signature]
APPROVED	[Signature]

CONTRACT NO	HO177069
UNLESS OTHERWISE SPECIFIED	
RESISTORS	5% TOLERANCE UNLESS OTHERWISE SPECIFIED
CAPACITORS	5% TOLERANCE UNLESS OTHERWISE SPECIFIED
WELDED	1/16" DIA 100% SOLDER
TREATMENT	
FINISH	
REPT. NO.	
APPLICATION	
ORDER NO.	

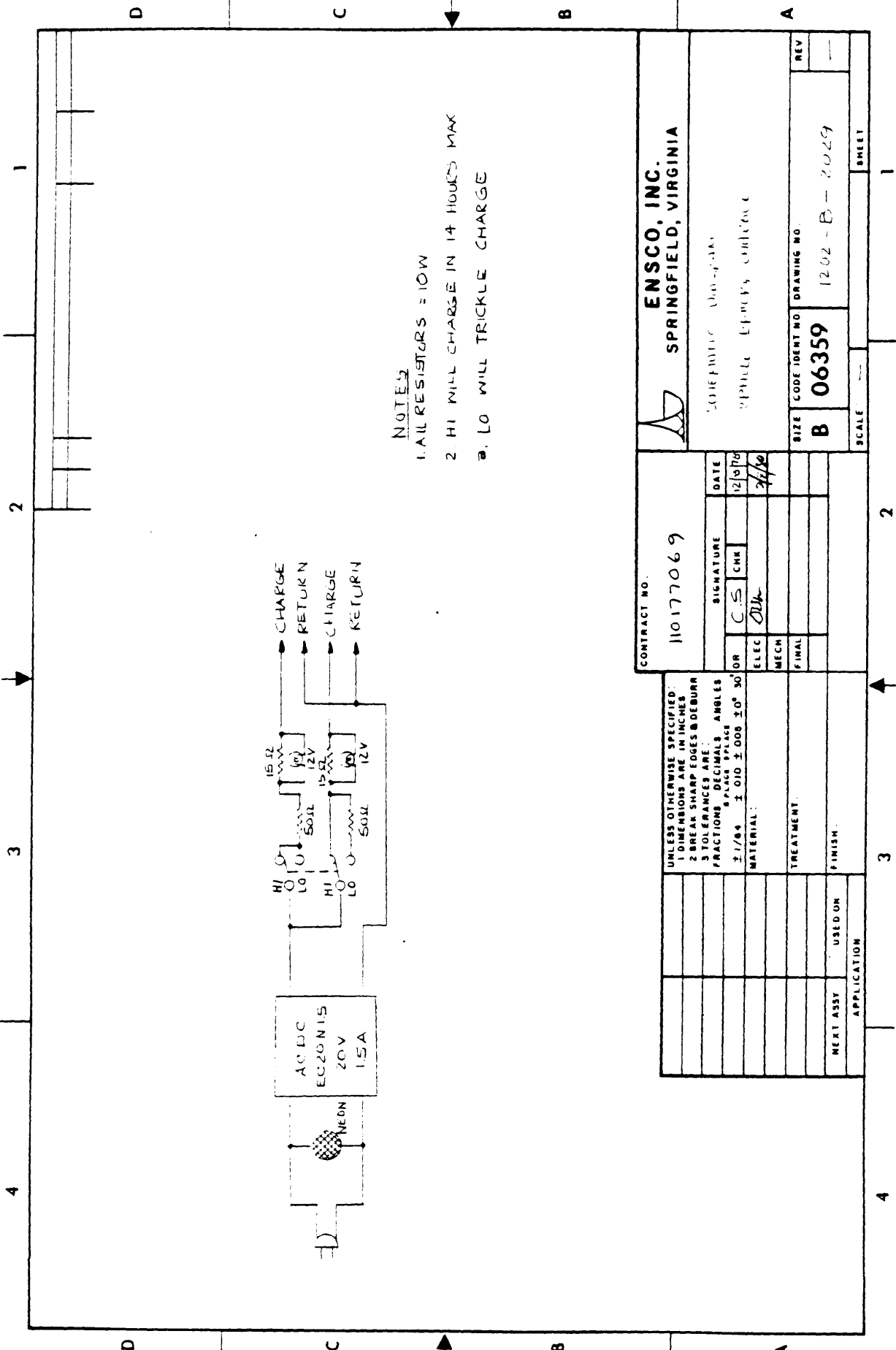
PART CODE IDENT NO. **06359**
 DRAWING NO. **1202 C 3000**




REV	DESCRIPTION	DATE

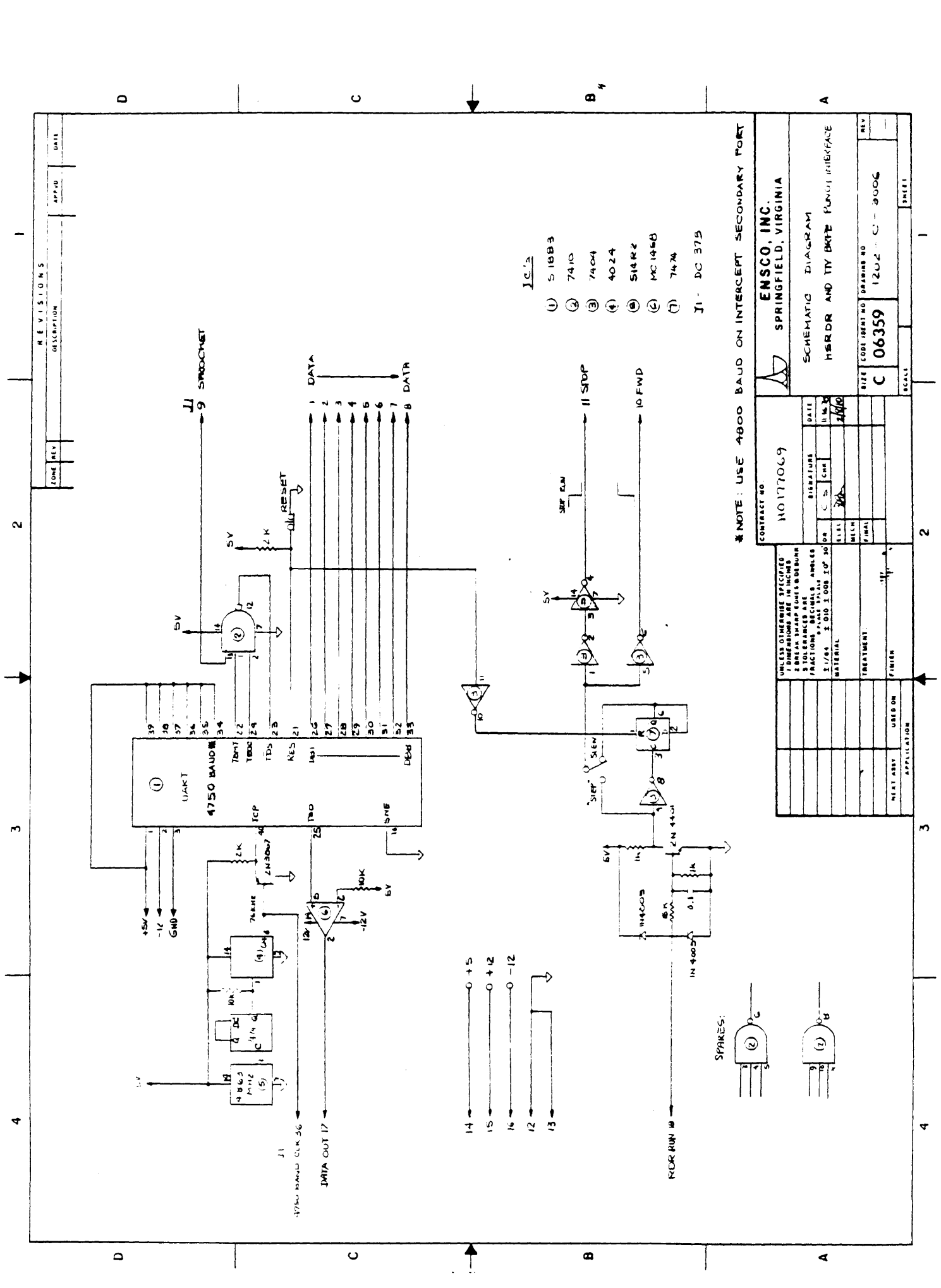
ENSCO, INC. SPRINGFIELD, VIRGINIA	
SCHEMATIC DIAGRAM, FRONT PANEL ELECTRONICS	
CONTRACT NO 110177069	SIZE 11/16"
SIGNATURE C 5 1/1/62	CHECKED C 5 1/1/62
DATE 1/1/62	MATERIAL 1/1/62
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE FRACTIONS DECIMALS ANGLES 1/100 0.010 0.005 0° 0' 0"	TREATMENT FINISH
PART NO USED ON	APPLICATION
QTY 1200 C-5000	SHEET 2 OF 2

The following schematics represent auxillary equipment developed during this project, but are not part of either the downhole or uphole package. None of these items are required for operational use.



NOTES
 1. ALL RESISTORS = 10W
 2. HI WILL CHARGE IN 14 HOURS MAX
 3. LO WILL TRICKLE CHARGE

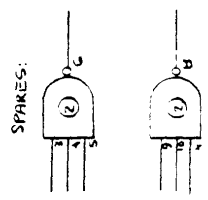
 ENSCO, INC. SPRINGFIELD, VIRGINIA		CONTRACT NO. 110177069	
SIZE B		CODE IDENT NO 06359	
DRAWING NO. 1202-B-2029		SHEET 1	
SCALE ---		DATE 12/10/79	
SIGNATURE <i>[Signature]</i>		CHECKED <i>[Signature]</i>	
ELEC <i>[Signature]</i>		MECH ---	
FINAL ---		MATERIAL ---	
TREATMENT ---		FINISH ---	
NEXT ASSY ---		USED ON ---	
APPLICATION ---			



- IC's**
- (1) 514R2
 - (2) 7410
 - (3) 7404
 - (4) 4024
 - (5) 514R2
 - (6) MC1448B
 - (7) 7474
 - J1 - DC 375

*NOTE: USE 4800 BAUD ON INTERCEPT SECONDARY PORT

CONTRACT NO. 140177069		DATE 11/13/83	
SIGNATURE C. S. GIBSON		MECH J. H. HARRIS	
UNLESS OTHERWISE SPECIFIED 1 DIMENSIONS ARE IN INCHES 2 BREAK SHARP EDGES UNLESS OTHERWISE SPECIFIED 3 1/8" 3.000 1 OF 30 MATERIAL		TREATMENT: FINISH: USED ON: APPLICATION:	
SIZE C	CODE 06359	DRAWING NO. 1202	REV. C-3006
SCHEMATIC DIAGRAM		HSRDR AND TTY BRKP PUNCH INTERFACE	
ENSCO, INC. SPRINGFIELD, VIRGINIA		SHEET	



The microprocessor employed in the uphole processor is the Intersil IM6100. It is a 12 bit CMOS type LSI Integrated Circuit that evaluates the software of the Digital Equipment Corporation (DEC) PDP8/E. All of the assembly language programs listed below are assembled using PDP8/E assembler available from DEC.

COMPUTER PROGRAM INDEX

PROGRAMS

ACC	Accumulate keyboard #'s
ANG,AVG	Displays angle average
ANGA,ANGE	Displays angle; changes keyboard # to radians
AON	Turns on APU power
APU DRIVERS	FLT; DIVF; ADDF; SUBF; PUSH; ARTAN; POP; MULF; MULD; ARSIN; SORT; FIX; DIVD; SUBD; SINE; CRAB; BW; WTAPUF; RDAPUF
APU OPERATORS	LDS; ADDS; MULS; XCH CHS
AVGV	Averages values
BATCHK	Checks batteries
BLANK & DISPR	Writes Display
BRTAB	KYSR branch table
CHEK	BATCHK extended
CHLITE	Changes lights
COM,COM1	Compares 2 values for out of limits
CONOE	Continue or enter
CONV	Displays memory
DATA	Accepts receiver data
DATCAL	Calculates data; battery condition and temperature
DAT1	DATCAL extended
DELAY	Delay
DIP/CAL	Calculates dip angle
DISCO	Displays code
DISTR	Distributes data for APU
DOOB	Loads and floats #
ENT	Enters 10,000
EXEC	Examines and modifies
EXEC OVERFLOW	EXEC extended
EXITE	EXEC extended

COMPUTER PROGRAM INDEX (CONT'D.)

FAULT	Handles the 9 code
GET	Gets a data word
GETIN	Computes initial conditions
GTIN	Sequences initial conditions
GTIN EXTENDED	Extends rouginte GTIN
INIT	Initialization bootstrap
INITCO	Initial conditions print routine
KYBLK	Key blank; KYSR patch
KYEX	KYSR extended
KYSR	Left-hand keyboard service routine
KYSRC	KYSR calling routine
LOA,B	Lights off - A,B
LSW	Least significant word
MAIN1	Main program, part 1
MAIN2	Main program, part 2
MA1EX	MAIN1 extended
MONITOR	System monitor
M2EX	MAIN2 extended
NORM	Normalizes data
ONES FILLER	Fills memory with 1's
PIAS	Pi; add or subtract
POF	Adds .005
PRINT	Operates printer
PRINT ROUTINES	INCO; RST; SUR
PROC1	Process 1
PROC2	Does survey calculations
PROM BURNER	Burns programmable read-only memory chips
PROPA	Process 1 extended
RBAT	Checks receiver batteries
RDT	Handles data monitoring
RESTR	Restart-print routine
RESTART	Restart
RSTC	Restart calling routine

COMPUTER PROGRAM INDEX (CONT'D.)

SCDATA	Scale data
SELF TEST CALLS & PATCHES	STST; STSTD; STSTC
STATUS	Checks sign of APU #
STEST	Self test
STESTC	Self test calling routine
STZ	Scale data; call
SUM	Sums keyboard numbers
SURVEY	Survey-print routine
TEME	Temperature errors
WAIT	Waits for receiver clock
.005 FLOAT	Supplies the number .005

PIA1 /from P1...Add or Subtract

♦2305

```
2305 1043 P1A1, TAD PBUF:/ if PBUF is 0
2306 7650   DCA CLA:
2307 5320   JMP P10: /return
2310 4172   CALL: /otherwise, load P1 and proceed
2311 6144   P1:
2312 1033   TAD KEYT: /if keyt hard 0
2313 7650   DCA CLA:
2314 5317   JMP P13 /add P1
2315 4156   3: /otherwise, subtract P1
2316 5320   JMP P10
2317 4153   P13, A
2320 5575   P10, RETURN
```

NORM

♦2337

```
2337 7774 FORM, -4:
2340 7775 THM, -3
2341 3042 NORM, DCA CTR2: /make CTR2 point to beginning of data
2342 1340 TAD THM: /make CTR count 3 things
2343 3020 DCA CTR:
2344 1042 TAD CTR2 /AC point to 1st word
2345 4137 MA, 0: /write the word
2346 4145 P: /square it
2347 4150 M:
2350 1010 TAD TEM: /"w" makes TEM point to next word
2351 2020 IIC CTR: /3 times?
2352 5245 JMP MA: /no, do it again
2353 4153 A: /yes, do  $(DW1)^2 + (DW2)^2 + (DW3)^2$ 
2354 4153 A:
2355 4172 CALL: / $\sqrt{(DW1)^2 + (DW2)^2 + (DW3)^2} = N$ 
2356 2703 IORT:
2357 1340 TAD THM /set up CTR for 3 things again
2360 3020 DCA CTR:
2361 1042 TAD CTR2: /point to 1st word again
2362 3010 DCA TEM
2363 4145 ME, P: /save N
2364 1010 TAD TEM: /write DW1
2365 4137 M:
2366 4172 CALL: /do  $DW1 \div N$ 
2367 3144 NCH:
2370 4161 D:
2371 1010 TAD TEM: /point back to DW1
2372 1337 TAD FORM: /replace DW1 with  $DW1 \div N$ 
2373 4142 P:
2374 3020 IIC CTR: /3 times?
2375 5245 JMP PE /no, do it again
2376 5575 RETURN /yes
```

PPDC1

P=4145;
 M=4150;
 F=4142;
 W=4137;
 I=4156;
 SINE=2723;
 ARDIN=2677;
 ARTAN=2655
 D=4161;
 MOH=3144;
 A=4153;
 PEUF=43;
 WEYT=33;
 STATUS=4347;
 CALL=4172;
 RETURN=5575
 TEM=10;
 QDS=6136;
 PI=6144;
 COST=2703;
 CTR2=42;
 CTR=20;
 CHS=3761;
 PGR=2261;
 PROPA=2220
 ◆2000

2000 0373 PIT, 373;
 2001 0257 66M, 257;
 2002 0257 65Y, 257;
 2003 0263 66Z, 263;
 2004 0253 YCOO, 253;
 2005 0243 YCOO, 243;
 2006 0247 YCOO, 247;
 2007 0513 INCE, 513;
 2010 0357 COCT, 357;
 2011 0317 DIP, 317;
 2012 0323 CIND, 323;
 2013 0227 COOD, 227;
 2014 0233 COOP, 233;
 2015 0237 CINF, 237;
 2016 0333 FSI, 333;
 2017 0223 F1, 223;
 2020 0227 F2, 227;
 2021 2020 FOO, FOO-1;
 2022 0227 227;
 2023 0243 243;
 2024 0172 172;
 2025 2024 TMO, TMO-1;
 2026 0000 0;
 2027 0200 200;
 2030 0002 2

```

2031 7300  PROC1, CLR:
2032 1201  TAD GSK:
2033 4137  M:
2034 4172  CALL:
2035 2677  RFIN:
2036 4145  R:
2037 1200  TAD PIT:
2040 5641  JMP I .+1: /patch in PROPA (W;XCH;CHS;A)
2041 6260  PROPA:
2042 1207  TAD INCB
2043 4142  R:
2044 4172  CALL:
2045 6136  COS:
2046 1210  TAD COCT:
2047 4142  R:
2050 1211  TAD DIP:
2051 4137  M:
2052 4145  R:
2053 4172  CALL:
2054 2723  SINE:
2055 1212  TAD SIND:
2056 4142  R:
2057 4172  CALL:
2060 6136  COS
2061 4145  R:
2062 1213  TAD COID:
2063 4142  R:
2064 1210  TAD COIT:
2065 4137  M:
2066 4150  M:
2067 1204  TAD XCOI:
2070 4137  M:
2071 1212  TAD SIND:
2072 4137  M:
2073 1201  TAD GSK:
2074 4137  M:
2075 4150  M:
2076 4156  S
2077 4172  CALL:
2100 3144  XCH:
2101 4161  D:
2102 1214  TAD COCF:
2103 4142  R:
2104 1202  TAD GSY:
2105 4137  M:
2106 4172  CALL:
2107 3761  CHI:
2110 4172  CALL:
2111 4347  STATUS:
2112 3033  DCA FEYT
2113 1203  TAD GSC:
2114 4137  M:
2115 4172  CALL:
2116 3761  CHI:
2117 4172  CALL:
2120 4347  STATUS:
2121 3043  DCA FEUF:
2122 4161  D:

```

```

2123 4172 CALL:
2124 2655 RSTAN:
2125 4172 CALL:
2126 2305 PIAS:
2127 4145 R:
2128 1216 TAD RPI:
2129 4142 R:
2130 4145 R:
2131 4172 CALL:
2132 2723 DINS:
2133 1206 TAD COOS:
2134 4137 M:
2135 4150 M:
2136 4172 CALL:
2137 3144 MCH:
2138 4172 CALL:
2139 6128 COI:
2140 1205 TAD YCOO:
2141 4137 M:
2142 4150 M:
2143 4156 S:
2144 1213 TAD COOD:
2145 4137 M:
2146 4161 D:
2147 4172 CALL:
2148 4347 STATUS:
2149 3033 DCA MEYT:
2150 1214 TAD COOP:
2151 4137 M:
2152 4145 R:
2153 4172 CALL:
2154 4347 STATUS:
2155 3043 DCA RBUF:
2156 4172 CALL:
2157 2661 POP:
2158 4161 D:
2159 4172 CALL:
2160 2655 RSTAN:
2161 4172 CALL:
2162 2305 PIAS:
2163 4172 CALL:
2164 3761 CHS:
2165 5776 JMP I .+1:
2166 2200 RR
      ◆2200
2200 1207 RA, TAD MSVR:
2201 4137 M:
2202 4156 S:
2203 1210 TAD BEER:
2204 4142 R:
2205 5579 RETURN:
2206 0337 PHI, 337:
2207 0347 MSVR, 347:
2210 0507 BEER, 507

```

DATA

```

    TEND=77
CALL=4172          Loads up the data bytes
    RETURN=5575
    DATD=74
    READD=6500     Comes back with AC=0...timeout
    TEM1=26        error, >25 ms between clks
    TEM2=DATD      1...no errors
    CTR=20
    CTR1=22
    CTR2=42
    B2B=6443
    PBUF=43
    LDR=3154

```

→2400

```

2400  7742  TN,      -36
2401  0243  DAT1,    243
2402  0001  MKK,     1
2403  7766  TE,     -12
2404  0006  SI,      6

2405  7305  DATA,   CLR CLL IAC RAL /00023
2406  4172          CALL
2407  2634          DICCO /display "2"
2410  4172          CALL
2411  3154          LDR/lights off
2412  7120          CTL/make sure all of L4 is off
2413  4172          CALL
2414  2512          CHLITE
2415  1200          TAD TN/set CTR up to count 3010 data bits that will
2416  3020          DCA CTR/#1 has already been 10 be thrown away
2417  5224          JMP GARB1      thrown away by EXEC, so
2420  4172  GARB,   CALL      /jump right to GARB1
2421  2557          WAIT
2422  7450          DNR
2423  5575          RETURN
2424  3077  GARB1,  DCA TEMD/has a 1 if no timeout error here
2425  2020          ISZ CTR
2426  5220          JMP GARB/throw away another one
2427  1201          TAD DAT1/addr of 1st 4 byte data location
2430  3010          DCA 10/into an autoindex
2431  1203          TAD TE/CTR1 is channel counter, set up with 1010
2432  3022          DCA CTR1
2433  3043  A,      DCA PBUF/clear PFOB
2434  4172          CALL/get a data word of 1210 bits
2435  3727          GET
2436  7450          DNR CLA/timeout error?
2437  5575          RETURN /yes
2440  1074          TAD TEM2/get data word
2441  7004          RAL/adjust it to be 2's complement binary
2442  7040          DNR

```

lower order 8 bits

higher order 4 bits

```

2443 7010 RAR
2444 3074 DCA TEM0/and save it
2445 4172 CALL/form 16 bit # in TEM2(LO) & TEM1(HI)
2446 3203 DISTR
2447 1074 TAD TEM0/get data word LO
2450 3410 DCA I 10/put in 1st of 4 bytes (i.e., location 244 & 245)
2451 1022 TAD TEM1/get data word HI
2452 3410 DCA I 10/put in 2nd of 4 bytes. Now a single precision 16 bit
2453 3410 DCA I 10 /INCR autoindex integer is available in the for
2454 3410 DCA I 10 /INCR autoindex the APU likes
2455 4172 CALL/wait for next clock
2456 2557 WAIT
2457 7650 SNA CLA/timeout error?
2460 5575 RETURN/yes
2461 7300 CLA CLL/no, get parity bit
2462 6500 READD
2463 0202 AND MSK/mask off LSB, bit 11
2464 1043 TAD FEUF/add the parity counter
2465 7010 RAR/get CSB of result into link
2466 7630 SEL CLA/Parity OK?
2467 5273 JMP C /no
2470 2022 ISZ CTR1/parity OK, chalk up another channel in CTR1
2471 5233 JMP A /get another one
2472 5305 JMP D /all done
2473 7040 C, EMA/turn on data error light
2474 7421 MQL
2475 7010 RAR/link is set, so make bit 0=1 for "data error" light
2476 4172 CALL/do it
2477 2512 CHLITE
2500 1204 TAD EI/display a "6" for parity error
2501 4172 CALL
2502 3234 DISCO
2503 3077 DCA TEM0/put a 0 in TEM0 to signal "data error"
2504 5233 JMP A /get another word without stopping
2505 4172 D, CALL/get receiver data
2506 3727 GET
2507 7650 SNA CLA/timeout error?
2510 5575 RETURN/yes
2511 1074 TAD TEM2/TEM2 has binary receiver data
2512 3410 DCA I 10 /put it into last data location
2513 1077 TAD TEM0/recall error info
2514 5575 RETURN
    
```

CHLITE /CHANGE LITE

LINK: 0=L3 latches
 1=L4 latches
 MO: 0=turn off an item
 0=turn on an item
 AC: bit to be turned on or off
 turn on-all zeros but desired bit
 turn off-all ones but desired bit

L3R=44
 L4R=21
 MCRAR=6425
 AM2=6431
 TEMC=73

♦2516

2516	3026	CHLITE.	DCR TEM1/hold AC
2517	7430		SEL/L3 or L4?
2520	1352		TAD L4/AC=1400g signifies L4 latches
2521	1351		TAD L3/AC=1000g signifies L3 latches
2522	6425		MCRAR/select the appropriate latch
2523	7630		SEL CLR
2524	5330		JMP T
2525	1353		TAD CH3/if L3, load TEMC with L3R address
2526	3073		DCR TEMC
2527	5332		JMP U
2530	1354	T.	TAD CH4/if L4, load TEMC with L4R address
2531	3073		DCR TEMC
2532	7321	U.	JMP/see if it's a turn on or a turn off
2533	7640		DCR CLR
2534	5341		JMP CH2/its a turn on
2535	1473		TAD I TEMC/get contents of latch register for turn off
2536	0025		AND TEM1/turn off the selected bit (i.e., latch the register)
2537	6431		AM2 /by doing an AW2
2540	5342		JMP EXIT
2541	1473	CH2.	TAD I TEMC/get contents of latch register
2542	7421		MOL/out in MO so can do an OR
2543	1026		TAD TEM1/get the turn on word
2544	7301		MOR/OR the latch register with the desired turn on word
2545	6431		AM2/turn on that bit
2546	3473	EXIT.	DCR I TEMC/update the latch holding register
2547	7100		CLL
2550	5573		RETURN
2551	1000	L3.	1000
2552	0400	L4.	400
2553	0044	CH3.	L3R
2554	0021	CH4.	L4R

		WAIT	Return with AC=1 if no timeout error, else AC=0
2555	0005	FI,	5
2556	4416	WATE.	-3362
2557	1355	WAIT.	TAD WATE/load CRT2 with timeout delay
2560	3042		DCR CTR2
2561	6443	W1,	BSZ/data clock?
2562	5285		JMP W2/no, jump to count down for timeout
2563	7201		CLA IAC/set AC=1
2564	5575		RETURN
2565	2042	W2,	ISZ CTR2/incr timeout counter
2566	5361		JMP W1/check again for data clock
2567	7340		CLA CLL CMA/signal "L3" & "turn on" to CHLITE
2570	7421		MQL
2571	7130		STL RAR/set "data error" bit
2572	4172		CALL
2573	2516		CHLITE/tight up "data error"
2574	1355		TAD FI/send "5" message code to display
2575	4172		CALL
2576	3234		DISCO
2577	5575		RETURN

		GET	Forms a raw 12 bit data word & return with PBUF indicating parity of that word
			♦3725
3725	0001	MSK1,	1
3726	7264	TM,	-14
3727	1326	GET.	TAD TM/CTR will count 12 ₁₀ bits
3730	3020		DCR CTR
3731	3074		DCR TEM2/clr TEM2, the data word accumulator (DWA)
3732	7004	GET1,	RAL/get link back in bit 11
3733	1074		TAD TEM2/put into DWA
3734	7004		RAL/move to the left
3735	3074		DCR TEM2/store back
3736	4172		CALL /wait for a data clk
3737	2557		WAIT
3740	7450		DNA/timeout error?
3741	5575		RETURN/yes
3742	7300		CLA CLL
3743	6500		FEADD/read a data bit (appears in AC's LSB)
3744	0325		AND MSK1 /and mask it off
3745	7010		RAR /put it in link
3746	7430		SEL/is it a 1?
3747	2043		ISZ PBUF/yes, count it in PBUF
3750	2020		ISZ CTR/no or yes, count # of bits, skip if 12 ₁₀ counted
3751	5332		JMP GET1/get another one
3752	7004		RAL/put LSB of data into bit 11
3753	1074		TAD TEM2 /add to DWA
3754	3074		DCR TEM2 /& replace
3755	7101		CLA IAC /signal no timeout error
3756	5575		RETURN

<DIITP

Forms a 16 bit 2's complement binary # for APU from data word

```

♦3200
3200 0010  MASK, 10
3201 0360  MIN, 360
3202 7774  FR, -4
3203 7681  DIITP, CAM
3204 1302  TAD FR /set up CTR to count 4 times
3205 3020  DCA CTR
3206 1074  TAD TEM2/get data word
3207 7100  DIS1, CLL/get 4 msb's into 4 LSB's of MO
3210 7004  RAL
3211 7521  SWP
3212 7004  RAL
3213 7521  SWP
3214 3020  ISZ CTR
3215 5207  JMP DIS1
3216 7012  RTR/put 8 LSB's of data word back in place
3217 7012  RTR
3220 3074  DCA TEM2/store in TEM2, call it DATA WORD LOW
3221 7521  SWP
3222 3026  DCA TEM1/store in TEM1, call it DATA WORD HI
3223 1026  TAD TEM1
3224 0200  AND MASK/mask off sign bit
3225 7650  SNA CLA/negative?
3226 5230  JMP .+2
3227 1201  TAD MIN/its negative...fill in one's for the 8 bit APU
3230 1026  TAD TEM1/get DATA WORD HI
3231 3026  DCA TEM1/restore
3232 7100  CLL
3233 5575  RETURN

```

<DISCG

```

BLANK=3606      Enter with # to be message in AC
TEMD=75        exits with that # saved in TEMD
DIS3=3672
D1=24
D2=25
DISFF=3630

```

♦3234

```

3234 3075  DISCG, DCA TEMD:/save AC
3235 4172  CALL:/blank display
3236 3606  BLANK:
3237 1075  TAD TEMD:/get display number
3240 1250  TAD MASK /put all one's in first two MSD's of display
3241 3025  DCA D2:/put in D2
3242 7040  SNA:/put all 1's in last 3 MSD's of display
3243 3024  DCA D1:
3244 4172  CALL:/DIS3 puts D2-D1 onto display
3245 3672  DIS3:
3246 7200  CLA:
3247 5575  RETURN:
3250 7760  DMCH, 7760

```

VDWT

◆3852

```
3852 0373 PIT, 373;  
3853 0387 LD, 387;  
3854 0433 VD, 433;  
3855 0453 WDEV, 453;  
3856 4137 VDWT, M;  
3857 1252 TAD PIT;  
3860 4137 M;  
3861 4156 S;  
3862 4172 CALL;  
3863 2723 DINE;  
3864 4150 M;  
3865 1253 TAD LD;  
3866 4137 M;  
3867 4150 M;  
3870 1254 TAD VD;  
3871 4137 M;  
3872 4172 CALL;  
3873 3144 MOH;  
3874 4156 S;  
3875 1255 TAD WDEV;  
3876 4142 R;  
3877 5575 RETURN
```

ENT

/used by DATCAL to enter $10,000_{10}$ and float it

◆3765

```
3765 0020 THA, 20;  
3766 0047 THB, 47  
3767 1325 ENT, TAD THA; /write 00208  
3770 6441 EM1;  
3771 7200 CLR;  
3772 1326 TAD THB; /write 00478  
3773 6441 EM1;  
3774 4200 R; /float it  
3775 5575 RETURN
```

```
R=JMS FLT  
FLT=164  
EM1=6441  
MOH=3144  
M=4137  
S=4156  
DINE=2723  
M=4150  
R=4142
```

• 231

CALL=4172
RETURN=5575
CHI=3781
KYCTR=80
K1=34
TEM=10
TEMP=220
CTR=20
CTR1=22
MINUS=31
DCA=6452
WCPAB=6455
WCPAB=6445
EM1=6441
TEM1=26
REG6=343
CONV=6014
KEYCTR=27
SUMT=76
P=4142:

RON=5440

			◆3000
3000	0005	FIVE,	5
3001	0012	TEM,	12
3002	7775	TM,	-3
3003	0008	SIX,	6
3004	0343	RS,	REG6
3005	0034	K,	K1
3006	0217	TEMP,	TEMP-1
3007	4172	BEGIN,	CALL
3010	5440		RON
3011	7200		CLA
3012	3080		DCA KYCTR
3013	1605		TAD I K
3014	7040		CMA
3015	7440		SCA
3016	7040		CMA
3017	4172		CALL
3020	3124		LDC
3021	2080	SUM1,	ISZ KYCTR
3022	1080		TAD KYCTR
3023	1205		TAD K
3024	3026		DCA TEM1
3025	1426		TAD I TEM1
3026	7040		CMA
3027	7650		SMA CLA
3030	5247		JMP JUMP
3031	1201	TAD TEM	
3032	4172	CALL	
3033	3124	LDC	
3034	4172		CALL
3035	3140		MULL
3036	1426	TAD I TEM1	
3037	4172		CALL
3040	3124		LDC
3041	4172		CALL
3042	3134		ADDI

```

3043 1080      TAD KEYCTR
3044 1202      TAD TM
3045 7840      SZA CLA
3046 5221      JMP SUM1
3047 4184      JMS F
3050 1205      TAD K
3051 1203      TAD SIX
3052 3026      DCA TEM1
3053 1426      TAD I TEM1
3054 4172      CALL
3055 3124      LDS
3056 4184      JMS F
3057 1206      TAD TEN2
3060 4137      JMS MT
3061 4161      JMS D
3062 1200      TAD FIVE
3063 1205      TAD K
3064 3026      DCA TEM1
3065 1426      TAD I TEM1
3066 4172      CALL
3067 3124      LDS
3070 4154      JMS F
3071 4153      JMS A
3072 1206      TAD TEN2
3073 4137      JMS MT
3074 4161      JMS D
3075 4153      JMS A
3076 7100      CLL
3077 1031      TAD MINUS
3100 7010      RAR
3101 7620      SNL CLA
3102 5305      JMP SUM3
3103 4172      CALL
3104 3781      CH3
3105 1204      SUM3, TAD R6;
3106 4142      R;
3107 1037      TAD KEYCTR
3110 7450      INR;
3111 5575      RETURN
3112 3076      DCA SUMT;
3113 1204      TAD R6;
3114 4172      CALL;
3115 6014      CONV;
3116 1204      TAD R6;
3117 4137      JMS MT
3120 1076      TAD SUMT;
3121 3027      DCA KEYCTR;
3122 5575      RETURN

```

APU OPERATORS

```

♦3124
3124 6441 LDI, B01 /take a number in the AC and load it into
3125 7300 CLR APU as a single fixed #
3126 6441 B01
3127 5575 RETURN
3130 0071 NOHD, 71
3131 0156 DMUL, 156
3132 0154 DADD, 154
3133 2734 B0X, B0
3134 4172 ADDS, CALL /add TOS and NOS as single fixed
3135 2727 CRAB
3136 1332 TAD DADD /get ADDS code
3137 5733 JMP I B0X /go do the command and return
3140 4172 MULI, CALL /multiply TOS and NOS as single fixed
3141 2727 CRAB
3142 1331 TAD DMUL
3143 5733 JMP I B0X
3144 4172 NOH, CALL /exchange TOS and NOS as double #'s
3145 2727 CRAB
3146 1330 TAD NOHD
3147 5733 JMP I B0X

```

/LOA,B /Lights off A&B

```

♦3151 Turns off LED's & other bits in the latch, except
3151 0003 L1, 3; LOA - .
3152 8000 L3, 8000; LOB - all but -, . and error lites
3153 0023 L4, 23
3154 7380 LOB, CLR ITL; /tell CHLITE to turn off L4's
3155 7421 MOL;
3156 1351 TAD L1; /turn off all but minus & decimal point
3157 4172 CALL;
3160 2516 CHLITE; /comes back with CLL
3161 7421 MOL; /turn off all of L3
3162 4172 CALL;
3163 2516 CHLITE
3164 7380 LOB, CLR ITL; /set up to turn off L4's
3165 7421 MOL;
3166 1353 TAD L4; /turn off all but LO BATT & - & .
3167 4172 CALL;
3170 2516 CHLITE;
3171 7421 MOL; /turn off L3's
3172 1352 TAD L3; /except for HI TEMP & DATA ERROR
3173 4172 CALL;
3174 2516 CHLITE;
3175 5575 RETURN

```

CHLITE=2516

BR1=6440

◆2600

APU DRIVER ROUTINES

F=164; /Arithmetic Processor Unit

D=151;
A=153;
S=156;
P=145;
M=150;
WT=137;
RD=142

FLT, DIVF, ADDF, SUBF, PUSH & MULF can be executed with a single instruction like JMS D; where D is the RAM location for a subroutine calling program loaded by INIT

All the rest require, e.g., CALL; POP

Result always in TOS if a function

2600	0400	CRA,	400	
2601	0003	COB,	3	
2602	0035	<u>FLTE,</u>	35	
2603	0023	FDI,	23	
2604	0020	FAD,	20	
2605	0007	ATAN,	7	
2606	0070	POPD,	70	
2607	0056	DMUL,	56	
2610	0005	ASIN,	5	
2611	0021	FCU,	21	
2612	0027	FTOD,	27	
2613	0022	FMUL,	22	
2614	0027	FINF,	27	
2615	0057	BDIV,	57	
2616	0055	BDUB,	55	
2617	4172	<u>FLT,</u>		CALL /set up APU for command
2620	2727			CRAB
2621	1202			TAD FLTE /get FLOAT code (floats a single fixed #)
2622	4172			CALL/go do the command
2623	2734			EW
2624	5564			JMP I F/exit through address stored in Page 0
2625	4172	<u>DIVF,</u>		CALL/divide NOS by TOS in float
2626	2727			CRAB
2627	1203			TAD FDI
2630	4172			CALL
2631	2734			EW
2632	5521			JMP I D
2633	4172	<u>ADDF,</u>		CALL/add TOS & NOS in float
2634	2727			CRAB
2635	1204			TAD FAD
2636	4172			CALL
2637	2734			EW
2640	5553			JMP I A
2641	4172	<u>SUBF,</u>		CALL/subtract TOS from NOS in float
2642	2727			CRAB
2643	1211			TAD FCU
2644	4172			CALL
2645	2734			EW
2646	5556			JMP I S
2647	4172	<u>PUSH,</u>		CALL/pushes TOS to NOS in float. Last variable is lost.
2650	2727			CRAB
2651	1212			TAD FTOD
2652	4172			CALL
2653	2734			EW
2654	5546			JMP I P

APU DRIVER ROUTINES, Page 2

2655	4172	<u>ATAN,</u>	CALL /set up APU for commands
2656	2727		CRAB
2657	1205		TAD ATAN/get code for Arc tangent
2660	5334		JMP BW/exit thru BW
2661	4172	<u>PCP,</u>	CALL/pop NOS to TOS in double precision
2662	2727		CRAB
2663	1206		TAD PCPD
2664	5334		JMP BW
2665	4172	<u>MULF,</u>	CALL/multiply TOSxNOS in float
2666	2727		CRAB
2667	1213		TAD FMUL
2670	4172		CALL
2671	2734		BW
2672	5550		JMP I M
2673	4172	<u>MULD,</u>	CALL /multiply TOSxNOS in double prec. integer
2674	2727		CRAB
2675	1207		TAD DMUL
2676	5334		JMP BW
2677	4172	<u>ASIN,</u>	CALL/do Arc sin in float
2700	2727		CRAB
2701	1210		TAD ASIN
2702	5334		JMP BW
2703	4172	<u>SORT,</u>	CALL/do SORT of TOS
2704	2727		CRAB
2705	7001		IAC/code for SORT
2706	5334		JMP BW
2707	4172	<u>FIX,</u>	CALL/FIX the TOS from foalt to single precision
2710	2727		CRAB
2711	1214		TAD FIXE
2712	5334		JMP BW
2713	4172	<u>DIVD,</u>	CALL/divide NOS by TOS in double prec. integer
2714	2727		CRAB
2715	1215		TAD DDIV
2716	5334		JMP BW
2717	4172	<u>DUED,</u>	CALL/subtract TOS from NOS in double prec. integer
2720	2727		CRAB
2721	1216		TAD DDUED
2722	5334		JMP BW
2723	4172	<u>SINE,</u>	CALL/do SINE of TOS
2724	2727		CRAB
2725	7305		CLA CLL IAC FAL
2726	5334		JMP BW

APU DRIVER ROUTINES, Page 3

2727	7200	<u>CRAE</u> ,	CLA /set up APU for command	
2730	1200		TAD CRA/get code for FLAG1 on, all else off	
2731	6445		WCRAE/write CRA of PIE B	
2732	7200		CLA	
2733	5575		RETURN	
2734	6441	<u>EW</u> ,	EW1/do the command	
2735	6452		IMP3/(or B53) wait for APU to do it	
2736	5335		JMP .-1	
2737	7200		CLA	
2740	6445		WCRAE/reset PIE B for APU "DATA"	
2741	5575		RETURN	
2742	3010	<u>WTAPUF</u> ,	DCA TEM /call WTAPUF by doing JMS 0137, AC=(floating # to be	1st byte of
2743	6445		WCRAE/set up APU for "DATA"	written into APU
2744	1376		TAD FM/count 4 things	
2745	3022		DCA CTR1	arranged:
2746	1410	<u>W1</u> ,	TAD I TEM/get 1st (or next) of 4 bytes (1 LSB; 2--; 3--;)	4 MSB
2747	6441		EW1	
2750	7200		CLA	
2751	2022		ISZ CTR1/done 4 bytes?	each byte:
2752	5345		JMP W1/no	000/00xx/xxx/xxx
2753	5537		JMP I WT/yes; exit via zero page	b ₀ b ₁₁
2754	7001	<u>RDAPUF</u> ,	IAC/call RDAPUF:JMS0142	
2755	3022		DCA TEM1/enter with AC=(1st byte of destination for TOS)-1	
2756	6445		WCRAE/set up "DATA" for APU	
2757	1376		TAD FM/count 4 things	
2760	3022		DCA CTR1	
2761	1022		TAD TEM1	
2762	1201		TAD CCR/add 3 to address, since data comes off MSB 1st from I	
2763	3022		DCA TEM1/store back in TEM1	
2764	6440	<u>R1</u> ,	BR1/1st BR1 gets up APU fo read, but puts garbage in AC	
2765	7200		CLA	
2766	6440		BR1/2nd BR1 actually reads it	
2767	3422		DCA I TEM1/store in destination	
2770	1022		TAD TEM1/decrement address pointer	
2771	1377		TAD QNM	
2772	3022		DCA TEM1/replace	
2773	2022		ISZ CTR1/4 times?	
2774	5364		JMP R1/no	
2775	5542		JMP I RD/yes, exit thru RAM	
2776	7774	<u>FM</u> ,	-4	
2777	7777	<u>QNM</u> ,	-1	

BLANK AND DISPR

```

                                MCARR=6425
                                LON1=4622
                                AM2=6431
                                CALL=4172
                                RETURN=5575
                                ◆20
0020 0000 CTR, 0
0021 0000 L4R, 0
0022 0000 CTR1, 0
0023 0000 AC, 0
0024 0000 DISPR1, 0
0025 0000 DISPR2, 0
0026 0000 TEM1, 0
0027 0000 KEYCTR, 0
                                ◆3600
3600 1400 L4, 1400
3601 0400 L2, 0400
3602 0000 L1, 0000
3603 7774 DP, 7774
3604 7773 DP1, -5
3605 7772 DP2, -6
3606 7200 BLANK, CLA
3607 3027 DCA KEYCTR
3610 7040 CMA
3611 3024 DCA DISPR1
3612 7040 CMA
3613 3025 DCA DISPR2
3614 4172 CALL
3615 3672 DIS3
3616 7000 NOP
3617 7200 CLA
3620 1200 TAD L4
3621 6425 MCARR
3622 7300 CLA CLL
3623 1021 TAD L4R
3624 0203 AND DP
3625 6431 AM2
3626 3021 DCA L4R
3627 5575 RETURN
3630 3023 DISPR, DCA AC
3631 7004 RAL
3632 3026 DCA TEM1
3633 1027 TAD KEYCTR
3634 1204 TAD DP1
3635 7650 CMA CLA
3636 5310 JMP KEYS
3637 1027 TAD KEYCTR
3640 1205 TAD DP2
3641 7650 CMA CLA
3642 5317 JMP KEYS
3643 1025 DISPR, TAD DISPR2
3644 7421 MOL
3645 1203 TAD DP
3646 3022 DCA CTR1
3647 1024 TAD DISPR1

```

BLANK AND DISPR, Page 2

3650	7104	DIS2,	OLL RAL
3651	7521		SWP
3652	7004		RAL
3653	7521		SWP
3654	3022		ISZ CTR1
3655	5250		JMP DIS2
3656	1023		TAD AC
3657	3024		DCA DISPR1
3660	7521		SWP
3661	3025		DCA DISPR2
3662	1023		TAD TEM1
3663	7650		SNA CLA
3664	5272		JMP DIS3
3665	7305		CLA OLL IAC RAL
3666	4172	CALL	
3667	4222	LOM1	
3670	3026	DCA TEM1	
3671	5242		JMP DIS1
3672	1201	DIS3,	TAD L2
3673	6425		MCRAA
3674	7200		CLA
3675	1025		TAD DISPR2
3676	6431		RW2
3677	7200		CLA
3700	1202		TAD L1
3701	6425		MCRAA
3702	7200		CLA
3703	1024		TAD DISPR1
3704	6431		RW2
3705	7300		CLA OLL
3706	1023		TAD AC
3707	5575		RETURN
3710	7100	KEYS,	OLL
3711	1023		TAD AC
3712	7006		RTL
3713	7006		RTL
3714	1024	DIS4,	TAD DISPR1
3715	3024		DCA DISPR1
3716	5272		JMP DIS3
3717	1023	KEYS,	TAD AC
3720	5314		JMP DIS4

◆3757

CHS

CRAB=2727 CHange Sign

3757	2734	EM1,	2734	FROM ADR OF EM
3760	0025	CHIF,	35	
3761	4172	CHC,	CALL	
3762	2727		CRAB	
3763	1350		TAD CHIF	
3764	5757		JMP I EM1	

ANGLE SYMBOL TABLE

A	4153
ANG	5355
ANGA	2214
ANGE	2233
ANGF	2251
ANI	2230
CALL	4172
CHS	3751
D	4161
KEYCTR	0027
P	4145
PF	2278
PI	2144
POF	2257
PODF	5474
POP	2261
RETURN	5575
S	4156
STATUS	4347
TEMS	0051
W	4137

```
PC00241 MD5214 R0000 L1 D0
>>2002 7002
>>
```

ANGLE, ANGE

/ANGA takes an angle in radians, converts to 0-2π radians, then gets ANG to display it in degrees

```
CALL=4172;
RETURN=5575; /ANGE-see next page
W=4137;
P=4145;
STATUS=4347;
PI=2144;
A=4153;
ANG=5355;
D=4161;
I=4156;
CHS=3751;
TEMS=51;
POP=2261;
PODF=5474;
KEYCTR=27
```

◆2214

```
2214 4137 ANGA, W;/write the value
2215 4145 P;/save
2216 4172 CALL;/+ or -?
2217 4347 STATUS;
2220 7550 INF CLR;/1 if minus; 0 if plus
2221 5230 INF ANI;
2222 4172 CALL;/-, add 2π then display it
2223 2144 PI;
2224 4172 CALL;
2225 2144 PI;
2226 4153 A;
2227 4153 A
2230 4172 ANI, CALL;/+, its OK - display it
2231 5355 ANG+1;
2232 5575 RETURN
```

/ANGE adjusts a number input by the keyboard so it is in
 $-\pi < a < \pi$ form in TOS

```

2233 4161 ANGE, D: / ÷ iso/π
2234 4145 P: /save it
2235 4172 CALL: /see which hemisphere it's in by subtracting PI & checking sign
2236 6144 PI:
2237 4156 S:
2240 4172 CALL:
2241 4347 STATUS:
2242 7640 BSR CLA: /0 if pos, 1 if neg
2243 5251 JMP ANGP/OK do it
2244 4172 CALL: /needs to have π subtracted so answer is  $-\pi < x < \pi$ 
2245 6144 PI:
2246 4156 S:
2247 3051 DCR TEM8: /clear TEM8, which indicates 'ANGLE'
2250 5575 RETURN
2251 4172 ANGP: CALL: /get answer on TOS
2252 2661 POP:
2253 3051 DCR TEM8: /clear TEM8
2254 5575 RETURN

```

POF

♦2257 POF/point 00five used by convert to avoid round
up/down error in CONN

```

2257 4137 POF, W: /write #
2260 4145 P: /save
2261 4172 CALL: /tor-?
2262 4347 STATUS:
2263 7421 MDL: /save answer in M0
2264 1276 TAD PF: /write .005
2265 4137 W:
2266 7501 MDR: /look at M0
2267 7650 BSR CLA: /1 if # neg, 0 if # was pos
2270 5273 JMP .+B: /pos, get add .005
2271 4172 CALL: /neg, subtr .005
2272 3761 CHD:
2273 4156 R:
2274 3027 DCR KEYCTR: /zeroize KEYCTR
2275 5575 RETURN
2276 5473 PF, P00F-1/address of floating .005

```

ACC

CALL=4178
 RETURN=5575
 LCM1=4688
 MCFPR=6485
 AVE=6431
 FREQ3=6433
 KYBLK=6554
 RF3=6430
 DIM=3007
 DICPR=3630
 BLANK=3606
 KEYCTR=27
 L4R=21
 AC=23

◆23

0030	0000	JMFR,	0
0031	0000	MINUS,	0
0032	0000	DONEF,	0
0033	0000	KEYT,	0
0034	0000	K1,	0
0035	0000	K2,	0
0036	0000	K3,	0
0037	0000	K4,	0
0040	0000	K5,	0
0041	0000	K6,	0
0042	0000	K7,	0

◆3300

3300	0005	FIV,	5
3301	7773	FIVE,	-5
3302	0034	K,	K1
3303	3540	A1,	ACCA
3304	7774	FOUR,	-4
3305	7771	SEVEN,	-7
3306	1400	L4,	1400
3307	1032	ACC4,	TAD DONEF
3310	7640		BCR CLR
3311	5703		JMP I A1
3312	1033		TAD AC
3313	7100		OLL
3314	4178		CALL
3315	3630		DICPR
3316	7200		CLR
3317	1027		TAD KEYCTR
3320	1302		TAD F
3321	3030		BCR JMFR
3322	1033		TAD AC
3323	3430		BCR I JMFR
3324	2027		ICD KEYCTR
3325	1027		TAD KEYCTR
3326	1304		TAD FOUR
3327	7650		JNA CLR
3330	5336		JMP ACC1
3331	1027		TAD KEYCTR
3332	1305		TAD SEVEN
3333	7640		BCR CLR
3334	5703		JMP I A1
3335	5331		JMP ACC2

3336	1306	ACC1,	TAD L4
3337	6425		MORAA
3340	7201		CLA IAC
3341	7040		DMA
3342	0021		AND L4R
3343	6431		AWB
3344	3021		DCA L4R
3345	7330		CLA CTL PAP
3346	3031		DCA MINUC
3347	7130		STL
3350	5357		JMP ACC5
3351	3032	ACC2,	ISC DONEF
3352	5703		JMP I A1
3353	1027	ACC3,	TAD KEYCTR
3354	1301		TAD FIVE
3355	7620		SNL CLA
3356	5703		JMP I A1
3357	4172	ACC5,	CALL
3360	3630		DISPR
3361	3032		DCA DONEF
3362	1300		TAD FIV
3363	3027		DCA KEYCTR
3364	5703		JMP I A1
			◆3400
3400	7773	FIVM,	-5
3401	3501	KB,	KEYB
3402	0017	ACCMF,	17
3403	3353	A,	ACC3
3404	3307	A4,	ACC4
3405	1400	L4R,	1400
3406	5356	KY0,	JMP ACC0
3407	1211	KY1,	TAD KY1+2
3410	5356		JMP ACC0
3411	0001		1
3412	1214	KY2,	TAD KY2+2
3413	5356		JMP ACC0
3414	0002		2
3415	1217	KY3,	TAD KY3+2
3416	5356		JMP ACC0
3417	0003		3
3420	1222	KY4,	TAD KY4+2
3421	5356		JMP ACC0
3422	0004		4
3423	1225	KY5,	TAD KY5+2
3424	5356		JMP ACC0
3425	0005		5
3426	1230	KY6,	TAD KY6+2
3427	5356		JMP ACC0
3430	0006		6
3431	1233	KY7,	TAD KY7+2
3432	5356		JMP ACC0
3433	0007		7
3434	1236	KY8,	TAD KY8+2
3435	5356		JMP ACC0
3436	0010		10
3437	1241	KY9,	TAD KY9+2
3440	5356		JMP ACC0
3441	0011		11

3442	7120	KYP*	STL
3443	5356		JMP ACC0
3444	1031	KYM*	TAD MINUS
3445	7710		SFA CLA
3446	5340		JMP ACCA
3447	2031		ISZ MINUS
3450	1205		TAD L4R
3451	6425		MCARR
3452	7200		CLA
3453	1031		TAD MINUS
3454	7012		RTR
3455	7700		SMA CLA
3456	5263		JMP KYM1
3457	7001		IAC
3460	4172		CALL
3461	4622		LOH1
3462	5340		JMP ACCA
3463	7201	KYM1*	CLA IAC
3464	7040		CMA
3465	0021		AND L4R
3466	6431		AME
3467	3021		DCA L4R
3470	5340		JMP ACCA
3471	4172	KYC*	CALL
3472	3606		BLANK
3473	5323		JMP ACC6
3474	4172	KYE*	CALL
3475	3007		SUM
3476	5575		RETURN
3477	5340	KYD*	JMP ACCA
3500	5340	KY3*	JMP ACCA
3501	5242	KEYB*	JMP KYP
3502	5234		JMP KY8
3503	5220		JMP KY4
3504	5271		JMP KYC
3505	5244		JMP KYM
3506	5223		JMP KY5
3507	5207		JMP KY1
3510	5277		JMP KYD
3511	5237		JMP KY6
3512	5226		JMP KY6
3513	5212		JMP KY2
3514	5274		JMP KYE
3515	5202		JMP KY0
3516	5231		JMP KY7
3517	5215		JMP KY3
3520	5300		JMP KY5

```

3521 6433 ACC,  KFEQ2
3522 7300      CLR CLL
3523 3031 ACCB,  DCA MINUC
3524 3027      DCA KEYCTF
3525 3032      DCA DCHRF
3526 3041      DCA K6
3527 3042      DCA K7
3530 7040      CMA
3531 3034      DCA K1
3532 7040      CMA
3533 3035      DCA K2
3534 7040      CMA
3535 3036      DCA K3
3536 7040      CMA
3537 3037      DCA K4
3540 6433 ACCA,  KFEQ2
3541 5240      JMP .-1
3542 7000      NOP
3543 7000      NOP
3544 7000      NOP
3545 7000      NOP
3546 7000      NOP
3547 7000      NOP
3550 7100 OUT,  CLL
3551 6430      ARE
3552 0202      AND ACCMK
3553 1201      TAD K6
3554 3030      DCA JMFR
3555 5762      JMP I KKK /go write ou what KYBLK is
3556 3023 ACCC,  DCA AC
3557 7630      CLL CLA
3560 5603      JMP I A
3561 5604      JMP I A4
3562 6554 KKK,  KYBLK

```

LSW /Least Significant Word
 ♦3365 takes LWS of a floating # & displays it

```

3365 0017 MDR, 17:
3366 0224 RG1, REG1:
3367 0223 RG1M, REG1-1
3370 1367 LSW, TAD RG1M:/get TOS into scratchpad
3371 4142 JMS PD:
3372 1766 TAD 1 RG1:/get LSW
3373 0265 AND MDR:/mask off least significant 4 bits
3374 4172 CALL:/display them as a decimal #, using DISPR. DISPR pushes the
3375 3930 BIFF:/displayed #'s to the left to make room for the new one.
3376 7200 CLR:
3377 5675 RETLH

```

```

STATUS=4347:
REG1=224:
PD=142

```


CONGE /from CON time Or Enter

```
♦5700
TEM10=54: /holds program and flashes the lights to let operator hand
KPB=6430:
ARB=6430: /any errors: pressing DISP shown the last message code
TEND=75: displayed (if "2", no errors), pressing CON will not accep
DISCO=3234: the current parameters. ENT does accept them. Must
BLANK=3606: enter with TEMN=0, exits with TEMN=1 if CLR/CONT presse
LOR=3154: 0 if ENT pressed
CHAR1=63
CALL=4172:
RETURN=5575:
TEMN=101:
LON1=4622
5700 7775 CNT, -3:
5701 7771 DCF, -7:
5702 0017 MK, 17:
5703 7765 ENT, -13
5704 1343 CONGE, TAD FLSH:/flash all the lights
5705 4172 CALL:
5706 4622 LON1
5707 6430 CN1, KPB:/wait for a KBR
5710 5307 JMP, -1:
5711 6430 ARB:/read & mask it
5712 0302 AND MK:
5713 3063 DCA CHAR1:/and store in CHAR1
5714 1063 TAD CHAR1:
5715 1300 TAD CNT:/is it CLR/CONT?
5716 7640 DCA CLR
5717 5336 JMP CN2:/no, try again
5720 2101 ISZ TEMN:/yes, indicate such in TEMN
5721 4172 O, CALL:/blank display
5722 3606 BLANK:
5723 4172 CALL:/turn off lights
5724 3154 LOR:
5725 5575 RETURN
5726 1063 CN2, TAD CHAR1:
5727 1301 TAD DCF:/is it DISP?
5730 7640 DCA CLR:
5731 5336 JMP CN3:/no, try again
5732 1075 TAD TEND:/fetch the last displayed message
5733 4172 CALL:/and display it
5734 3234 DISCO:
5735 5307 JMP CN1/wait for another keystroke
5736 1063 CN3, TAD CHAR1:
5737 1302 TAD ENT:/is it ENTER?
5740 7640 DCA CLR:
5741 5307 JMP CN1:/no, illegal entry. Ignore & start over
5742 5331 JMP O/yes, exit with TEMN=0
5743 0010 FLSH, 10
```

DIPCAL /calculates DIP angle

```

PIA3=3305;
PBU5=43;
KEYT=33;
DRTCAL=4250;
ARTAN=2655;
REG4=527;
ANG=5255;
DORT=2703;
STATUS=4347;
M=4137;
R=4142;
P=4145;
N=4150;
A=4153;
D=4161;
YCOS=243;
XCOS=253;
ZCOS=247;
♦5745
5745 0243 Y, YCOS;
5746 0253 X, XCOS;
5747 0247 Z, ZCOS;
5750 0527 R4, REG4
5751 1345 DIPCAL, TAB Y;/write Y cos
5752 4137 M;
5753 4145 P;
5754 4150 M;/YCOS2
5755 1347 TAB ZC
5756 4137 M;
5757 4145 P;
5760 4150 M;/ZCOS2
5761 4153 A;/YCOS2+ZCOS2
5762 4172 CALL;  $\sqrt{YCOS^2+ZCOS^2}$ 
5763 2703 DORT;/ $\sqrt{YCOS^2+ZCOS^2}$ 
5764 1346 TAB X;
5765 4137 M;
5766 4161 D;/XCOS/ $\sqrt{YCOS^2+ZCOS^2}$ 
5767 4172 CALL;
5770 2655 ARTAN /tan-1(XCOS/ $\sqrt{YCOS^2+ZCOS^2}$ )=dip angle
5771 1350 TAB R4;/put in REG4
5772 4142 P;
5773 1350 TAB R4;/display REG4 as a -180<x<180 angle
5774 4172 CALL;
5775 5255 ANG;
5776 5275 RETURN

```

```

GTIN /sequences thru initial conditions necessary
CALL=4172:
RETURN=5575:
M=4710:
L=4732:
LOR=3154:
E=4664
GETIN=4463:
MAIN2=6620:
SLEN=4703
♦5400
5400 4172 GTIN, CALL;/lights off
5401 3154 LOR:
5402 4172 CALL;/go to BRTAB to handle INITIAL BER input
5403 4732 L:
5404 4172 CALL;/lights off
5405 3154 LOR:
5406 4172 CALL;/go to BRTAB to handle INITIAL INC input
5407 4710 M
5410 4172 CALL;/lights off
5411 3154 LOR:
5412 4172 CALL;/go to BRTAB to handle INITIAL ROD input
5413 4664 E:
5414 4172 GTIN1, CALL;/lights off
5415 3154 LOR:
5416 4172 CALL;/go to BRTAB to handle INITIAL SLEW input
5417 4703 SLEN:
5420 5266 JMP EXTEN;/match to EXTEN (5466)
5421 6620 MAIN2 /unnecessary

```

```

MEEK /MAIN2 EXTENDED
EXEC=5011:
PROC2=4032:
M4=6640:
MAIN2=6620:
TEM13=57:
TEM11=55
5422 7040 MEEK, CMA;/disallow continue
5423 3057 DCR TEM13:
5424 4172 CALL;/wait for new data or "AR","ENTER"
5425 5011 EXEC:
5426 1055 TAD TEM11/what was it?
5427 7700 CMA CLA:
5430 5637 JMP I M4;/new data, go back to M4
5431 4172 CALL;/AR ENTER
5432 5446 RDN:
5433 4172 CALL;/get the PROC2 values
5434 4032 PROC2
5435 5636 JMP I M2/go back to MAIN2
5436 6620 M2, MAIN2:
5437 6640 M4, M4

```

DATCAL

DISB=3976;
DISPR2=25;
BLAMP=1606;
DISPR=3627;
SUBD=2717;
FIN=2707
MULD=3673;
MINUS=31;
DIVD=2713;
REG1=224;
CALL=4172;
RETURN=5575
TEM3=11;
TEM4=12;
TEM=10;
TEM1=26;
EM1=8441;
MT=137;
SD=142;
SUEF=156;
LCN=4620
PUSH=145;
ADDF=153;
MULF=150;
CHS=3761;
FLT=164;
CRAB=2727;
RR1=8440;
CHLITE=2516
POF=2661;
STACK=175;
DIME=161;
SQRT=2703;
CTR=20;
CTR1=22;
KCH=3144;
LDC=3124
ADD3=2134;
MUL3=3140;
CTR2=42;
REG2=230;
EM=2734;
KEYCTR=27;
NOFM=2341
CCDATA=2305;
CHER=2532;
ENT=3787;
REAR=2520;
TEMS=2526;
FAULT=2452

◆4200

4200	0277	REF.	277		NEEDS WORK
4201	0174	AV1.	174	/YCOS	
4202	0010		10		DATCAL DOES:
4203	0320	AM1.	320		$\frac{(\text{Data Word}) \times 10000 - AV}{AV} \rightarrow \text{data}$
4204	0330		330		
4205	0071	AV2.	71	/ZCOS	
4206	0377		377		
4207	0331	AM2.	331		
4210	0046		46		
4211	0210	AV3.	210	/XCOS	
4212	0002		2		
4213	0327	AM3.	327		CHANGED THE VALUES
4214	0046		46		
4215	0043	AV4.	43	/GGX (CHANGE SIGN)	
4216	0000		0		
4217	0014	AM4.	14		
4220	0333		333		
4221	0043	AV5.	43	/GGZ	
4222	0000		00		
4223	0020	AM5.	20		
4224	0047		47		
4225	0042	AV6.	42	/GGY (CHANGE SIGN)	
4226	0000		0		
4227	0047	AM6.	47		
4230	0331		331		
4231	7772	SM.	-6		
4232	4200	AV.	AV1-1		
4233	0243	DATL.	243		
4234	7774	FM.	-4		
4235	0273	TEMP.	273/downhole temperature		
4236	0004	TEML.	4 /temperature limit, high end		
4237	0040	MAX.	40		
4240	4237	TFFR.	TFFR-1 /2.47 /reference voltage check		
4241	6424		6424		
4242	6636		6636		
4243	6402		6402		
4244	4243	TFR.	TFR-1 / .05		
4245	6714		6714		
4246	6714		6714		
4247	6574		6574		
4250	4172	DATCAL.	CALL /scale the data		
4251	6305		SCIDATA		
4252	1240		TAD TFFR/check reference voltage		
4253	4137		JMS MT		
4254	1200		TAD REF		
4255	4137		JMS MT		
4256	4156		JMS EUEF/APUTOS has 2.47-REF		
4257	4172		CALL		
4260	4247		STATUS		
4261	7650		ORA CLA/negative?		
4262	5265		JMP .+3/no, skip ahead to 4265		
4263	4172		CALL/yes, falut		
4264	5452		FAULT		
4265	1244		TAD TFR/subtract .05 from the remainder		
4266	4137		JMS MT		
4267	4156		JMS EUEF		
4270	4172		CALL		

```

4271 4347          STATUS
4272 7640          SZA CLA/positive?
4273 5276          JMP .+3/no, OK
4274 4172          CALL/yes, 247-rd-.05 was >0
4275 5452          FAULT/fault displays "9" & waits for a go-ahead from KBR
4276 1235          TAD TEMP/check for interrupt, load APU with temp. word
4277 4137          JMS MT
4300 1235          TAD TEMP/load temperature limit (4.0 is 40°C)
4301 4172          CALL
4302 3124          LDS
4303 4164          JMS FLT /should be a JMS SUBF here
4304 4172          CALL<7>/check if negative: 0 is x>0, 1 is x<0
4305 4347          STATUS
4306 7650          SZA CLA<—should be SZA CLA
4307 5312          JMP DATE
4310 4172          CALL/temperature error—TEMP sets HI TEMP light & puts 77778
4311 6526          TEMP/into TEMP and 00018 into TEMP(0100)
4312 1343          DATE, TAD BATH/get addr of neg batt voltage
4313 4137          JMS MT/write it
4314 4172          CALL/change sign
4315 3761          CHE
4316 1240          TAD TFFA/write 2.5
4317 4137          JMS MT
4320 4156          JMS SUBF/get BATN-2.5V
4321 4172          CALL/CHEK sets Lo Bat light & puts 1 into TEMP(0100) if error
4322 6536          CHEK
4323 1344          TAD BATA/write positive battery voltage
4324 4137          JMS MT
4325 1240          TAD TFFA/write 2.5V
4326 4137          JMS MT
4327 4156          JMS SUBF/get Bat p-2.5
4330 4172          CALL/CHEK sets Lo Bat light & puts 1 into TEMP(0100) if error
4331 6536          CHEK
4332 4172          CALL/check receiver battery; if OK, return; if not OK
4333 6520          BATA/set LO BATT lite & put 1 into TEMP(0100)
4334 1231          TAD EM/load CTR2 to count 6
4335 3042          DCA CTR2
4336 1232          TAD AV/set TEMP3 to point to data coefficients AV1-> AM6
4337 3011          DCA TEMP3
4340 1232          TAD BATL/set AC to point to 1st data word
4341 5742          JMP I .+1
4342 4401          DAT1/end of DATCAL is located at 4401
4343 0203          BATH, 303
4344 0307          BATA, 307
4345 7775          TM, -3

```

STATUS /checks APU TOS & exits: AC=0 if positive
AC=1 if negative

```

*4346
4346 0100          BAH, 100
4347 4172          STATUS, CALL/get status word from APU
4350 2727          CRAB
4351 6440          BR1
4352 7200          CLA
4353 6440          BR1
4354 0346          AND MAB/mask sign info 0=positive
4355 5575          RETURN 1=negative

```

COM

/COMPARE - works out data limits & determines if out of limit

```

C=4156:
M=4137:
TEMP=53
4356 4137 COM, M:/write 2nd parameter
4357 4156 C:/param 1 - param 2
4360 4172 CALL:/get absolute value
4361 4347 STATUS:
4362 7650 JMA CLA:
4363 5575 RETURN:/done - its positive
4364 4172 CALL:/change sign - its negative
4365 3751 CHS:
4366 5575 RETURN/done

```

COM1

```

4367 4137 COM1, M:/subtract limit from parameter difference
4370 4156 C:
4371 4172 CALL:
4372 4347 STATUS:
4373 7640 JCA CLA:/error? (result of line 4370 will be neg if limit was bigger
4374 5575 RETURN:/no than difference, i.e., OK)
4375 2053 JSC TEMP:/yes, signal TEMP
4376 5575 RETURN

```

/DAT1

*4400 /DATCAL EXTENDED - does $\frac{(\text{data word}) \times 10000 - AV}{AM}$

```

4400 7774 TMD, -4
4401 3010 DAT1, DCA TEM/put start of data into TEM
4402 1010 DATX, TAD TEM
4403 4137 JMC MT/write data word
4404 4172 CALL/enter 10,000
4405 3757 ENT
4406 4150 JMC MULF/multiply
4407 4172 CALL/load & float 1st (next) coefficient (AV)
4410 4426 DDOF
4411 4156 JMC DDEF/subtract
4412 4172 CALL/load & float 2nd (next) coefficient (AM)
4413 4426 DDOF
4414 4151 JMC DIVF/divide
4415 1010 TAD TEM /point back to
4416 1200 TAD TMD /beginning of this word
4417 4142 JMC R/replace if with adjusted value
4420 2042 JSC CTFE/done it 6 times?
4421 5202 JMP DATX/no, do it again
4422 1235 TAD DTL/yes, make AC point to beginning of data
4423 4172 CALL/normalize the data
4424 6570 NPMCAL
4425 5575 RETURN

```

DDOF

```

4426 1411 TAD I TEMP /loads & floats # pointed to by TEMP
4427 6441 BM1
4430 7200 CLA
4431 1411 TAD I TEMP
4432 6441 BM1
4433 4164 JMC FLT
4434 5575 RETURN
4435 0243 DTL, 243
NPMCAL=6570

```

RESTART

/sequence thru what values are necessary to put computer at an old position in the borehole; will fill in value for BER1; INCL; SLEW; LAT; DEP & Vertical Depth

```

CALL=4172;
RETURN=5575;
L=4732;
M=4710;
H=4703;
B=4645;
F=4725;
G=4676;
CTR4=73;
TEMS=45;
LDR=3154;
LOH=4620;
LOH1=4622;
TEMS=51;
D=4657
♦S125
5125 1000 FLT, 1000;
5126 0507 ENG, 507;/BER2 (not used)
5127 0513 INCL, 513;/INC2 (not used)
5130 0403 CLE, 403;
5131 0413 LAT1, 413;
5132 0423 DPT, 423;
5133 0433 VDD, 433;
5134 4732 LR, L;/BER1
5135 4710 IR, M;/INCL
5136 4703 HR, H;/SLEW
5137 4645 BR, B;/LAT
5140 4725 FR, R;/DEP
5141 4676 GR, G;/VD
5142 5133 LRA, LR-1
5143 5161 ROM, RET1;
5144 4172 CALL;
5145 5464 JMP I 54;
5146 7771 IM, -7
5147 1346 RET, TAD EM/6 parameters (put LSZ CET4 in such a place that it
5150 3072 DCA CTR4; needs to count to 7)
5151 1342 TAD LRA;/start with BER address in BRTAB
5152 3011 DCA 11;/put in autoindex
5153 1343 TAD ROM;/set up call routine in RAM
5154 3054 DCA 54;
5155 1344 TAD ROM+1;
5156 3055 DCA 55;
5157 1345 TAD ROM+2;
5158 3057 DCA 57;
5161 4172 RET1, CALL;/lights off
5162 3154 LCA;
5163 1335 TAD FLT;/turn on "RS" light
5164 4172 CALL;
5165 4622 LOH1;
5166 7046 CMA PTL;
5167 7005 PTL;
5170 3045 DCA TEM5;/signal "INITIAL" to KYSR (TEM5>0) AC=7767 L=1 and INCL,BER1
5171 1411 TAD I 11;
5172 3056 DCA 56;
5173 2072 JIC CTR4;
5174 5055 JMP 55;
5175 4172 CALL;/all done/turn off lights
5176 3154 XXXXXX JMP I+1 (5776)
5177 5575 XXXXXX 6440

```


BRANCH TABLE

BRANCH TABLE

TEMP=50;
 CHLITE=5516;
 CALL=4172;
 RETURN=5575;
 TEM6=46;
 TEM8=51;
 TEM5=45;
 KYSR=5611
 KYSR0=5647;
 KYSR2=5631
 ◆4600

4600	5240	DIP, JMP A;/branch table	
4601	5245	LAT, JMP B;	
4602	5765	TEST, JMP I KR;/ignore, start over at KYSR (5611)	
4603	5766	INIT, JMP I KR;/initial into service with KYSR2 (5631)	
4604	5252	VIEW, JMP C;	
4605	5257	THD, JMP D	
4606	5765	READ, JMP I KR;/ignore, start over at KYSR (5611)	
4607	5264	ROD, JMP E;	
4610	5271	LIEW, JMP F;	
4611	5276	VD, JMP G;	
4612	5303	CLEN, JMP H;	
4613	5310	INC, JMP M	
4614	5320	ROT, JMP J;	
4615	5325	DEP, JMP K;	
4616	5765	RD, JMP I KR;/ignore	
4617	5332	BER, JMP L	
4620	7100	LON, CLL;	} call LON writes an L1 LED latch with contents of AC
4621	7410	SKP;	
4622	7120	LON1, STL;	} call LON1 writes an L2 LED latch with contents of AC
4623	7421	MCL;	
4624	7501	MOR;	
4625	4172	CALL;	
4626	2516	CHLITE;	
4627	5575	RETURN	
4630	3046	ANGL, DCA TEM6;/put value in TEM6	
4631	7040	CMA;/signal it's an angle by putting somethin in TEM8	
4632	3051	DCA TEM8;	
4633	5764	JMP I KC/back to KYSR to finish (5647)	
4634	3046	END, DCA TEM6;/put value in TEM6	
4635	3051	DCA TEM8;/clear TEM8	
4636	5764	JMP I KC/back to KYSR to finish (5647)	

```

♦4840
4840 7007 A. IAC RTL:/turn on DIP light
4841 4172 CALL:
4842 4820 LON:
4843 1348 TAD IP:/get addr of DIP
4844 5234 JMP ANGL/exit (angle)
4845 1342 B. TAD LTL:/turn on LAT light
4846 4172 CALL:
4847 4822 LON1:
4850 1347 TAD LT:/get addr of LAT
4851 5234 JMP END/exit
4852 1350 C. TAD VW:/turn on V DEVIATION
4853 4172 CALL:
4854 4820 LON:
4855 1351 TAD VDE:/get addr of VDEV
4856 5234 JMP END
4857 1345 D. TAD THDL:/turn on THD
4858 4172 CALL:
4859 4822 LON1:
4862 1352 TAD TH:/get addr of THD
4863 5234 JMP END/exit
4864 1374 E. TAD RDL:/turn on ROD
4865 4172 CALL:
4866 4820 LON:
4867 1354 TAD RD:/get addr of ROD
4870 5234 JMP END/exit
4871 1355 F. TAD LD:/turn on HOR DEVIATION
4872 4172 CALL:
4873 4820 LON:
4874 1356 TAD LV:/get contents of LDEV
4875 5234 JMP END/exit
4876 1344 G. TAD VDL:/turn on VD (vertical depth)
4877 4172 CALL:
4700 4822 LON1:
4701 1357 TAD WDF:/get contents of VD
4702 5234 JMP END/exit
4703 1360 H. TAD CL:/turn on string length
4704 4172 CALL:
4705 4820 LON:
4706 1361 TAD STR:/get contents of SLEW
4707 5234 JMP END/exit
4710 7105 M. CLL IAC RAL:/turn on INCLINATION
4711 4172 CALL:
4712 4820 LON:
4713 1045 TAD TEM5:/"INITIAL"
4714 7440 CLR/DO NOT CLA
4715 1362 TAD TM:/yes, subtract  $16_{10}$  (if "INITIAL" TEM5=-1) or  $24_{10}$  (if RESTART
4716 1362 TAD AVI:/no, just load, TEM5=9 DOES THIS) from AVI (addr of AVINC)
4717 5234 JMP ANGL/exit of AVINC AVI → AC(addr to make it addr AINC or INCI
4720 1367 J. TAD RT:/turn on ROTATION light
4721 4172 CALL:
4722 4820 LON:
4723 1370 TAD RPA:/get addr of ROT
4724 5234 JMP ANGL/exit (angle)
4725 1343 K. TAD DPL:/turn on DEPARTURE light
4726 4172 CALL:
4727 4822 LON1:
4730 1371 TAD DE:/get addr of DEP
4731 5234 JMP END/exit

```

4732	1372	L, TAD BR;/turn on BEARING light
4733	4172	CALL;
4734	4820	LON;
4735	1045	TAD TEMS/"INITIAL" pressed?
4736	7440	BEA;/do not CLA
4737	1362	TAD TM;/yes,subtr 16 ₁₀ (if "INITIAL" TEMS=-1) or 24 ₁₀ (if RESTART TEMS
4740	1373	TAD AVE;/no, just load addr of does this) from addr of AVBER & pu
4741	5230	JMP ANGL/exit, AVBER into AC in 4C (induce it A-BER) or BERL
4742	0040	(angle)
4742	0040	LTL, 40;
4743	0100	DPL, 100;
4744	0200	VDL, 200;
4745	0400	THDL, 400;
4746	0317	BP, 317;
4747	0413	LT, 413;
4750	0400	WV, 400;
4751	0453	WDE, 453;
4752	0443	TH, 443;
4753	0100	PD, 100;
4754	0367	PD, 367;
4755	0010	LD, 10;
4756	0463	LW, 463;
4757	0433	VDP, 433;
4760	0020	IL, 20;
4761	0403	STP, 403;
4762	7761	TM, -17;/-15 ₁₀
4763	0523	AVI, 523/AVINC
4764	5647	K1, KYCP1;
4765	5611	K2, KYCP2;
4766	5631	K3, KYCP3;
4767	0200	PT, 200;
4770	0333	STA, 333;
4771	0423	DE, 423;
4772	0040	BR, 40;
4773	0517	AVE, 517/AVBER
4774	0100	FIL, 100

INIT

INITIALIZATION

```
♦5510
  SETUP=7706;
  CH=125;
  LON=4620;
  LOA=3124;
  CALL=4172;
  RETURN=5575;
  BLANK=3206
  L4R=44;
  L3R=21;
  ADR=5440;
  RPUCF=6600
  W=4137;
  R=4142;
  F=4124;
  LDC=3124;
  STUP=71;
  INF=70;
  BR2=6450
5510 5253 CH, -3525;
5511 1000 MI, 1000;
5512 3522 TR, TRF-1;
5513 0347 MG, 347;
5514 5516 RDT, RIDT-1;
5515 0217 TEMP, 217;
5516 0373 RIT, 373;
5517 6732 RIDT, 6732:/π/2 float
5520 6417 6417;
5521 6711 6711;
5522 6401 6401;
5523 6400 TRF, 6400:/10 float
5524 6400 6400;
5525 6640 6640;
5526 6404 6404;
5527 7706 CTR, SETUP
5530 5534 INBA, IN2
5531 1330 INIT, IAD INBA:/start. set up return addr
5532 3071 DCR ITUP:/in 0071 so you can
5533 5727 JMP I CTR/do 7706 routine in MONITOR
```

```

5534 3044 IN2. DCA L4R:/OK, clear LAR & L3R
5535 3021 DCA L3R:
5536 4172 CALL:/lights off
5537 3154 LDR:
5540 4172 CALL:/blank display
5541 3806 BLANK:
5542 1125 TAD CHK:/check memory valid
5543 1310 TAD CH:
5544 7850 BNA CLR/OK?
5545 5354 JMP IN1:/yes
5546 1311 TAD MI:/no, turn on memory invalid light
5547 4172 CALL:
5550 4820 LDR:
5551 1310 TAD CH:/put correct value in mean check location (125)
5552 7041 CIA:
5553 3125 DCA CHK
5554 4172 IN1. CALL:/turn on APU
5555 5440 RDN:
5556 4172 CALL:/load a single 0 into APU
5557 3124 LDR:
5560 4124 F:/float it
5561 1313 TAD MG:/put in MAGNETIC VECTOR
5562 4142 F:
5563 1312 TAD TF:/put 10 floated into TENF
5564 4137 M:
5565 1315 TAD TENF:
5566 4142 F
5567 1314 TAD POT:/out  $\pi/2$  floated into PIT
5570 4137 M:
5571 1312 TAD FIT:
5572 4142 F:
5573 5470 JMP I INF/jump wherever calling routine wants to go

```

EXEC EXECUTIVE

B02=8443;
 B04=8453;
 RDT=7035;
 CHAR1=83;
 CALL=4173;
 RETURN=8375;
 BLANK=8606
 TEM11=55;
 AR2=8430;
 NYSP=8511;
 TEM13=57;
 KR1=8433;
 STEST=8412;
 RET=5147
 DICO=8234;
 KR2=8433;
 LOR=3154;
 APUOP=8600;
 RON=5440;
 BKPT=4167
 KYSPC=8210;
 RSTC=8222;
 STESTC=8215;
 ENEM=8200;
 EXITE=8244

Exits with TEM11=0 got a data clock
 1 "continue" pressed
 7777₈ "ADD ROD", "ENT" pressed

◆5000
 5000 7771 DIF, -7;
 5001 0017 MEK, 17;
 5002 7035 DATA, RDT;
 5003 7775 CONT, -3;
 5004 7776 TEST, -2;
 5005 7772 AR, -2;
 5006 7761 TTY, -17;
 5007 7762 RI, -18;
 5010 7765 ENT, -13
 5011 5812 EXEC, JMP I .+1;/patch to 6200
 5012 8200 ENEM;/CAP, turn on "RESET" lite, turn off APU
 5013 3055 DCR TEM11;/clear TEM11
 5014 8433 AR2;/KBR request?
 5015 5251 JMP E4;/no
 5016 8430 AR2;/yes, mask & save
 5017 0201 AND MEK;
 5020 3063 DCR CHAR1
 5021 1063 TAD CHAR1;/recall
 5022 1200 TAD DIF;/was it DISPLAY request?
 5023 7840 DCR CLA;
 5024 5237 JMP E2;/no, check further
 5025 4173 CALL;/yes
 5026 8210 NYSPC
 5027 1202 E2, TAD TTY;/was it MONITOR request?
 5030 1063 TAD CHAR1;
 5031 7840 DCR CLA;
 5032 5236 JMP E3;/no, check further
 5033 8453 B04;/yes, see if TTY plugged in
 5034 7000 GOR;
 5035 5802 JMP I DATA/doesn't matter - go to RDT (7038) - calls out raw data

```

5036 1203 E3: TAD CONT;/"CONTINUE" pressed?
5037 1063 TAD CHAR1;
5040 7100 CLL;
5041 7840 SZA CLA;
5042 5251 JMP E4;/no, go on
5043 1057 TAD TEM13/yes, is "CONTINUE" allowed? (TEMB=0 allowed
5044 7840 SZA CLA; #1 disallowed
5045 5251 JMP E4;/no, go on
5046 7101 CLL IAC;/yes, put a 1 in TEM11 to signal "CONTINUE"
5047 3055 DCA TEM11;
5050 5724 JMP I EXIT/exit to 6246
5051 6432 E4: KRF1/KBL request? (if it was any other KBR, program flow just
5052 5322 JMP E5;/no, go on clears it out)
5053 6430 AR2;/yes
5054 0201 AND MEK;/mask & save
5055 3053 DCA CHAR1;
5056 1063 TAD CHAR1;/recall
5057 1204 TAD TEST;/"TEST" pressed?
5060 7840 SZA CLA
5061 5254 JMP E6;/no, go on
5062 4172 CALL;/yes, run "self test"
5063 6215 STETC
5064 1063 E6: TAD CHAR1;
5065 1207 TAD AR;/was "RG" pressed?
5066 7840 SZA CLA;
5067 5272 JMP E7;/no, go on
5070 4172 CALL;/do "RESTART"
5071 6222 RSTC
5072 1063 E7: TAD CHAR1;
5073 1205 TAD AR;/was "ADD ROD" pressed?
5074 7840 SZA CLA;
5075 5322 JMP E5;/no, go on
5076 4172 CALL;/yes, lights off
5077 3154 LOP;
5100 7001 IAC;/message "1"
5101 4172 CALL;
5102 3234 DISCO;
5103 7200 CLA;
5104 6433 KRB/wait for a KBR
5105 5304 JMP .-1
5106 6430 AR2;/yes, mask & test
5107 0201 AND MEK;
5110 1210 TAD ENT;/enter pressed?
5111 7840 SZA CLA;
5112 5320 JMP E8;/no, go on
5113 7040 CMA;/yes
5114 3055 DCA TEM11;/signal "AR","ENTER" pressed by loading TEM11 with 7777
5115 4172 CALL;/blank & return
5116 3606 BLANK;
5117 5575 RETURN
5120 4172 E8: CALL;/blank on general principles
5121 3606 BLANK
5122 5723 E5: JMP I BATECH;/go to the battery check stuff, which will
5123 6502 BATECH: 6502/recycle back to EXEC
5124 6246 EXIT: EXITE+2

```

MSIM

IRF=703
ARG=5355;
FIT=374;
ELANF=3203;
TEMS=45;
TEM13=57;
TEM11=55;
DATA=2405;
TEMP=100
DIFCAL=5751;
LOA=3154;
EXEC=5011;
LOS=3124;
R=4142;
OTPS=47;
TEM10=54;
F=4164
A=4153;
M=4150;
D=4167;
P=4145;
S=4156;
M=4137;
L=4732;
M=4710;
E=4664;
TEMH=101
POTOTPS=52;
TEMP=50;
AVGV=4555;
CONOE=5704;
COM=4355;
COM1=4367;
PAKL=4441
SLEG=403;
M2EN=5420;
GTIN=5400
PROCI=2031;
DICOQ=3234;
PROCE=4022;
INIT=5531;
IDLE=5725;
STEST=6407;
LOH=4620
PRINIT=7072;
PRPO=7072;
CALL=4173;
RETURN=5575
DATCAL=4850;
SETIN=4463;
TEMP=53;
APUCF=6500;
ACB=5440;
MCFRR=6425;
BME=6451
MA157=6227


```

      *5200                                NEEDS WORK
5200 5212 MHA, MN1:
5201 0005 ID, 5:                                CTR3=>counts # of shots for
5202 0317 DIFF, 317:                            DIP averaging
5203 5531 INTA, INIT:
5204 0527 R54, 527:
5205 0004 BF, 4:
5206 4441 PBL, PABL:
5207 0403 CLEN, CLE5
5210 1200 MAIN1, TAB MHA:/start.  put return addr from "INIT" in loc 0070
5211 3070 DCA INP:
5212 5603 JMP I INTA/go do INIT
5213 6425 MN1, MCRAB:/set up PIE
5214 6451 BME2:
5215 5616 JMP I .+1;/patch to 6227
5216 6227 MA1EM/if KBL, continue @ MN; if KBR, go to MAIN2 @ MA2; also clears
5217 3047 MN, DCA CTR3;/clear CTR3
5220 7100 CLL:
5221 1201 TAB ID;/turn on "DIP" LED + "INITIAL" LED
5222 4172 CALL:
5223 4620 LON:
5224 3057 DCA TEM13;/a-low "continue"
5225 1202 TAB DIFF;/display current dip value
5226 4172 CALL:
5227 5355 ANG;/displays # stored as binary radians is 0-368 angle
5230 7040 CMA
5231 3045 DCA TEM5:
5232 4172 CALL;/go to EXEC for further instructions
5233 5011 EXEC
5234 1055 TAB TEM11;/data received? (i.e., TEM1=0?)
5235 7640 DCA CLA:
5236 5332 JMP ME;/no, go on
5237 3742 DCA I DIP1;/clear "DIP" @ LOC 0320
5240 3743 DCA I DIP2:
5241 3744 DCA I DIP3:
5242 3745 DCA I DIP4
5243 4172 M1, CALL;/go get new data set
5244 2405 DATA;/AC20, timeout error. AC=1
5245 3054 DCA TEM10;/TEM10 now has error information from DATA
5246 3100 DCA TEMP;/clear TEMP
5247 4172 CALL;/turn on APU
5250 5440 ADN:
5251 4172 CALL;/do data calibration
5252 4250 BATEAL:
5253 4172 CALL;/calculate dip & put it in REG4 & display it
5254 5751 DIFCAL
5255 1100 TAB TEMP;/is there a battery or other CHEK error?
5256 7640 DCA CLA:
5257 5261 JMP .+2;/yes
5260 5334 JMP .+4;/no
5261 1054 TAB TEM10;/yes, get TEM10
5262 7040 CMA;/complementing TEM10 make sure it indicates an error, no matter
5263 3054 DCA TEM10;/how DATA came out
5264 1305 TAB BF;/light up DIP light only
5265 4172 CALL
5266 4620 LON:
5267 1204 TAB R54;/get AC to point to REG4 for ANG
5270 4172 CALL;/display REG4 as an angle
5271 5355 ANG:
5272 6600 RANOFF;/turn off APU

```

```

5273 3101 DCA TEMN:/clear TEMN
5274 4172 CALL:/go to CONOE to handle any data error
5275 5704 CONOE:
5276 1101 TAD TEMN/CLR/CONT or ENT pressed?
5277 7850 DCA CLA:
5300 5306 JMP MB:/ENT pressed, go on
5301 7040 CMA/CLR/CONT pressed, put 7777g into TEM13 to disallow CONT
5302 3057 DCA TEM13:/in EXEC
5303 4172 CALL:/wait for operator requests or DATA. Assumes you didn't
5304 5011 EXEC:/like that Dip reading. It gets thrown away
5305 5243 JMP M1:/got a data clock, back to M1
5306 1047 MB, TAD CTR3:/we are continuing with a valid DIP reading
5307 3053 DCA TEM9:/put current CTR3 into TEM9 for AVGV
5310 1204 TAD R64:/point to current value of dip
5311 3055 DCA TEM11/put in TEM11 for AVGV
5312 1202 TAD DIFF:/make TEM7 point to accumulated average for AVGV
5313 3050 DCA TEM7:
5314 4172 CALL:/turn on APU
5315 5440 AON
5316 4172 CALL:/do the current average for DIP
5317 4555 AVGV:
5320 1205 TAD DF:/turn on DIP light
5321 4172 CALL:
5322 4220 LON:
5323 1202 TAD DIFF:/get current DIP average
5324 4172 CALL:/display as an angle
5325 5355 ANG:
5326 3057 DCA TEM13/allow continue
5327 4172 CALL:/wait for operator command or data
5330 5011 EXEC:
5331 1055 TAD TEM11/what happened?
5332 7840 DCA CLA:
5333 5336 JMP MB:/continue pressed (actually "AR","ENT" will get here too)
5334 2047 INC CTR3/increment average counter
5335 5243 JMP M1/do it again
5336 7040 MB, CMA:
5337 3045 DCA TEM5/signal "INITIAL" by making TEM5#0
5340 5741 JMP I .+1:
5341 5400 STIH/go on
5342 0320 DIP1, 320:
5343 0321 DIP2, 321:
5344 0322 DIP3, 322:
5345 0323 DIP4, 323:

```

<AWG, AWG

```

CONV=6014;
REGS=533;
CON=5604
M=4137;
R=4133;
I=4181;
F=4145;
RETURN=5575;
CALL=4172;
M=4150;
KEYT=33
ITATUD=4347;
PEUP=43;
R=4142
<REGS
◆5353
5353 5603 CN: CON-1;
5354 0533 REGS: REGS
5355 4137 AWG: M:/write REG4
5356 1353 TAB CN:/write ISO/π
5357 4137 M;
5358 4150 M:/do REG4x180 .
5359 1354 TAB REGS;/stroke in REG5
5360 4142 R;
5361 1354 TAB REGS;/point to REG5
5364 4172 CALL;/display # in REG5
5365 6014 CONV;
5366 5575 RETURN
<AWG
TWO=2025
5367 2024 TWOT, TWO-1
5370 4137 AWG: M;
5371 4153 R;
5372 1387 TAB TWOT;
5373 4137 M;
5374 4181 I;
5375 4145 F;
5376 5575 RETURN

```

KEYSER

KEY SERVICE

```

KR2=6433;
KR1=6432;
AR2=6430;
CHARF=61;
TEM8=51;
TEM7=50;
TEM5=45;
TEM14=62;
DIBCO=6234;
ACC1=3525;
KEYCTR=27;
CALL=4172;
RETURN=5575;
LOR=3154;
CONV=6014;
TEM6=46;
LON=4620;
ANG=5355;
M=4150;
R=4142;
W=4137;
KEYEN=6341;
BLANK=3606;
D=4161;
RNGE=2233;
*5600

```

```

5600 0017 MASK, 17;
5601 7775 IN1, -3;
5602 4600 DI, 4600;
5603 5603 OR, CON-1;
5604 6740 OR, 6740;
5605 6456 6456;
5606 6745 6745;
5607 6406 6406;
5610 0007 CE, 7;
5611 4172 MYER, CALL;/lights off
5612 3154 LOR;
5613 4172 CALL;/blank display
5614 3606 BLANK; 0-not "INITIAL"
5615 3045 DCA TEM5;/clear TEM5-used for else-"INITIAL"
5616 3051 DCA TEM8;/clear TEM8-used for 0=not an angle
5617 6007 ORF/clear any requests else-an angle
5620 6432 KR1;/wait for KBL request
5621 5230 JMP .-1;
5622 6430 AR2;/read keyboard
5623 0200 AND MASK;/mask least significant 4 bits
5624 3061 DCA CHARF;/save
5625 1061 TAD CHARF/recall
5626 1201 TAD IN1;/was "INITIAL" pressed?
5627 7640 OR CLR;
5630 5243 JMP 5201/no, go on
5631 7901 MYER2, IAC;/yes, light "INITIAL" light
5632 4172 CALL;
5633 4620 LON;
5634 7040 DCA;
5635 3045 DCA TEM5/load TEM5 with 7777

```

```

5636 6432 KYCR3, KR1:/next press?
5637 5235 JMP .-1;
5640 6430 KR2:/get it
5641 0200 AND MCRK;
5642 3061 DCR CHAR/save it
5643 1061 KYCR1, TAD CHAR
5644 1202 KYCR0, TAD DI:/add branch table starting addr to it
5645 3062 DCR TEM14:/put in RAM
5646 5462 JMP I TEM14/jump to branch table, 4600+ CHAR
5647 4172 KYCR0, CALL:/patch: KYEX displays value & gets another one in
5650 6341 KYEX/TOS of "INITIAL"
5651 7200 CLA;
5652 1027 TAD KEYCTR:/get KYCTR#if new value has been keyed in
5653 7850 CMA CLA;
5654 5575 RETURN/return if no change to selected variable
5655 1045 TAD TEM5/"INITIAL" selected?
5656 7850 CMA CLA;
5657 5272 JMP KR/no; ∴ error...can't change parameter w/o "INITIAL"
5660 1051 TAD TEM3:/is it an angle?
5661 7850 CMA CLA;
5662 5267 JMP KR:/no
5663 1203 TAD CR:/yes, load 180/π
5664 4137 M;
5665 4172 CALL:/do the conversion fromdegrees to radians (0°-360°)
5666 2223 ANGE
5667 1046 KR, TAD TEM6:/puts result in parameter pointed to by TEM6
5670 4142 R;
5671 5575 RETURN
5672 1210 KR, TAD CR:/signal "7" error message (never does this)
5673 4172 CALL;
5674 3234 DISCO;
5675 7200 CLA;
5676 5575 RETURN

```

can do without, just make KR, RETURN

GETIN

/GET initial conditions does initial calculations
GTIN actually gets parameters

```

W=4137:
P=4145:
R=4142:
C=4156:
SINE=2723:
COS=6138:
M=4150:
CALL=4172:
RETURN=5575
♦4442
4442 6400 PARL, 6400:
4443 6400 6400:
4444 6640 6640:
4445 6405 6405:
4446 0403 LLEN, 403:
4447 0413 LT1, 413:
4450 0423 DEPPT, 423:
4451 0373 PITT, 373:
4452 0477 ABER, 477:
4453 0503 AINC, 503:
4454 0467 BER1, 467:
4455 0507 BER2, 507:
4456 0473 INC1, 473:
4457 0513 INC2, 513:
4460 0517 AVBER, 517:
4461 0523 AVINC, 523:
4462 0433 VDR, 433/vd
4463 1252 GETIN, TAD ABER;/write ABER
4464 4137 W:
4465 4145 P:
4466 1254 TAD BER1;/put ABER into BER1
4467 4142 R:
4470 4145 P:
4471 1260 TAD AVBER;/and AVBER
4472 4142 R:
4473 1255 TAD BER2;/and BER2
4474 4142 R:
4475 1253 TAD AINC;/put AINC into INC1
4476 4137 W:
4477 4145 P:
4500 1256 TAD INC1:
4501 4142 R:
4502 4145 P:
4503 1261 TAD AVINC;/and AVINC
4504 4142 R:
4505 1257 TAD INC2;/and INC2
4506 4142 R:
4507 1253 TAD AINC:
4510 4137 W:

```

```

4511 1251 TAD PITT;/get AINC- $\pi/2$ 
4512 4137 M;
4513 4156 D;
4514 4145 P;
4515 4172 CALL;
4516 2723 SINE;/sin (AINC- $\pi/2$ )
4517 1246 TAD CLEN;
4520 4137 M;
4521 4150 M;/slewxsin(AINC- $\pi/2$ )=VD
4522 1252 TAD VDH;/VD $\rightarrow$ 0434-0437
4523 4142 R;
4524 4172 CALL;/cos(AINC- $\pi/2$ )
4525 6136 COS;
4526 1246 TAD CLEN;
4527 4137 M;
4530 4150 M;/slewxcos(AINC- $\pi/2$ )
4531 4145 P;
4532 1250 TAD DEPPT/store in DEPPT
4533 4142 R;
4534 1252 TAD ABER;
4535 4137 M;
4536 4172 CALL;
4537 6136 COS;
4540 4150 M;/cos(ABER)xslewxcos(AINC- $\pi/2$ )
4541 1247 TAD LT1;
4542 4142 R;/put in LAT
4543 1250 TAD DEPPT;
4544 4137 M;
4545 1252 TAD ABER;
4546 4137 M;
4547 4172 CALL;
4550 2723 SINE
4551 4150 M;/sin ABERxslewxcos(AINC- $\pi/2$ )  $\rightarrow$ DEP
4552 1250 TAD DEPPT;
4553 4142 R;
4554 5575 RETURN

```

<PROC2

```

ADDP=153;
ARAIN=2277;
ARTAN=2255;
CALL=4172;
CHS=3761;
DIMP=151;
KEYT=33;
MULF=150;
WDMT=3258;
DETT=6138;
AVG=5370;
RBUF=43;
PIAS=2305;
POP=2221;
PUSH=145;
RD=142;
RETURN=5575;
SORT=2703;
STATUS=4347;
SUBF=156;
XCH=3144;
WT=137;
R=JMC ADDP;
D=JMC DIMP;
P=JMC PUSH;
R=JMC RD;
S=JMC SUBF;
M=JMC MULF;
W=JMC WDMT;
LINE=2723;
COD=6138;
RBUF=43

```

<PROC2
***4000**

```

4000 0467 BEP1, 467;
4001 0503 AINC, 503;
4002 0517 AVBEP, 517;
4003 0403 CLE6, 403;
4004 0367 RDDL, 367;
4005 0413 LAT1, 413;
4006 0473 INCI, 473;
4007 0523 AVINC, 523;
4010 0423 DEPT, 423;
4011 0433 VD, 433;
4012 0443 THDP, 443;
4013 0477 BEEP, 477;
4014 0327 LRD, 327;
4015 0463 LIEM, 463;
4016 0223 COB, 223;
4017 0227 COA, 227;
4020 0223 IIB, 223;
4021 0223 IIA, 223;

```



```

4022 1206 PROC2: TAD INC1;
4023 4137 M;
4024 1207 TAD RWIND;
4025 4172 CALL;
4026 5370 AVG;
4027 4172 CALL;
4030 6136 COS;
4031 1221 TAD CIA;
4032 4142 R;
4033 4172 CALL;
4034 2723 SINE;
4035 1217 TAD COA;
4036 4142 R /SIN(COA) REVERSED TO CONV RWIND TO THETA
4037 1204 TAD FOOL;
4040 4137 M;
4041 1203 TAD CLEG;
4042 4137 M;
4043 4153 A;
4044 1203 TAD CLEG;
4045 4142 R;
4046 1200 TAD BEP1;
4047 4137 M;
4050 1202 TAD RWBER;
4051 4172 CALL;
4052 5370 AVG;
4053 4172 CALL;
4054 2723 SINE;
4055 1220 TAD SIB;
4056 4142 R;
4057 4172 CALL;
4060 6136 COS;
4061 4145 R;
4062 1216 TAD COB;
4063 4142 R;
4064 1217 TAD COA;
4065 4137 M;
4066 4150 M;
4067 1204 TAD FOOL;
4070 4137 M;
4071 4150 M;
4072 1205 TAD LAT1;
4073 4137 M;
4074 4153 A;
4075 4172 CALL;
4076 4347 STATUS;
4077 3043 ICA PEUF
4100 1205 TAD LAT1
4101 4172 CALL;
4102 6156 DETT
4103 1211 TAD VD;
4104 4137 M;
4105 1204 TAD FOOL;
4106 4137 M;
4107 1221 TAD CIA;
4110 4137 M;
4111 4150 M;
4112 4156 C;
4113 1211 TAD VD;
4114 4142 R;

```

```

4115 1205 TAD LAT1:
4116 4137 M:
4117 4145 P:
4120 4150 M:
4121 1210 TAD DEPT:
4122 4137 M:
4123 4145 P:
4124 4150 M:
4125 4153 A:
4126 4145 P:
4127 4172 CALL:
4130 2703 COPT:
4131 1214 TAD LAD:
4132 4142 P:
4133 1211 TAD VD
4134 4137 M:
4135 4145 P:
4136 4150 M:
4137 4153 A:
4140 4172 CALL:
4141 2703 COPT:
4142 1212 TAD THD:
4143 4142 P
4144 1210 TAD DEPT:
4145 4137 M:
4146 1205 TAD LAT1:
4147 4137 M:
4150 4161 D:
4151 4172 CALL:
4152 2255 RTAN:
4153 4172 CALL:
4154 2305 PIAC:
4155 1213 TAD ABEP:
4156 4137 M:
4157 4156 D:
4160 4145 P:
4161 4172 CALL:
4162 5136 COI:
4163 4172 CALL:
4164 3144 MOH:
4165 4172 CALL:
4166 2723 SINE
4167 1214 TAD LAD:
4170 4137 M:
4171 4150 M:
4172 1215 TAD LDEV:
4173 4142 P
4174 1201 TAD PIAC:
4175 4172 XXXXXXXX JMPI+1 (5776)
4176 3252 XXXXXXXX 6451
4177 5575 XXXXXXXX

```

AVGV, SYMBOL TABLE

```

A      4153
AVGW   4555
CALL   4172
D      4161
F      4164
LD0    3124
M      4150
R      4142
RETURN 5575
TEM11  0055
TEM7   0050
TEM9   0053
W      4137
    
```

```

PC00241 MD5214 A0000 U3155 L1 D0
>02002 7002
>0
    
```

AVGW

/from AVerage Value

```

TEM9=53;           Enter with TEM7-> (current value)
TEM11=55;          TEM9-> # of iterations (0=1st time)
TEM7=50;           TEM11-> (average value)
LD0=3124;         Exit with TEM7-> (unchanged)
W=4137;           TEM9-> unchanged
M=4150;           TEM11-> (new average value)
F=4164;
R=4142;
D=4161;
CALL=4172;
RETURN=5575;
R=4142
    
```

```

4555  1053  AVGW, TAD TEM9;/fetch current # of iterations (N)
4556  4172  CALL;/load & float
4557  3124  LD0;
4558  4164  F;
4561  1050  TAD TEM7;/point to accumulated average (AV)
4562  4137  W;
4563  4150  M;/ (NxAV)
4564  1055  TAD TEM11;/write current value (CV)
4565  4137  W;
4566  4153  R/ (NxAV)+CV
4567  1053  TAD TEM9;/load N+1
4570  7001  IAC;
4571  4172  CALL;
4572  3124  LD0;
4573  4164  F;  $(NxAV)+CV$ 
4574  4161  D;/  $\frac{N+1}{N+1}$  = new AV
4575  1050  TAD TEM7;/put the result in loc pointed to by TEM7
4576  4142  R;
4577  5575  RETURN
    
```

BATCHK /check batteries

```
DISCO=3234;
LON1=4622;
CALL=4172;
RETURN=5575;
B01=6442;
B02=6443;
TEMP=100
STATUS=4347;
EXITE=6244
♦6500
6500 0020 LB, 20;
6501 5012 EXEC1, 5012;
6502 6442 BATCHK, B01;/processor battery low?
6503 5313 JMP .+8;/no, go on
6504 1300 TAD LB;/yes, turn on "LO BATTERY"
6505 4172 CALL;
6506 4622 LON1;
6507 4172 CALL;/display a "0" code
6510 3234 DISCO
6511 7000 NOP;
6512 7000 NOP;
6513 5714 JMP I .+1;/continue with EXITE
6514 6244 EXITE;
6515 7000 NOP
```

```

REBAT /Receiver Battery Check
6516 0004 STTM, 4;
6517 0314 RSTAT, 314;
6520 1717 RBAT, TAD I RSTAT; /get receiver status word
6521 0316 AND STTM;/mask off bit 9
6522 7650 SNA CLA;/battery OK?
6523 5325 JMP .+2 /no
6524 5575 RETURN;/yes, return
6525 5343 JMP CHEK2 /exit thru CHEK2 to turn on LO BATTERY

```

```

TEME /TEMPERATURE ERROR HANDLER
TEM0=75
6526 7132 TEME, STL RTR; /turn on HI TEMP
6527 4172 CALL;
6530 4620 LON;
6531 7040 CMA; /put 77778 into TEMD
6532 3075 DCA TEMD;
6533 5350 JMP CHEK3 /exit thru CHEK3 to set TEMP=1

```

```

CHEK /used to handle battery check
TEM10=54;
LON=4620
6534 0020 LITE, 20;
6535 0010 DIS, 10;
6536 4172 CHEK, CALL; /number in TOS negative?
6537 4347 STATUS;
6540 7650 SNA CLA;
6541 5575 RETURN;/yes
6542 1335 CHEK1, TAD DIS /no, display "8" code
6543 4172 CHEK2, CALL;
6544 3234 DISCO;
6545 1334 TAD LITE; /turn on "LO BATT" lite
6546 4172 CALL;
6547 4622 LON1 /LON1 turns on L4 lites
6550 7001 CHEK3, IAC; /put a "1" in TEMP
6551 3100 DCA TEMP;
6552 5575 RETURN

```

```

KYBLK
BLANK=3606;
JMPR=30;
KEYCTR=27;
MINUS=31
♦6553
6553 4264 ENTER, -3514
6554 1031 KYBLK, TAD MINUS;
6555 1027 TAD KEYCTR;
6556 7640 SZA CLA;
6557 5430 JMP I JMPR;
6560 1353 TAD ENTER;
6561 1030 TAD JMPR
6562 7650 SNA CLA;
6563 5430 JMP I JMPR;
6564 4172 CALL;
6565 3606 BLANK;
6566 5430 JMP I JMPR

```

KYEX

```
TEMS=45;  
LON=4620;  
TEMS=51;  
TEMS=46;  
CONV=6014;  
CALL=4172;  
RETURN=5575;  
ACC=3521;  
ANG=5355;  
CONV=6014;  
KEYCTR=27;  
ROM=5440;  
APUOF=6600;  
ANGA=2214  
♦6341  
6341 4172 KYEX, CALL;/turn on APU  
6342 5440 ROM;  
6343 1051 TAD TEMS;/is it an angle?  
6344 7650 SNA CLA;  
6345 5352 JMP KYSRD;/no  
6346 1046 TAD TEMS;/yes, display as 0°-360°  
6347 4172 CALL;  
6350 2214 ANGA;  
6351 5355 JMP KE  
6352 1046 KYSRD, TAD TEMS;/display as a length in feet  
6353 4172 CALL;  
6354 6014 CONV  
6355 6600 KE, APUOF;/turn off APU  
6356 1045 TAD TEMS;/"INITIAL"?  
6357 7650 SNA CLA;  
6360 5373 JMP KM;/no  
6361 7001 IAC;/yes, turn on "INITIAL" lite  
6362 4172 CALL;  
6363 4620 LON;  
6364 4172 CALL;/get a # from operator  
6365 3521 ACC;  
6366 7000 NOP  
6367 1087 TAD KEYCTR;/was a new # entered?  
6370 7650 SNA CLA;  
6371 5373 JMP KM;/no  
6372 5575 RETURN  
6373 3027 KM, DCA KEYCTR;/zeroize keycounter  
6374 5575 RETURN  
  
6375 7000 PRINT, NOP;  
6376 5575 RETURN  
6377 7000 PRPO, NOP;  
6400 5575 RETURN
```

EXEC OVERFLOW

```
APUDF=6600;
EXEC=5013;
STEST=6412;
KYSR=5611;
RST=5147;
CALL=4172;
RETURN=5575
LON1=4622;
TEMS=57
/EXEC
*6200
6200 6007 EXEC, CAF;/clear all requests
6201 6600 APUDF;/turn off APU
6202 1207 TAD RDY;/turn on RESET lite
6203 4172 CALL;
6204 4622 LON1;
6205 5606 JMP I EXE/return to EXEC
6206 5013 EXE, EXEC;
6207 2000 RDY,2000
/KYSRC
6210 4172 KYSRC, CALL;/calling routine for KYSR
6211 6246 EXITE+2;
6212 4172 CALL;
6213 5611 KYSR;
6214 5575 RETURN
/STESTC
6215 4172 STESTC, CALL;/calling routine for STEST
6216 6246 EXITE+2;
6217 4172 XXXXX JMPL.+1 5620
6220 6412 STEST;
6221 5575 RETURN
/RSTC
6222 4172 RSTC, CALL;/calling routine for RST
6223 6246 EXITE+2;
6224 4172 CALL;
6225 5147 RST;
6226 5575 RETURN
```

MA1EX /MAIN1 EXTENSION

MA1EX

```

6227 6007 MA1EX; CHF; /clear all requests
6230 1200 TAD EXEX; /display "T"
6231 4172 CALL;
6232 3234 DISCO;
6233 6432 KR1;/KBL?
6234 5236 JMP MA1EX1;/no, try KBR
6235 5643 JMP I MNA/yes, back to MAIN1 @ MN
6236 6433 MA1EX1, KFE;/KYBR?
6237 5227 JMP MA1EX;/no, start over
6240 3057 DCH TEM5;/yes, clear TEM5
6241 5642 JMP I MA2N;/back to MAIN2 @ MA2
6242 6632 MA2N, MA2;
6243 5217 MNA, MN
/EXITE
B32=6443;
CHLITE=2516
6244 6443 EXITE, B32;/this is not done
6245 5201 JMP EXEX+1;
6246 7320 CLA STL;/turn off RESET lite
6247 7421 MDL;
6250 1254 TAD RDYD;
6251 4172 CALL
6252 2516 CHLITE;
6253 5575 RETURN;/return
6254 5777 RDYD, 5777
/EEDEF
W=4137; /change to PROC1 to call 0° down
XCH=3144; see PROC1 for explanation
S=4156;
CHS=3761;
R=4153
*6260
6260 4137 PROPA, W;
6261 4172 CALL;
6262 3144 XCH;
6263 4172 CALL;
6264 3761 CHS;
6265 4153 R /S IF 0 DEGREES IS LF
6266 5667 JMP I .+1;/back to PROC1 @ 2042
6267 2042

```



```

CTR2=42;
TEM=10;
LDS=3124;
WT=137;
ADDS=3134;
MULS=3140;
FLT=164
EW1=6441;
DIWF=161;
CHS=3761;
RD=142;
CALL=4172;
RETURN=5575

```

SCDATA ♦6300 /Scale Data

```

6300 0243 R,      243
6301 0005 FI,    5
6302 7774 TMD,   -4
6303 0007 TFS,   7
6304 7766 TE,    -12
6305 1304 SCDATA, TAD TE/make CTR2 count 1010 times
6306 3042      DCA CTR2
6307 1300      TAD R /put addr of 1st data loc (244-247) into T
6310 3010      DCA TEM
6311 1301 SCA,   TAD FI/load 5 into TOS
6312 4172      CALL
6313 3124      LDS
6314 1010 TAD TEM /load 1st (next) data word [D.W.] as 32 bit
6315 4137 JMS WT
6316 4172      CALL/create 16 bit # (single) for DW
6317 3134      ADDS
6320 4172      CALL/DW (single) x5 (single)
6321 3140      MULS
6322 4164 JMS FLT /float the result
6323 7040      CMA /load 204710 (float)
6324 6441      EW1
6325 0303      AND TFS
6326 6441      EW1
6327 4164 JMS FLT      D.W.x5
6330 4161 JMS DIWF/get 204710 (float)
6331 4172      CALL/change sign to compensate for downhole inver
6332 3761      CHS
6333 1010 TAD TEM /WT advances the addr in TEM, so get it
6334 1302 TAD TMD /back and load with the scaled data
6335 4142 JMS RD
6336 2042 ISZ CTR2 /10 times?
6337 5311 JMP SCA/no, do-it again
6340 5575      RETURN /yes, return

```

FIELD TEST CALLS AND PATCHES

STEST=5500;
 LON=4620;
 LON1=4622;
 MEMOR=6100;
 MEMNOR=6500;
 CALL=4172;
 RETURN=5575;
 DATA=2405;
 ACM=5440;
 RPUCP=6600;
 CONV=6014;
 RET=5563;
 TEMP=101

		♦S400
6400	7840	<u>STST</u> , CLR CMA;
6401	4172	CALL;
6402	4620	LON;
6403	7040	CMA;
6404	4172	CALL;
6405	4622	LON1;
6406	6100	MEMOR;
6407	5510	JMP I,+1;
6410	5500	STEST
6411	6500	<u>STST</u> , MEMNOR;
6412	4172	CALL;
6413	2405	DATA;
6414	6100	MEMOR;
6415	5516	JMP I,+1;
6416	5563	RET
6417	6500	<u>STST</u> , MEMNOR;
6420	4172	CALL;
6421	5440	ACM;
6422	1101	TRD TEMP;
6423	4172	CALL;
6424	6014	CONV;
6425	5270	JMP END;
6426	7000	NOP;
6427	7000	NOP

INITIAL CONDITIONS PRINT ROUTINE

		INCO=4400;
		MAINE=6620
6430	6100	INITCO , MEMOR;
6431	5532	JMP I,+1;
6432	4400	INCO
6433	6500	INIT1, MEMNOR;
6434	4172	CALL;
6435	3506	BLANK;
6436	5537	JMP I,+1;
6437	6620	MAINE

RESTART PRINT ROUTINE

LDA=3154;
RST=4412
6440 4172 RESTR; CALL;
6441 3154 LDA;
6442 6100 MEMSW;
6443 5844 JMP I .+1;
6444 4412 RST
6445 6500 RESTR1; MEMNOR;
6446 4172 CALL;
6447 3606 BLANK;
6450 5575 RETURN

SURVEY PRINT ROUTINE

WDVT=3256;
SUR=4424;
BLANK=3606
6451 4172 SURVEY; CALL;
6452 3256 WDVT;
6453 6100 MEMSW;
6454 5855 JMP I .+1;
6455 4424 SUR
6456 6500 SURV1; MEMNOR;
6457 4172 CALL;
6460 3606 BLANK;
6461 5575 RETURN

USED BY PRINT CALLER

ANSA=2214
6462 6500 STSTA; MEMNOR;
6463 4172 CALL;
6464 5440 ANI;
6465 1101 TAD TENN;
6466 4172 CALL;
6467 2214 ANSA;
6470 6600 END; AFUOF;
6471 6100 MEMSW;
6472 7800 CLA;
6473 5575 RETURN

CONV

/displays a # as a decimal #

♦8000/enter with # to be displayed in TOS

6000	0004	FOUR,	4
6001	7000	BLK,	7000
6002	0217	TENF,	217/addr of 10 floated
6003	7773	FI,	-5
6004	0240	HTH,	240
6005	0206		206
6006	0001		1
6007	0000		0
6010	6003	HTHL,	HTH-1/addr of HTH for WT routine
6011	0230	REG2,	REG2
6012	0227	REG2M,	REG2-1/addr of REG2 for WT routine
6013	0001	TW,	1
6014	4172	CONV,	CALL/if is \geq xxxx.xx5, rounds up. $<$ xxxx.xx5, rounds down
6015	2257		POF
6016	1203		TAD FI/make CTR2 count to 5
6017	3042		DCA CTR2
6020	4172		CALL/blank display
6021	3606		BLANK
6022	1202		TAD TENF/load 10
6023	4137	JMS WT	
6024	4145	JMS PUSH	
6025	4150	JMS MULF	
6026	4150	JMS MULF/create #x100	
6027	4172		CALL /plus or minus?
6030	4347		STATUS
6031	7650		SNA CLA
6032	5236		JMP .+4/plus
6033	4172		CALL/minus, change sign, &
6034	3761		CHS
6035	7013		IAC RTR/put 1 in MSB of AC
6036	3031		DCA MINUS/store in MINUS
6037	4172		CALL /FIX (double precision -16 bits) the #
6040	6130		FIXD
6041	1210		TAD HTHL/write 100,000
6042	4137	JMS WT	
6043	7100	CE,	CLL
6044	2027		ISZ KEYCTR/increment keystroke counter
6045	1212		TAD REG2M/put TOS into REG2 (will have the next power of 10)
6046	4142	JMS RD	
6047	4145	JMS PUSH	/push the working number
6050	1212		TAD REG2M/get the power of 10 back
6051	4137	JMS WT	
6052	4172		CALL /÷ by the power of 10, truncate fractional part
6053	2713		DIWD
6054	4145	JMS PUSH	/save it in the stack
6055	4172		CALL/picks off the 4 LSB's of TOS & uses DISPR to display
6056	3370		LSW it as a decimal #. Throws
6057	1212		TAD REG2M/get power of 10 out TOS
6060	4137	JMS WT	
6061	4172		CALL /multiply by truncated integer
6062	2673		MULD
6063	4172		CALL /remove MSD from working #
6064	2717		SUBD
6065	2042		ISZ CTR2/done 5 times?
6066	5273		JMP C3/no
6067	2027		ISZ KEYCTR/causes DISPR to put in decimal pt. after 4 #s
6070	4172		CALL/goes to DISPR with 6th digit
6071	3370		LSW
6072	5312		JMP EXIT 195

6073	1212	OS,	TAD R6EM /create next lower power of 10
6074	4137	JMS WT	
6075	1202		TAD TENF
6076	4137	JMS WT	
6077	4172		CALL
6100	6130		FIXD
6101	4172		CALL
6102	2713		DIVD
6103	1213		TAD TW/is this the 4th time?
6104	1042		TAD CTR2
6105	7640		SZA CLA
6106	5243		JMP C2/no, do it again
6107	4172		CALL/yes, DISPR will push digits over 2 places
6110	3630		DISPR/out in a decimal point, then return
6111	5243		JMP C2/do it again
6112	1031	EXIT,	TAD MINUS/negative #?
6113	7650		SNA CLA
6114	5575		RETURN/no, return
6115	1025		TAD DISPR2/yes, make sure MSD of display is bl
6116	1201		TAD BLK/so minus sign may appear
6117	3025		DCA DISPR2
6120	4172		CALL
6121	3672		DIS3
6122	7240	CLA CMA/	turn on minus sign
6123	7421		MQL
6124	7121		IAC STL
6125	4172		CALL
6126	2516		CHLITE
6127	5575		RETURN/done
6130	4172	FIXD,	CALL/the "fix double" APU routine
6131	2727		CRAB
6132	1335		TAD .+3
6133	5734		JMP I .+1
6134	2734		BW
6135	0036		36
			/COS
6136	4172	COS,	CALL/the cosine routine
6137	2727		CRAB
6140	1343		TAD .+3
6141	5742		JMP I .+1
6142	2734		BW
6143	0003		3
			/PI
6144	4172	PI,	CALL/puts PI in TOS
6145	2727		CRAB
6146	1351		TAD .+3
6147	5750		JMP I .+1
6150	2734		BW
6151	0032		32

FDT

```

R2=6433;
RR2=6430;
R=4164;
CALL=4172;
RETURN=5575;
M=4137;
R=4142;
RDN=3440;
CHAR1=63;
CT=102;
CONV=6014;
BC4=6453;
M=4150;
AFUCF=6600;
DIDRR2=25;
DIDG=3672;
D=4161;
BM=2734;
CFRB=2727;
R=4153;
CTR=27;
R=4145;
MEMNOR=6500;
EXITE=6246

```

•7010

```

7010 0243 LIST, 243;
7011 0247 247;
7012 0253 253;
7013 0257 257;
7014 0263 263;
7015 0267 267;
7016 0273 273;
7017 0277 277;
7020 0303 303;
7021 0307 307;
7022 7007 START, LIST-1;
7023 0314 RCMR, 314;
7024 0217 TEN, 217;
7025 0567 DEBUS, 567;
7026 7766 CONT, -12;
7027 0017 MCK, 17;
7030 7771 DICE, -7;
7031 0377 MK, 377;
7032 0003 MK1, 3;
7033 5011 EMSC, 5011;
7034 7770 EM, -10;
7035 5371 FDT, JMP AMD;
7036 6433 BK, RR2;
7037 5236 JMP .-1;
7040 6430 RR2;
7041 0227 AND MCK;
7042 3063 DCA CHAR1;
7043 1063 TAD CHAR1;
7044 1350 TAD DICE;
7045 7640 ICA CLR;
7046 5350 JMP NEXT;
7047 7100 CLL;
7050 1226 TAD CONT;
7051 3102 DCA CT;
7052 1222 TAD START;
7053 3011 DCA 11

```

7055	5440	CALL;
7056	1411	TAD I 11;
7057	4137	M;
7058	1224	TAD TEN;
7059	4137	M;
7060	4150	M;
7061	1224	TAD TEN;
7062	4137	M;
7063	4150	M;
7064	1225	TAD DEBUG;
7065	4142	R;
7066	1225	TAD DEBUG;
7067	4172	CALL;
7068	6014	COMV;
7069	6600	AFUDF;
7070	6433	KR2;
7071	6274	JMP .-1;
7072	6102	ISZ CT;
7073	6254	JMP BACK;
7100	6500	REC. MEMNOR;
7101	4172	CALL;
7102	5440	ACN;
7103	1353	TAD TTF;
7104	4137	M;
7105	1623	TAD I PCVR;
7106	7012	RTR;
7107	7421	MOL;
7110	1232	TAD MK1;
7111	7501	MOR;
7112	6441	6441;
7113	7002	BCW;
7114	7012	RTR;
7115	0227	AND MKK;
7116	6441	6441;
7117	4164	F;
7120	4161	D;
7121	4172	CALL;
7122	7184	LOG;
7123	1224	TAD TEN;
7124	4137	M;
7125	4145	R;
7126	4153	A;
7127	4150	M;
7130	4145	R;
7131	4153	A;

RDT, Page 2

7132	1683	TAD I ACVR;
7133	7012	ATR;
7134	7012	ATR;
7135	7230	IDL CLA;
7136	5342	JMP .+4;
7137	1260	TAD THY;
7140	4127	M;
7141	4153	A
7142	1225	TAD DEBUG;
7143	4142	R;
7144	1225	TAD DEBUG;
7145	4172	CALL;
7146	6014	CONV;
7147	5633	JMP I EXEC
7150	6453	NEXT, B34;
7151	5633	JMP I EXEC;
7152	4167	4167
7153	7152	ITF, ITF-1;
7154	6400	6400;
7155	6600	6600;
7156	6413	6413;
7157	0010	LG, 10
7160	7157	THY, THY-1;
7161	6400	6400;
7162	6760	6760;
7163	6405	6405
7164	4172	LOG, CALL;
7165	2727	CRAB;
7166	1357	TAD LG;
7167	5770	JMP I .+1;
7170	2734	BM
7171	6007	RAD, CAF;
7172	4172	CALL;
7173	6246	EXITE;
7174	5236	JMP BK

ZMIBR

IR=70;
ANG=5355;
PIT=374;
BLANK=3606;
TEMS=45;
TEM13=57;
TEM11=55;
DATA=2405;
TEMP=100
DIPCAL=5751;
LOR=3154;
EXEC=5011;
LDS=3124;
R=4142;
CTR3=47;
TEM10=54;
F=4164
A=4153;
M=4150;
D=4167;
P=4145;
S=4156;
W=4137;
TEMH=101
ROTCTR=52;
TEM7=50;
AVGW=4555;
COMOE=5704;
COM=4356;
COM1=4367;
PAKL=4441
SLEG=403;
MSEX=5422;
GTIN=5400;
ROM=5440;
APUDF=6600
PROC1=2031;
DISCO=3234;
PROC2=4022;
INIT=5531;
IDLE=5765;
STEST=6407;
LON=4620
PRINIT,=7772;
PRPO=7772;
CALL=4172;
RETURN=5575
DATCAL=4250;
GETIN=4463;
TEM9=53

```

6600 0467 B1, 467;
6601 0507 B2, 507;
6602 0473 I1, 473;
6603 0513 I2, 513;
6604 6603 ER, ER-1; /Bearing limit - should be approx. 1.5°
6605 6400 6400;6567
6606 6600 6600;6726 1.5° in radians* IS ON ROM 2/22/80
6607 6477 6477;6573
6610 6607 IN, IN-1; /inclination limit - should be approx. 1.5°
6611 6400 6400;6772
6612 6600 6600;6616 } 2° in radians* IS ON ROM 2/22/80
6613 6477 6477;6574 }
6614 0003 THR, 3;
6615 0517 AVBR, 517;
6616 0523 AVIN, 523;
6617 0002 INL, 2
6620 4172 MAIN2, CALL; /turn on APU
6621 5440 ROM;
6622 1215 TAD AVBR;
6623 4137 W; } /replace BER1 with AVBR
6624 1200 TAD B1; }
6625 4142 R; }
6626 1216 TAD AVIN; }
6627 4137 W; } /replace INCI with AVINC
6630 1202 TAD I1; }
6631 4142 R }
6632 4172 MA2, CALL; /wait for new data
6633 5011 EXEC;
6634 1055 MA2N, TAD TEM11; /make sure pressing "AP", "ENT" does not
6635 7640 SZA CLA; /move the program on; only new data
6636 5232 JMP MA2;
6637 3052 DCA ROTCTR /clear rotation counter
    
```

- *- to get change these values:
- (1) on front panel, set initial dip to value you want (e.g., 2°)
 - (2) read locations 0321, 0322 & 0323 for the 3 octal #'s for that angle

```

6640 4172 M4, CALL; / get DATA
6641 2405 DATA;
6642 3054 DCA TEM10; /store DATA's error-message
6643 3100 DCA TEMP; /zeroize TEMP
6644 4172 CALL; /APU ON
6645 5440 ADN
6646 4172 CALL;/calibrate data
6647 4250 DATCAL;
6650 1100 TAD TEMP;/any DATCAL errors? (TEMP = 1?)
6651 7640 SZA CLA;
6652 5254 JMP .+2 /yes
6653 5257 JMP .+4; /no
6654 1054 TAD TEM10;/complement TEM10 so it will indicate error
6655 7040 CMA; /however DATA left it
6656 3054 DCA TEM10
6657 4172 M5, CALL;/calculate BER2 and INC2
6660 2031 PROC1;
6661 3053 DCA TEM9;/ clear TEM9, used here as error store for COM1
6662 1201 TAD B2;/compare BER2 with BER1 to see if it in limits
6663 4137 W;
6664 1200 TAD B1;
6665 4172 CALL;
6666 4356 COM;
6667 1204 TAD B3;
6670 4172 CALL;
6671 4367 COM1
6672 1203 TAD I2;/compare INC2 with INC1
6673 4137 W;
6674 1202 TAD I1;
6675 4172 CALL;
6676 4356 COM;
6677 1210 TAD IN;
6700 4172 CALL;
6701 4367 COM1
6702 1053 TAD TEM9
6703 7650 SNA CLA;/out of limits?
6704 5317 JMP M6;/no, go on
6705 3053 DCA TEM9;/yes
6706 1214 TAD THR;/display "3" code
6707 4172 CALL;
6710 3234 DISCO;
6711 6433 KR2;/wait for KBR to show operator acknowledge
6712 5311 JMP .-1
6713 4172 CALL;/lights off
6714 3154 LDR;
6715 4172 CALL;/APU on. (unnecessary)
6716 5440 ADN

```

```

6717 1217 MS, TAD INL:/turn on INC lite
6720 4172 CALL:
6721 4620 LDM
6722 1203 TAD I2:/display INC2
6723 4172 CALL:
6724 5355 AVG:
6725 5600 APUOF /AUP off
6726 3101 DCR TEMN:/clear TEMN
6727 4172 CALL:/blink the lights and wait for operator "ENT" or "CLR"
6730 5704 CONGE:/
6731 1101 TAD TEMN:/TEMN = 1 if CLR, 0 if ENT
6732 7650 CMA CLA:/1 ENT?
6733 5341 JMP M7:/yes, go on
6734 7040 CMA:/no, disallow "CONTINUE"
6735 3057 DCR TEM13 /and wait for new data
6736 4172 CALL:/Pressing "AR", "ENT" here will cause a time out error
6737 5011 EXEC:
6740 5240 JMP M4 /go back to M4 with new data
6741 1052 M7, TAD ROTCTR:/get Rotation counter
6742 3053 DCR TEM9:/set up AVGV (average value) routine
6743 1201 TAD EE:
6744 3055 DCR TEM11:/with ROTCTR, BER2 AND AVBER
6745 1215 TAD AVBER:
6746 3050 DCR TEM7:
6747 4172 CALL:
6750 5440 AON:/APU on
6751 4172 CALL:
6752 4555 AVGV:/get new average (AVBER)
6753 1203 TAD I2:/now do it for INC
6754 3055 DCR TEM11:
6755 1215 TAD AVIN:
6756 3050 DCR TEM7:
6757 4172 CALL:
6760 4555 AVGV:/get new avinc
6761 2052 I2 ROTCTR /advance ROTCTR
6762 1217 TAD INL:/turn on "INC"lite
6763 4172 CALL:
6764 4620 LDM
6765 1215 TAD AVIN:/display average inclination
6766 4172 CALL:
6767 5355 AVG:
6770 5771 JMP I .+1:/jump to the MAIN2 patch, MZEX
6771 5422 MZEX

```

DD PC01153 MD6111 R0304 L1 D0

>2

240000000 MD7777 R0000 L0 D0

>2

>10000 2002

>2005

IC 0200 AT 0200

AON 5440
 CALL 4172
 MEMNOR 6500
 MEMSW 6100
 RETURN 5575
 SCDATA 6305
 STZ 6270

PC00241 MD5214 R0000 L1 D0

>2002 7002

>0

PC01505 MD5227 R0000 L0 D0

>7002 7002

>0

<SCDATA CALL

MEMNOR=6500;
 MEMSW=6100;
 CALL=4172;
 RETURN=5575;
 AON=5440;
 SCDATA=6305

◆6270

6270	6500	STZ	MEMNOR;
6271	4172		CALL;
6272	5440		AON;
6273	4172		CALL;
6274	6305		SCDATA;
6275	6100		MEMSW;
6276	5575		RETURN

MONITOR

SYMBOL DEFINITION

CALL=JMC CALLX
 RETURN=JMP I RETX
 MCRRA=6425
 MCRRA=6435
 MCRRE=6445
 MCRRE=6455
 FMT=6421
 FCK=6423
 MCK=6422
 KRD=6420

7776	<u>5210</u>	RESET,	♦7776
7777	5776		5210 JMP I .-1
			♦7800
7800	7567	J4A,	J4
7801	7773	NOTR,	-5
7802	7770	CHK,	-10
7803	7520	CK1,	-250
7804	7561	F,	FAULT
7805	0007	DOCTR,	7
7806	1200	PACK2,	TAD J4A
7807	3131		DCR NOTR1
7810	1201		TAD NOTR
7811	3005		DCR CTR
7812	2005	EEG,	ISZ CTR
7813	5215		JMP NUMB
7814	5575		RETURN
7815	4172	NUMB,	CALL
7816	7747		READ
7817	1127		TAD CHAR
7820	0202		AND CHK
7821	1203		TAD CK1
7822	7640		DCR CLA
7823	5604		JMP I F
7824	1127		TAD CHAR
7825	0205		AND DOCTR
7826	7100		CLL
7827	5531		JMP I NOTR1
7830	6420	CALLF,	KRI
7831	7300		CLR
7832	1241		TAD CPA
7833	4172		CALL
7834	7742		PRINT
7835	1242		TAD LPA
7836	4172		CALL
7837	7742		PRINT
7840	5575		RETURN
7841	0275	CPA,	ST5 1 = sign to save paper
7842	0275	LPA,	ST5 1 = sign to save paper

READER

TRI=6420
 SKIP=6422
 EXIT=7
 CTR1=6
 CTR=5
 DECT=4
 TEM=3

7243	7772	LD,	B1
7244	7286	B11,	B4
7245	7273	B2,	B3
7246	7332	B70,	B7
7247	7335	B80,	B8
7250	7756	CT1,	-B2
7251	7777	MOHE,	-1
7252	0077	MDK,	77
7253	6420	READER,	TRD
7254	6422		SKIP
7255	7000		NOZ
7256	7300		CLR CLL
7257	1244		TAD B11
7260	3003		DCR TEM
7261	1245		TAD B2
7262	3007		DCR EXIT
7263	3005		DCR CTR
7264	1250		TAD CT1
7265	3006		DCR CTR1
7266	3005	B4,	ISZ CTR
7267	5273		JMP B3
7270	2006		ISZ CTR1
7271	5273		JMP B3
7272	5643		JMP I LD
7273	7200	B3,	CLR
7274	6422		SKIP
7275	5403		JMP I TEM
7276	6420		TRD
7277	7006		RTL
7300	7006		RTL
7301	7104		CLL RAL
7302	7430		COL
7303	5407		JMP I EXIT
7304	7004	B1,	RAL
7305	7481		MOL
7306	7480		SNL
7307	5312		JMP B5
7310	1246		TAD B70
7311	3004		DCR DECT
7312	5315		JMP B6
7313	1247	B5,	TAD B80
7314	3004		DCR DECT

7315	7501	B6.	MOR
7316	7012		ATP
7317	7012		ATP
7320	7012		ATP
7321	0252		AND MSK
7322	7002		BSW
7323	7421		MOL
7324	6422		SKIP
7325	5324		JMP' .-1
7326	6420		TFD
7327	0252		AND MSK
7330	7501		MOR
7331	5404		JMP I DEST
7332	1251	B7.	TAD MONE
7333	3010		DCR 10
7334	7410		SKP
7335	3410	B8.	DCR I 10
7336	1243		TFD
7337	3007		DCR EXIT
7340	1245		TAD B2
7341	3003		DCR TEM
7342	5273		JMP B3
7343	0000	JM20.	0
7344	5541		JMP I MT+2
7345	2742		2742
7346	0000		0
7347	5544		JMP I PD+2
7350	2754		2754
7351	0000		0
7352	5547		JMP I PUSH+2
7353	2647		2647
7354	0000		0
7355	5552		JMP I MULF+2
7356	2665		2665
7357	0000		0
7360	5555		JMP I ADIF+2
7361	2633		2633
7362	0000		0
7363	5520		JMP I SUBF+2
7364	2641		2641
7365	0000		0
7366	5523		JMP I DIVF+2
7367	2625		2625
7370	0000		0
7371	5522		JMP I FLT+2
7372	2617		2617
7373	0000		0

			◆7400
7400	7534	CP1,	-354
7401	0272	CD,	272
7402	7540	CP,	-340
7403	0240	CPAC,	240
7404	7477	A,	-301
7405	7642	AC1,	AC2
7406	7646	AC3,	AC4
7407	7476	B,	-302
7410	7471	G,	-307
7411	7520	CHK1,	-320
7412	4167	JMPIN,	JMS JMPI
7413	7521	CLASH,	-357
7414	0136	NUM2,	NUM1
7415	0277	QUEST,	277
7416	7300	BEGIN,	CLA CLL
7417	4172		CALL
7420	7706		SETUP
7421	4172		CALL
7422	7230		CLF
7423	1201		TAD CD
7424	4172		CALL
7425	7742		PRINT
7426	7300		CLA CLL
7427	3130		DCR NUM
7430	4172		CALL
7431	7206		PACKS
7432	4172	NEXT,	CALL
7433	7747		READ
7434	1127		TAD CHAR
7435	1202		TAD CP
7436	7450		SNP
7437	5256		JMF DISP
7440	7200		CLA
7441	1127		TAD CHAR
7442	1207		TAD E
7443	7650		SNP CLA
7444	5333		JMF BKPT
7445	1127		TAD CHAR
7446	1210		TAD G
7447	7650		SNP CLA
7450	5606		JMF I AC3
7451	1127		TAD CHAR
7452	1204		TAD A
7453	7650		SNP CLA
7454	5205		JMF I AC1
7455	5361		JMF FAULT
7456	7100	DISP,	CLL
7457	4172		CALL
7460	7614		OUTC
7461	4172	NEXT1,	CALL
7462	7747		READ
7463	1130		TAD NUM
7464	3136		DCR NUM1
7465	1127		TAD CHAR
7466	1213		TAD CLASH
7467	7650		SNP CLA
7470	5276		JMF MOD
7471	1127		TAD CHAR
7472	1200		TAD CP1
7473	7650		SNP CLA
7474	5312		JMF MOD1
7475	5361		JMF FAULT

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7476 4172 MOD,   DCR NUM
7477 4172      CALL
7500 7808      PACKS
7501 4172      CALL
7502 7747      READ
7503 1127      TAD CHAR
7504 1200      TAD CP1
7505 7850      DCR CLR
7506 5810      JMP MODE
7507 5861      JMP FAULT
7510 1130 MODE,  TAD NUM
7511 3536      DCR I NUM1
7512 1136 MOD1,  TAD NUM1
7513 7001      IAC
7514 3136      DCR NUM1
7515 1214      TAD NUM2
7516 3130      DCR NUM
7517 4172      CALL
7520 7830      CALF
7521 4172      CALL
7522 7614      DOTS
7523 1203      TAD SPAC
7524 4172      CALL
7525 7742      PRINT
7526 1136      TAD NUM1
7527 3130      DCR NUM
7530 4172      CALL
7531 7614      DOTS
7532 5281      JMP NEXT1
7533 1135 BKPT,  TAD INSTR
7534 3526      DCR I LOC
7535 1130      TAD NUM
7536 3126      DCR LOC
7537 1530      TAD I NUM
7540 3135      DCR INSTR
7541 1212      TAD JMPIN
7542 3530      DCR I NUM
7543 5216      JMP BEGIN
7544 3132 BKPT1, DCR ACS
7545 1377      TAD AAC
7546 3130      DCR NUM
7547 7521      SWP
7550 3133      DCR MQ
7551 7004      RAL
7552 3134      DCR LINK
7553 4172      CALL
7554 7614      DOTS
7555 4172      CALL
7556 7830      CALF
7557 5216      JMP BEGIN
7560 0200 STK,   B00
7561 1360 FAULT, TAD STK
7562 3176      DCR 176
7563 1219      TAD QUEST
7564 4172      CALL
7565 7742      PRINT
7566 5216      JMP BEGIN

7567 7004 J4,   RAL
7570 7006      RTL
7571 7004      RAL
7572 7006      RTL
7573 7004      RAL
7574 7006      RTL
7575 5776      JMP I .+1
7576 7000

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7577	0132	AC0,	•7577 ACS
7500	1130		TAD NUM
7501	3130		DCA NUM
7502	1131		TAD NCTR1
7503	7001		IAC
7504	7001		IAC
7505	3131		DCA NCTR1
7506	5807		JMP I .+1
7507	7212		BSG
7510	7525	JSAI,	JS
7511	7773	NCTR1,	7773
7512	0007	OCTMKI,	7
7513	0260	ZEPD,	260
7514	1210	OUTS,	TAD JSAI
7515	3131		DCA NCTR1
7516	1211		TAD NCTR1
7517	3005		DCA CTR
7520	2005	OUTS1,	ISZ CTR
7521	5223		JMP OUTS2
7522	5575		RETURN
7523	1530	OUTS2,	TAD I NUM
7524	5531		JMP I NCTR1
7525	7010	JS,	RAR
7526	7012		RTF
7527	7010		RAP
7530	7012		RTF
7531	7010		RAP
7532	7012		RTF
7533	0212		AND OCTMKI
7534	1213		TAD ZEPD
7535	4172		CALL
7536	7742		PRINT
7537	3131		ISZ NCTR1
7540	3131		ISZ NCTR1
7541	5220		JMP OUTS1
7542	1130	AC2,	TAD NUM
7543	3132		DCA ACS
7544	5845		JMP I .+1
7545	7416		ZEGIN
7546	4172	AC4,	CALL
7547	7230		CALLF
7550	1134		TAD LINK
7551	7010		RAR
7552	7200		CLP
7553	1133		TAD NO
7554	7421		MDL
7555	1132		TAD ACS
7556	5530		JMP I NUM
7557	3177	CALLY,	DCA AC
7560	2176		ISZ STACK
7561	1173		TAD CALLX
7562	7001		IAC
7563	3576		DCA I STACK
7564	1572		TAD I CALLX
7565	3173		DCA CALLX
7566	1177		TAD AC
7567	5572		JMP I CALLX
7570	3177	RETY,	DCA AC
7571	1576		TAD I STACK
7572	3172		DCA CALLX
7573	7060		CAP CML
7574	1176		TAD STACK
7575	3176		DCA STACK
7576	1177		TAD AC

7700	4290	CPEGBA, 4	-1360
7701	4800	CPEGBE, 4	500
7702	7342	CODE, 1	JM03-1
7703	0136	COD, 1	136
7704	7747	CT, 1	-31
7705	7761	CD, 1	J03-1
7706	6481	SETUP, 1	PMT
7707	6480		KFD
7710	7200		CLA
7711	6445		WCPAB
7712	6425		WCPAA
7713	1301		TAD CPEGBE
7714	6455		WCPBB
7715	7200		CLA
7716	1300		TAD CPEGBA
7717	6435		WCPBA
7720	7200		CLA
7721	1304	TAD CT	
7722	3005		DCR CTR
7723	1302		TAD CODE
7724	3010		DCR 10
7725	1303		TAD COD
7726	3011		DCR 11
7727	1410	XX,	TAD I 10
7730	7040		CMA
7731	7450		CMA
7732	5526		JMP I LOC
7733	7040		CMA
7734	3411		DCR I 11
7735	2005		ICE CTR
7736	5327		JMP XX
7737	1305		TAD CD
7740	3010		DCR 10
7741	5327		JMP XX
7742	6423	PRINT,	PCY
7743	5342		JMP .-1
7744	6421		PMT
7745	7200		CLA CLL
7746	5575		RETURN
7747	7200	READ,	CLA
7750	6422		KCK
7751	5350		JMP .-1
7752	6420		KFD
7753	0361		AND .+6
7754	3127		DCR CHAR
7755	1127		TAD CHAR
7756	4172		CALL
7757	7742		PRINT
7760	5575		RETURN
7761	0377		SET
7762	5571	JOB,	JMP I CALLX-1
7763	7544		BRPT1
7764	0000		0
7765	5574		JMP I CALLX+2
7766	7657		CALLY
7767	7670		RESTY
7770	6200		STACK+2
7771	7777		7777
7772	1375	BT,	TAD BE
7773	3126		DCR LOC
7774	5306		JMP SETUP
7775	7416	BE,	BEGIN

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                                ♦137
0137 0000 WT, 0
0140 5541 JMP I .+1
0141 2742 2742
0142 0000 RD, 0
0143 5544 JMP I .+1
0144 2754 2754
0145 0000 PUCH, 0
0146 5547 JMP I .+1
0147 2647 2647
0150 0000 MULF, 0
0151 5552 JMP I .+1
0152 2665 2665
0153 0000 ADDF, 0
0154 5555 JMP I .+1
0155 2633 2633
0156 0000 SUBF, 0
0157 5560 JMP I .+1
0160 2641 2641
0161 0000 DIVF, 0
0162 5563 JMP I .+1
0163 2625 2625
0164 0000 FLT, 0
0165 5566 JMP I .+1
0166 2617 2617
0167 0000 JMPI, 0
0170 5571 JMP I .+1
0171 7544 BKPT1
0172 0000 CALLX, 0
0173 5574 JMP I .+1
0174 7657 CALLY
0175 7670 RETX, RETY
0176 0600 STACK, .+2
0177 0000 RC, 0
RAM
♦136
0126 0000 LDC, 0
0127 0000 CHAR, 0
0130 0000 NUM, 0
0131 0000 NCTR1, 0
0132 0000 ACS, 0
0133 0000 MD, 0
0134 0000 LINK, 0
0135 0000 INSTR, 0
0136 0000 NUM1, 0

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PRINT

←EQUATES
CALL=4172;
RETURN=5575;
BACTR=100;
AUTO=10;
ALPHA=102;
DICTR1=24;
DICTR2=25;
BA=103;
S=123;
D=114;
Q=115;
J=116;
T=117;
ROCTR=120;
ELCTR=121;
DICTR=122;
A=77;
ADR=100;
ADR1=101;
C=124;
CTRS=47;
DINC=1461;
MCARR=6425;
BMS=6451;
DISCC=3234

←CONSTANTS

♦5000
5000 0037 MCK1, 37;
5001 4000 DIGIT, 4000;
5002 7775 FOURM, -3;
5003 0017 MCK2, 17;
5004 5236 DOTM, DOTS;
5005 5256 CHARM, CHAR;
5006 0102 BAA, BA-1
5007 7776 PD, -2;
5010 7772 PDS, -6;
5011 7773 EL, -5;
5012 7771 DP, -7;
5013 0040 PWR, 40;
5014 0004 FOUR, 4
5015 5212 PEE12, F12;
5016 5204 PEE14, F14;
5017 5103 PES, P5
5020 4172 PRINT, CALL;
5021 5400 PON;
5022 3120 DCA ROCTR;
5023 3121 DCA ELCTR;
5024 7300 CLA CLL
5025 1206 TRD BAA;
5026 3010 DCA AUTO;

5030	7430	COL;
5031	7002	EDM;
5032	0200	AND MCK1;
5033	3410	DCR I AUTO;
5034	7630	COL CLR
5035	5240	JMP P2;
5036	7120	STL;
5037	5227	JMP P1;
5040	1025	P2, TAD DIOPF2;
5041	4172	CALL;
5042	5443	DISSUB;
5043	1024	TAD DIOPF1;
5044	4172	CALL;
5045	5443	DISSUB
5046	1214	TAD FOUR;
5047	4172	CALL;
5050	3234	DISCO
5051	1217	START, TAD PES;
5052	3101	DCR ADR1
5053	7330	PS, CLA STL BAR;
5054	3114	DCR D;
5055	3122	DCR DICTR;
5056	1206	TAD BAR;
5057	3010	DCR AUTO
5060	1410	P11, TAD I AUTO;
5061	7104	OLL PAL;
5062	1205	TAD CHARM;
5063	3117	DCR T;
5064	1120	TAD ROCTR;
5065	1202	TAD FOURM
5066	7640	DCR CLA;
5067	5272	JMP .+3;
5070	1217	TAD PES;
5071	3101	DCR ADR1;
5072	7330	ENL CLA
5073	5275	JMP .+2;
5074	2117	ISS T;
5075	1517	TAD I T;
5076	5501	JMP I ADR1
5077	7012	P4, RTR;
5100	7012	RTR;
5101	7012	RTR;
5102	7012	RTR
5103	0203	PS, AND MCK2;
5104	1204	TAD DOTEM;
5105	3100	DCR ADR;
5106	1201	TAD DIGIT;
5107	6425	MCARR
5110	7200	CLA;
5111	1114	TAD D;
5112	6451	EM2
5113	7201	P20, CLA IAC;
5114	3124	DCR C;
5115	3121	DCR ELCTR
5116	6425	P8, MCARR
5117	1124	P9, TAD C;
5120	0500	AND I ADR;
5121	7450	ONR;
5122	5327	JMP P7;
5123	1213	TAD PWR;
5124	6451	EM2;
5125	4172	CALL;
5126	5412	BURN

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5130 7104    CLL PAR;
5131 3124    DCA C;
5132 3121    ISZ ELCTR;
5133 1121    TAD ELCTR;
5134 1211    TAD EL;
5135 7640    SZA CLA;
5136 5317    JMP P9;
5137 3121    DCA ELCTR;
5140 2122    P10, ISZ DICTR;
5141 1114    TAD D;
5142 7110    CLL PAR;
5143 3114    DCA D;
5144 1122    TAD DICTR;
5145 1207    TAD PD;
5146 7650    SNA CLA;
5147 5340    JMP P10;
5150 1201    TAD DIGIT;
5151 6425    MCRAR;
5152 7200    CLA;
5153 1114    TAD D;
5154 6451    BMB;
5155 7200    CLA;
5156 1122    TAD DICTR;
5157 1212    TAD DF;
5160 7640    SZA CLA;
5161 5616    JMP I PEE14;
5162 1120    TAD RDCTR;
5163 7640    SZA CLA;
5164 5340    JMP P10;
5165 1204    TAD DOTEM;
5166 7001    IAC;
5167 7001    IAC;
5170 3100    DCA ADR;
5171 5313    JMP P20;

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      +5200
5200 7776    ROT, -2;
5201 7766    DI, -12;
5202 7772    RDSN, -6;
5203 5053    PEE6, P6;
5204 1201    P14, TAD DI;
5205 1122    TAD DICTR;
5206 7650    SNA CLA;
5207 5212    JMP P12;
5210 5611    JMP I .+1;
5211 5060    P11;
5212 1101    P12, TAD ADR1;
5213 1200    TAD ROT;
5214 3101    DCA ADR1;
5215 2120    ISZ RDCTR;
5216 4172    CALL;
5217 5424    MOTOR;
5220 1202    TAD RDSN;
5221 1120    TAD RDCTR;
5222 7640    SZA CLA;
5223 5603    JMP I PEE6;
5224 4172    CALL;
5225 5424    MOTOR;
5226 4172    CALL;
5227 5424    MOTOR;
5230 6451    BMB;
5231 5575    RETURN;

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CTR4=72
♦5400:

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5400	7300	FORN, CLA CLL;
5401	6425	MCARR;
5402	1266	TAD FMR2;
5403	6451	BW2
5404	7200	CLA;
5405	1265	TAD DEL
5406	3072	DCA CTR4;
5407	2072	ISZ CTR4;
5410	5207	JMP .-1;
5411	5575	RETURN;
5412	7200	BURN, CLA;
5413	1264	TAD BRST;
5414	6425	MCARR;
5415	7200	CLA
5416	1263	TAD BUR;
5417	3047	DCA CTR3;
5420	3047	ISZ CTR3;
5421	5220	JMP .-1;
5422	6425	MCARR;
5423	5575	RETURN;
5424	7200	MOTOR, CLA;
5425	1271	TAD MOT
5426	6425	MCARR;
5427	7200	CLA;
5430	1270	TAD MOT2;
5431	3047	DCA CTR3;
5432	6451	MOT1, BW2;
5433	1267	TAD MOTIM;
5434	3072	DCA CTR4;
5435	2072	ISZ CTR4
5436	5235	JMP .-1;
5437	2047	ISZ CTR3;
5440	5232	JMP MOT1;
5441	6425	MCARR;
5442	5575	RETURN;
5443	3077	DISSUB, DCA A;
5444	1273	TAD THR
5445	3047	DCA CTR3;
5446	1077	DISS, TAD A;
5447	0272	AND MSK;
5450	7104	CLL PAL;
5451	7006	RTL;
5452	7006	RTL;
5453	3410	DCA I AUTO;
5454	1077	TAD A
5455	7006	RTL;
5456	7006	RTL;
5457	3077	DCA A;
5460	3047	ISZ CTR3
5461	5246	JMP DISS;
5462	5575	RETURN
5463	5577	BUR, 5577;
5464	7000	BRST, 7000;
5465	0320	DEL, 320;
5466	0040	AMPC, 40;
5467	7300	MOTIM, 7300
5470	7774	MOT2, -4;
5471	2000	MOT, 2000;
5472	7400	MCH, 7400;
5473	7775	THR, -3

410. PIT AND CURVEY PRINT ROUTINES

CALL=4172;
 RETURN=5575;
 ALPHA=102;
 INIT1=8433;
 RESTR1=8445;
 CURV1=8456;
 AUTO1=13;
 AUTO2=14;
 CTR6=15;
 STOR=30

◆4400

4400	7200	<u>INCO</u> , CLA;
4401	1211	TAD INI;
4402	3102	DCA ALPHA;
4403	1334	TAD ADD2;
4404	3030	DCA STOR;
4405	4172	CALL;
4406	4436	PRINIT;
4407	5610	JMP I .+1
4410	8433	INIT1;
4411	2117	INI, 2117

4412	7200	<u>RST</u> , CLA;
4413	1223	TAD RS;
4414	3102	DCA ALPHA;
4415	1333	TAD ADD3;
4416	3030	DCA STOR;
4417	4172	CALL;
4420	4436	PRINIT;
4421	5622	JMP I .+1
4422	6445	RESTR1;
4423	2322	RS, 2322

4424	7200	<u>SUR</u> , CLA;
4425	1234	TAD SV;
4426	3102	DCA ALPHA;
4427	3030	DCA STOR;
4430	4172	CALL;
4431	4436	PRINIT;
4432	5633	JMP I .+1;
4433	6456	CURV1;
4434	2523	SV, 2523

TEST

CALL=4172;
 RETURN=5575;
 ACM=5440;
 LCM=4620;
 LCM1=4622;
 DISS=3672
 AUTO=17;
 STCLK=6600;
 ICMGR=6047;
 MCRAB=6445;
 MCRBB=6455;
 DATA=3405
 SCDATA=6305;
 BSS=6443;
 M=4150;
 W=4137;
 CTR3=47;
 CTR4=16;
 TEMN=101
 R=4142;
 TEMP=100;
 DISPR1=24;
 DISPR2=25;
 CONV=6014;
 LOA=3154
 STPAT=6046;
 ELCTR=121;
 POCTR=120;
 POM=5400;
 STSTD=6411;
 STSTC=6417
 APUCF=6600;
 STZ=6870

*5600

5600	7200	STEST, CLR;
5601	1366	TAD EIGHT;
5602	3024	DCA DISPR1;
5603	1365	TAD EIGHTS
5604	3025	DCA DISPR2;
5605	4172	CALL;
5606	3672	DISS;
5607	7200	CLR;
5610	1356	TAD FIV;
5611	4172	CALL;
5612	5340	DELAY;
5613	4172	CALL;
5614	3154	LOA;
5615	1387	TAD SIXT;
5616	3047	DCA CTR3
5617	1331	TAD DATA;
5620	3017	DCA AUTO;
5621	1330	ST1, TAD TWEL;
5622	3016	DCA CTR4
5623	1417	TAD I AUTO;

5624	6047	ICC TR3:
5625	6600	CTCLK:
5626	7010	APP:
5627	6047	ICC TR3:
5630	5232	JMP .+2:
5631	5236	JMP .+5
5632	6016	ICC TR4:
5633	5224	JMP ST2:
5634	7200	CLA:
5635	5221	JMP ST1:
5636	7200	CLA
5637	1352	TAD CCYHC:
5640	6445	MCRAB:
5641	7200	CLA:
5642	1355	TAD FIF:
5643	4172	CALL:
5644	5340	DELAY
5645	1353	TAD BCYHC:
5646	6445	MCRAB:
5647	7200	CLA:
5650	1356	TAD FIV:
5651	4172	CALL:
5652	5340	DELAY
5653	1354	TAD DATS:
5654	6445	MCRAB:
5655	7200	CLA:
5656	6007	CAF:
5657	6443	BSE:
5660	5257	JMP .-1
5661	5662	JMP I .+1:
5662	6411	STSTD:
5663	7200	RET, CLA:
5664	1328	TAD NUMB:
5665	3017	DCA AUTO:
5666	1362	TAD TEN:
5667	3018	DCA TR4
5670	1325	SACK, TAD BLK:
5671	3417	DCA I AUTO:
5672	3016	ICC TR4:
5673	5270	JMP BACK
5674	4172	CALL:
5675	5400	POH:
5676	3121	DCA ELCTR:
5677	3120	DCA FOOTR:
5700	4172	CALL:
5701	5046	START
5702	4172	CALL:
5703	6270	ST2:
5704	6600	APUDF:
5705	7200	CLA:
5706	1362	TAD TEN:
5707	3100	DCA TEMP:
5710	1357	TAD CHAN
5711	3101	DCA TEMN:
5712	4172	DICP, CALL:
5713	6417	STSTD:
5714	1362	TAD TEN:
5715	4172	CALL:
5716	5340	DELAY
5717	1101	TAD TEMN:
5720	1363	TAD FOUR:
5721	3101	DCA TEMN:
5722	3100	ICC TEMP:
5723	5312	JMP DICP:
5724	5764	JMP I RDTREC

```

5725 0026 ELP, 26;
5726 0102 RUMP, 102;
5727 7400 CINT, -400;
5728 7764 TMEL, -14;
5731 5731 DATA, .;
5732 5415 5415;
5733 0323 0323;
5734 7473 7473;
5735 7777 7777;
5736 7777 7777;
5737 7774 7774;
5740 1475 1475;
5741 1467 1467;
5742 4643 4643;
5743 3111 3111;
5744 0226 0226;
5745 3100 3100;
5746 2146 2146;
5747 1146 1146;
5750 2463 2463;
5751 5314 5314;
5752 2000 CSYNC, 2000;
5753 4000 BSYNC, 4000;
5754 6000 DATS, 6000;
5755 7563 FIF, -215;
5756 7721 FIV, -57;
5757 0243 CHAN, 243;
5760 2024 TWO, 2024;
5761 0567 DEBUG, 567;
5762 7766 TEN, -12;
5763 0004 FOUR, 4;
5764 7100 FDTREC, 7100;
5765 0210 EIGHTS, 210;
5766 4210 EIGHT, 4210
      *5340
       DELAY
5340 3047 DELAY, DCA CTR3;
5341 3016 DCA CTR4;
5342 2016 ISZ CTR4;
5343 5342 JMP .-1;
5344 2047 ISZ CTR3;
5345 5342 JMP .-3;
5346 5575 RETURN

```

FROM BURNER

*PUT HIGH ADDR IN 1000
 *PUT LOW ADDR IN 1001
 *PUT FROM START ADDR IN 1002
 *ENTER 1200 FOR WRITE
 *THEN, PRESS "C" TO READ, OR ,
 *ENTER 1200 FOR READ
 *BELL RINGS ON ERROR, PRINTS D IF OK
 *ERROR LOC IS IN 1025, FROM DATA IS IN 1023,
 / "SHOULD BE" IS IN 1021.
 *HALTS AFTER START TO GIVE TIME FOR -40V, 100MA LIMIT
 / VOLTAGE TO BE TURNED ON.

FCK=8113
 FWT=8111
 MORA=8465
 MORB=8475
 F1=8460
 M1=8461

1200 G must be executed before turning on 40 v

To step in the middle of a burn, turn off -40 v first, then hit break.

*1000

1000	0000	HI,	0
1001	0000	LD,	0
1002	0000	FROM,	0
1003	0360	M,	360
1004	6400	F1,	6400
1005	7400	F2,	7400
1006	2400	F3,	2400
1007	0400	F4,	400
1010	6000	F5,	6000
1011	0207	BELL,	207
1012	0304	D,	304
1013	0000	JUM,	0
1014	1064	J1,	JUMP
1015	7776	HUN,	-2
1016	0000	CTR1,	0
1017	5513	C15,	5513
1020	7133	C5,	7133
1021	0000	HLD,	0
1022	0000	CTR,	0
1023	0000	HLD1,	0
1024	0000	L,	0
1025	0000	F,	0
1026	0017	MAK,	17

1027	6111		CLA
1030	6111		FMT
1031	1203		TAD W
1032	6475		MOFB
1033	7200		CLA
1034	1202		TAD FROM
1035	3225		DCA P
1036	1201		TAD LO
1037	3224		DCA L
1040	1204		TAD F1
1041	6465		MOFA
1042	7402	FB,	HLT
1043	7200	FB,	CLA
1044	1215		TAD HUN
1045	3216		DCA CTR1
1046	7604	FB,	LAS
1047	1214		TAD J1
1050	3213		DCA JUM
1051	1225		TAD P
1052	6461		M1
1053	7200		CLA
1054	1205		TAD F2
1055	6465		MOFA
1056	7200		CLA
1057	1204		TAD F1
1060	6465		MOFA
1061	7200		CLA
1062	1624		TAD I L
1063	5813		JMP I JUM
1064	7012	JUMP,	ATR
1065	7012		ATR
1066	7012		ATR
1067	7012		ATR
1070	0226		AND MASK
1071	3221		DCA HLD
1072	1221	JUMP1,	TAD HLD
1073	6461		M1
1074	7200		CLA
1075	1206		TAD F3
1076	6465		MOFA
1077	7200		CLA
1100	1207		TAD F4
1101	6465		MOFA
1102	7200		CLA
1103	1217		TAD C15
1104	3222		DCA CTR
1105	2222	P1,	ISZ CTR
1106	5305		JMP P1
1107	1206		TAD F3
1110	6465		MOFA
1111	7200		CLA
1112	1220		TAD C5
1113	3222		DCA CTR
1114	2222	P2,	ISZ CTR
1115	5314		JMP P2

1116	1204	F21.	TAD F1
1117	6485		MOFA
1120	7200		CLA
1121	1210		TAD F5
1122	6485		MOFA
1123	6480		F1
1124	0226		AND MARK
1125	3223		DOA HLD1
1126	1204		TAD F1
1127	6485		MOFA
1130	7200		CLA
1131	1221		TAD HLD
1132	7041		OMA IAC
1133	1223		TAD HLD1
1134	7640		DOA CLA
1135	5337		JMP F3
1136	5346		JMP F4
1137	2216	F3.	ISZ CTR1
1140	5246		JMP F5
1141	1211	F31.	TAD BELL
1142	6113		POK
1143	5342		JMP .-1
1144	6111		PWT
1145	7402		HLT
1146	2225	F4.	ISZ P
1147	2224		ISZ L
1150	7000		NOP
1151	1200		TAD HI
1152	7040		OMA
1153	1224		TAD L
1154	7640		DOA CLA
1155	5243		JMP F6
1156	1212		TAD D
1157	6113		POK
1160	5357		JMP .-1
1161	6111		PWT
1162	7402		HLT
1163	6111		6111
1164	6113		6113
1165	7000		NOP
1166	5787		JMP I .+1
1167	1230		READ

T=TAD BELL
H=TAD HLD
J4=JMP F4
J=JMP F31

◆1200

```

1200 7200 00172.  CLR
1201 1216      TAD 17
1202 3815      DCA I 16
1203 1214      TAD 15
1204 3813      DCA I 14
1205 1221      TAD 110
1206 3820      DCA I 109
1207 5812      JMP I 103
    
```

```

1210 1211 01.  T
1211 5316 02.  J
1212 1027 03.  BEGIN
1213 1072 04.  JUMP1
1214 1221 05.  H
1215 1141 06.  F31
1216 5346 07.  J4
1217 7000 08.  NOP
1220 1042 09.  FB
1221 7402 10.  HLT
      +1230
    
```

```

1230 7200 READ.  CLR
1231 1211      TAD 02
1232 3813      DCA I 14
1233 1210      TAD 01
1234 3815      DCA I 16
1235 1217      TAD 08
1236 3820      DCA I 109
1237 5812      JMP I 103
    
```

ONES FILLER

>HI REF IN 400
>LO REF IN 401

+400

```

0400 0000 HIGH.  0
0401 0000 LOW.   0
0402 7200 ONES.  CLR
0403 1201      TAD LOW
0404 3010      DCA 10
0405 7040 ON.   CMA
0406 3410      DCA I 10
0407 1200      TAD HIGH
0410 7040      CMA
0411 1010      TAD 10
0412 7840      DCA CLR
0413 5205      JMP ON
0414 7402      HLT
    
```

GENERAL DISCUSSION

Consider a right-handed rectangular coordinate system X, Y, Z , defined by the local magnetic north direction (X -axis) with the Z direction being the local gravitationally defined vertical.

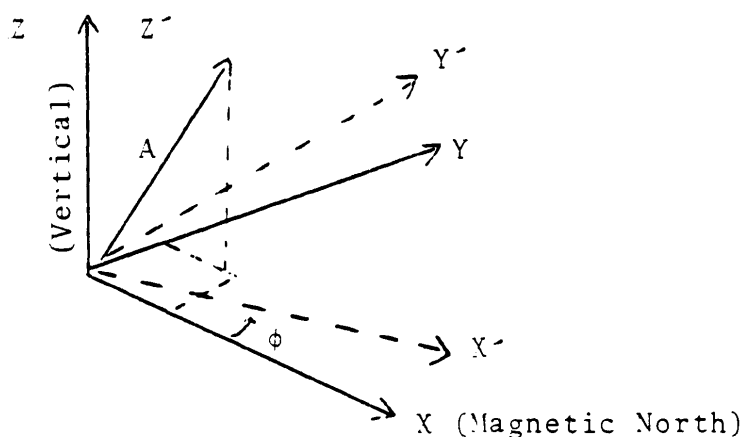


Figure 1

Let the components of an arbitrary vector \vec{A} be given by A_x , A_y , and A_z in this coordinate system. Our first objective is to be able to calculate the components of this vector in another right-handed coordinate system defined by three successive and independent rotations:

- a. A rotation ϕ about the Z axis ($-\pi \leq \phi \leq +\pi$)
- b. A rotation θ about the new Y' axis ($-\pi/2 \leq \theta \leq \pi/2$)
- c. A rotation ψ about the new X' axis ($-\pi \leq \psi \leq \pi$)

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ESS/SAS Divisions.

Let \vec{A}' denote the components of \vec{A} in the new coordinate system defined by the first rotation about **Z axis** of Figure 1. Then we have:

$$\begin{aligned} A'_z &= A_z \\ A'_x &= A_x \cos\phi + A_y \sin\phi \\ A'_y &= -A_x \sin\phi + A_y \cos\phi \end{aligned} \tag{1}$$

Next, let \vec{A}'' denote the components of \vec{A} in the coordinate system defined by the second rotation about **the Y' axis** (see figure below).

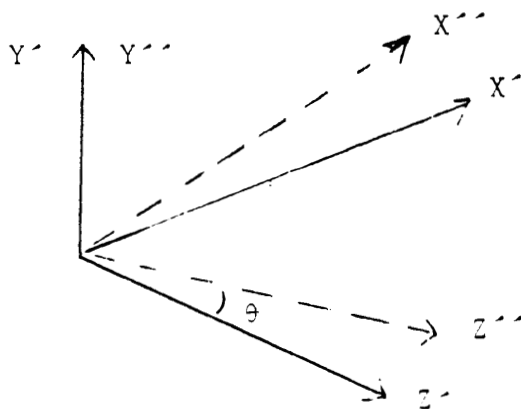


Figure 2

Thus:

$$\begin{aligned} A''_y &= A'_y \\ A''_z &= A'_z \cos\theta + A'_x \sin\theta \\ A''_x &= -A'_z \sin\theta + A'_x \cos\theta \end{aligned} \tag{2}$$

Finally, let \vec{A}''' denote the components of \vec{A} in the coordinate system defined by the third rotation about the X''' axis (see figure below).

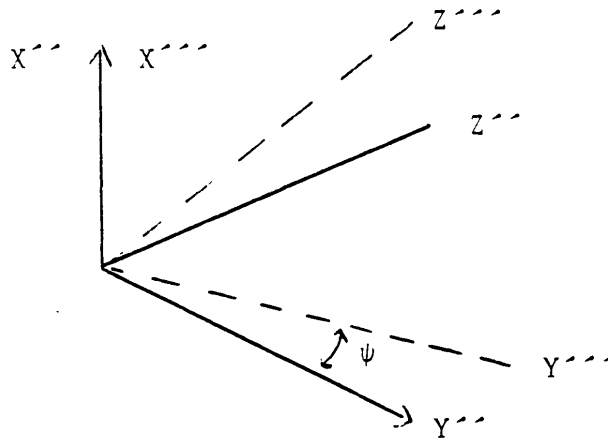


Figure 3

Again we have:

$$\begin{aligned}
 A_x''' &= A_x'' \\
 A_y''' &= A_y'' \cos \psi + A_z'' \sin \psi \\
 A_z''' &= -A_y'' \sin \psi + A_z'' \cos \psi
 \end{aligned}
 \tag{3}$$

In matrix ~~form~~, these rotations can be expressed as

$$\begin{aligned}
 \vec{A}' &= [R_\phi] \vec{A} \\
 \vec{A}'' &= [R_\theta] \vec{A}' \\
 \vec{A}''' &= [R_\psi] \vec{A}''
 \end{aligned}
 \tag{4}$$

where the R's are defined by the above equations.

$$R_\phi = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_\theta = \begin{bmatrix} \cos\theta & 0 & -\sin\theta \\ 0 & 1 & 0 \\ \sin\theta & 0 & \cos\theta \end{bmatrix}
 \tag{5}$$

$$R_\psi = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\psi & \sin\psi \\ 0 & -\sin\psi & \cos\psi \end{bmatrix}$$

The transformation from \vec{A} to the final \vec{A}''' is defined by:

$$\vec{A}''' = [R_\psi][R_\theta][R_\phi]\vec{A}
 \tag{6}$$

Thus the matrix product

$$[R] = [R_\psi][R_\theta][R_\phi] \quad (7)$$

defines the general matrix for transforming coordinates from the initial to final coordinate system. Performing the successive matrix multiplications yields:

$$[R] = \begin{bmatrix} \cos\theta\cos\phi & \cos\theta\sin\phi & -\sin\theta \\ -\cos\psi\sin\phi & \cos\psi\cos\phi & \sin\psi\cos\phi \\ +\sin\psi\sin\theta\cos\phi & +\sin\psi\sin\theta\sin\phi & \\ \sin\psi\sin\phi & -\sin\psi\cos\phi & \cos\psi\cos\theta \\ +\cos\psi\sin\theta\cos\phi & +\cos\psi\sin\theta\sin\phi & \end{bmatrix} \quad (8)$$

Our second objective is the following. Let the local magnetic field \vec{F} be defined and known in the (XYZ) coordinate system as

$$\begin{aligned} F_x &= F\cos\alpha \\ F_y &= 0 \\ F_z &= -F\sin\alpha \end{aligned} \quad (9)$$

where α =dip angle ($0 \leq \alpha \leq \pi/2$). F_y is zero since the X-axis is defined as the magnetic north. Let the local gravitational field be known and defined as

$$\begin{aligned} G_x &= 0 \\ G_y &= 0 \\ G_z &= -G \end{aligned} \quad (10)$$

Now assume that we are given measured components of \vec{F} along the $(X''''Y''''Z''')$ coordinate system (or the direction cosines since magnitude F is known). Also, we are given the components of \vec{G} along the $(X''''Y''''Z''')$ coordinate system.

From this information we are to estimate the values of the rotation parameter ϕ , θ , and ψ . That is, calculate the orientation of the $(X''''Y''''Z''')$ coordinate system.

Using the rotation matrix $[R]$ given by equation (8), we get for the magnetic field components

$$\begin{aligned} X_{\text{cos}} &= \cos\theta\cos\phi\cos\alpha + \sin\theta\sin\alpha \\ Y_{\text{cos}} &= -\cos\psi\sin\phi\cos\alpha + \sin\psi[\sin\theta\cos\phi\cos\alpha - \cos\theta\sin\alpha] \\ Z_{\text{cos}} &= +\sin\psi\sin\phi\cos\alpha + \cos\psi[\sin\theta\cos\phi\cos\alpha - \cos\theta\sin\alpha] \end{aligned} \quad (11)$$

where

$$\begin{aligned} X_{\text{cos}} &= F'_x/F \\ Y_{\text{cos}} &= F'_y/F \\ Z_{\text{cos}} &= F'_z/F \end{aligned} \quad (12)$$

For the gravitational field we get

$$G'_x = (+\sin\theta)G \quad (13)$$

θ PARAMETER

Given the G'_x and G values, equation (13) gives:

$$\theta = \sin^{-1} \left(\frac{G'_x}{G} \right) \quad (14)$$

Given that G and G'_X are well defined and $G > 0$ and that θ is restricted to $-\pi/2 < \theta < \pi/2$, we have a valid and unique estimation for θ .

ϕ PARAMETER

The first equation of equations (11) can be solved for $\cos\phi$ as

$$\cos\phi = \frac{X\cos - \sin\theta\sin\alpha}{\cos\theta\cos\alpha} \quad (15)$$

where θ and α are known quantities.

The second and third of equations (11) are solved for $\sin\phi$:

$$Y\cos(\cos\psi) = -\cos^2\psi\sin\phi\cos\alpha + A$$

$$Z\cos(\sin\psi) = \sin^2\psi\sin\phi\cos\alpha + A$$

where: $A = \sin\psi\cos\psi[\sin\theta\cos\phi\cos X - \cos\theta\sin\alpha]$

subtracting the two, and solving for $\sin\phi$:

$$\sin\phi = \frac{\sin\psi Z\cos - \cos\psi Y\cos}{\cos\alpha}$$

$$\text{or } \phi = \tan^{-1} \left[\frac{\sin\phi}{\cos\phi} \right] \quad (16)$$

ψ PARAMETER

The ψ parameter is derived from the components of the \vec{G} in the direction of G_Y and G_Z as follows:

$$\psi = \tan^{-1} \frac{-G_Y}{-G_Z}$$

θ is inclination $-\pi/2$, ϕ is bearing and ψ is package rotation.

NORMALIZATION

Each of the three sensor values from the magnetometers and the accelerometers must be normalized as in the following example:

$$X_{\text{cos norm}} = \frac{X_{\text{cos}}}{\sqrt{X_{\text{cos}}^2 + Y_{\text{cos}}^2 + Z_{\text{cos}}^2}}$$

Therefore, all of the operational algorithms use normalized values.

THE SURVEY EQUATIONS

The following are used for survey equations. This is a straight line between points, angle averaging method, and the assumed rod length normally is 10 feet to minimize errors.

Survey

$$\cos(\overline{\text{INC}})\cos(\overline{\text{BER}}) \text{ rod1} + \text{LAT2} = \text{LAT1}$$

$$\cos(\overline{\text{INC}})\sin(\overline{\text{BER}}) \text{ RODL} + \text{DEP2} = \text{DEP1}$$

$$\text{VD2} - \sin(\overline{\text{INC}}) \text{ RODL} = \text{VD1}$$

$$\sqrt{(\text{VD1})^2 + (\text{LAT1})^2 + (\text{DEP1})^2} = \text{THD}$$

$$\sin(\text{TAN}^{-1}\left(\frac{\text{DEP1}}{\text{LAT1}}\right) - \text{ABER}) \cdot \sqrt{(\text{LAT1})^2 + (\text{DEP1})^2} = \text{HDEV}$$

$$\text{VD1} - \sin(\text{AINC} - \pi/2)\cos(\text{TAN}^{-1}\left(\frac{\text{DEP1}}{\text{LAT1}}\right) - \text{ABER})\sqrt{(\text{LAT1})^2 + (\text{DEP1})^2} = \text{VDEV}$$

Initial Hole Conditions

$$\sin (AINC - \pi/2) SLEN = VD1$$

$$\sin (ABER) \cos(AINC - \pi/2) SLEN = DEP1$$

$$\cos (ABER) \cos(AINC - \pi/2) SLEN = LAT1$$

where

ABER = initial bearing

AINC = initial indication

\overline{BER} = average bearing, previous survey and current survey

\overline{INC} = average inclination, previous survey and current survey

VD1 = current vertical depth

VD2 = previous vertical depth

LAT1 = current latitude

LAT2 = previous latitude

DEP1 = current departure

DEP2 = previous departure

RODL = rod length

THD = tone hole depth

HDEV = horizontal deviation

VDEV = vertical deviation

SLEN = string length